ETSI TR 138 903 V15.0.0 (2018-10)

TECHNICAL REPORT

5G;
NR;
Derivation of test tolerances and measurement uncertainty for User Equipment (UE) conformance test cases
(3GPP TR 38.903 version 15.0.0 Release 15)

Reference

DTR/TSGR-0538903vf00

Keywords

5G

ETSI

650 Route des Lucioles
F-06921 Sophia Antipolis Cedex - FRANCE

Tel.: +33 4 92 94 42 00 Fax: +33 4 93 65 47 16

Siret N° 348 623 562 00017 - NAF 742 C
Association à but non lucratif enregistrée à la
Sous-Préfecture de Grasse (06) N° 7803/88

Intellectual Property Rights

Essential patents

IPRs essential or potentially essential to normative deliverables may have been declared to ETSI. The information pertaining to these essential IPRs, if any, is publicly available for **ETSI members and non-members**, and can be found in ETSI SR 000 314: *"Intellectual Property Rights (IPRs); Essential, or potentially Essential, IPRs notified to ETSI in respect of ETSI standards"*, which is available from the ETSI Secretariat. Latest updates are available on the ETSI Web server (https://ipr.etsi.org/).

Pursuant to the ETSI IPR Policy, no investigation, including IPR searches, has been carried out by ETSI. No guarantee can be given as to the existence of other IPRs not referenced in ETSI SR 000 314 (or the updates on the ETSI Web server) which are, or may be, or may become, essential to the present document.

Trademarks

The present document may include trademarks and/or tradenames which are asserted and/or registered by their owners. ETSI claims no ownership of these except for any which are indicated as being the property of ETSI, and conveys no right to use or reproduce any trademark and/or tradename. Mention of those trademarks in the present document does not constitute an endorsement by ETSI of products, services or organizations associated with those trademarks.

Foreword

This Technical Report (TR) has been produced by ETSI 3rd Generation Partnership Project (3GPP).

The present document may refer to technical specifications or reports using their 3GPP identities, UMTS identities or GSM identities. These should be interpreted as being references to the corresponding ETSI deliverables.

The cross reference between GSM, UMTS, 3GPP and ETSI identities can be found under http://webapp.etsi.org/key/queryform.asp.

Modal verbs terminology

In the present document "**should**", "**should not**", "**may**", "**need not**", "**will**", "**will not**", "**can**" and "**cannot**" are to be interpreted as described in clause 3.2 of the ETSI Drafting Rules (Verbal forms for the expression of provisions).

"**must**" and "**must not**" are **NOT** allowed in ETSI deliverables except when used in direct citation.

Contents

Foreword

This Technical Report has been produced by the 3rd Generation Partnership Project (3GPP).

The contents of the present document are subject to continuing work within the TSG and may change following formal TSG approval. Should the TSG modify the contents of the present document, it will be re-released by the TSG with an identifying change of release date and an increase in version number as follows:

Version x.y.z

where:

- x the first digit:
  - 1 presented to TSG for information;
  - 2 presented to TSG for approval;
  - 3 or greater indicates TSG approved document under change control.
- y the second digit is incremented for all changes of substance, i.e. technical enhancements, corrections, updates, etc.
- z the third digit is incremented when editorial only changes have been incorporated in the document.

Introduction

FFS

1 Scope

The present document specifies a general method used to derive Measurement Uncertainties and Test Tolerances for UE conformance tests. The acceptable uncertainties for each test case are documented and establish a system for relating the Test Tolerances to the measurement uncertainties of the Test System.

For UE radio transmitting and reception tests, only FR2 is considered in this document. For UE RRM and Demodulation tests, both FR1 and FR2 are considered in this document.

The test cases which have been analysed to determine Test Tolerances are included as .zip files.

The present document is applicable from Release 15 up to the release indicated on the front page of the present Terminal conformance specifications.

2 References

The following documents contain provisions which, through reference in this text, constitute provisions of the present document.

- References are either specific (identified by date of publication, edition number, version number, etc.) or non-specific.
- For a specific reference, subsequent revisions do not apply.
- For a non-specific reference, the latest version applies. In the case of a reference to a 3GPP document (including a GSM document), a non-specific reference implicitly refers to the latest version of that document *in the same Release as the present document*.

[1] 3GPP TR 21.905: "Vocabulary for 3GPP Specifications".

[2] 3GPP TR 36.903: " Evolved Universal Terrestrial Radio Access (E-UTRA) and Evolved Universal Terrestrial Radio Access Network (E-UTRAN); Derivation of test tolerances for Radio Resource Management (RRM) conformance tests".

[3] 3GPP TS 36.904: " Evolved Universal Terrestrial Radio Access (E-UTRA) and Evolved Universal Terrestrial Radio Access Network (E-UTRAN); Derivation of test tolerances for User Equipment (UE) radio reception conformance tests".

[4] ETSI ETR 273-1-2: "Improvement of radiated methods of measurement (using test sites) and evaluation of the corresponding measurement uncertainties; Part 1: Uncertainties in the measurement of mobile radio equipment characteristics; Sub-part 2: Examples and annexes".

[5] 3GPP TS 36.521-1: "User Equipment (UE) conformance specification, Radio transmission and reception Part 1: conformance testing".

[6] 3GPP TS 38.521-1: "NR; User Equipment (UE) conformance specification; Radio transmission and reception; Part 1: Range 1 Standalone".

[7] 3GPP TS 38.521-2: "NR; User Equipment (UE) conformance specification; Radio transmission and reception; Part 2: Range 2 Standalone".

[8] 3GPP TS 38.521-3: "NR; User Equipment (UE) conformance specification; Radio transmission and reception; Part 3: NR interworking between NR range1 + NR range2; and between NR and LTE".

[9] 3GPP TS 38.521-4: "NR; User Equipment (UE) conformance specification; Radio transmission and reception; Part 4: Performance requirements".

[10] 3GPP TS 38.533: "NR; User Equipment (UE) conformance specification; Radio Resource Management (RRM)".

3 Definitions, symbols and abbreviations

3.1 Definitions

For the purposes of the present document, the terms and definitions given in 3GPP TR 21.905 [1] and the following apply. A term defined in the present document takes precedence over the definition of the same term, if any, in 3GPP TR 21.905 [1].

Editor's note: intended to capture definitions

3.2 Symbols

For the purposes of the present document, the following symbols apply:

Editor's note: intended to capture symbols

3.3 Abbreviations

For the purposes of the present document, the abbreviations given in 3GPP TR 21.905 [1] and the following apply. An abbreviation defined in the present document takes precedence over the definition of the same abbreviation, if any, in 3GPP TR 21.905 [1].

Editor's note: intended to capture abbreviations.

4 General Principles

4.1 Principle of Superposition

For multi-cell tests there are several cells each generating various Physical channels. In general cells are combined along with AWGN, so the signal and noise seen by the UE may be determined by more than one cell.

Since several cells may contribute towards the overall power applied to the UE, a number of test system uncertainties affect the signal and noise seen by the UE. The aim of the superposition method is to vary each controllable parameter of the test system separately, and to establish its effect on the critical parameters as seen by the UE receiver. The superposition principle then allows the effect of each test system uncertainty to be added, to calculate the overall effect.

The contributing test system uncertainties shall form a minimum set for the superposition principle to be applicable.

4.2 Sensitivity analysis

A change in any one channel level or channel ratio generated at source does not necessarily have a 1:1 effect at the UE. The effect of each controllable parameter of the test system on the critical parameters as seen by the UE receiver shall therefore be established. As a consequence of the sensitivity scaling factors not necessarily being unity, the test system uncertainties cannot be directly applied as test tolerances to the critical parameters as seen by the UE.

EXAMPLE: In many of the tests described, the $\hat{E}s / I_{ot}$ is one of the critical parameters at the UE. Scaling factors are used to model the sensitivity of the $\hat{E}s / I_{ot}$ to each test system uncertainty. When the scaling factors have been determined, the superposition principle then allows the effect of each test system uncertainty to be added, to give the overall variability in the critical parameters as seen at the UE.

There are often constraints on several parameters at the UE. The aim of the sensitivity analysis, together with the acceptable test system uncertainties, is to ensure that the variability in each of these parameters is controlled within the limits necessary for the specification to apply. The test has then been conducted under valid conditions.

4.3 Statistical combination of uncertainties

The acceptable uncertainties of the test system are specified as the measurement uncertainty tolerance interval for a specific measurement that contains 95 % of the performance of a population of test equipment. In the RRM and UE radio transmission and reception conformance tests covered by the present document, the Test System shall enable the stimulus signals in the test case to be adjusted to within the specified range, with an uncertainty not exceeding the specified values.

The method given in the present document combines the acceptable uncertainties of the test system, to give the overall variability in the critical parameters as seen at the UE. Since the process does not add any new uncertainties, the method of combination should be chosen to maintain the same tolerance interval for the combined uncertainty as is already specified for the contributing test system uncertainties.

The basic principle for combining uncertainties is in accordance with ETR 273-1-2 [4]. In summary, the process requires 3 steps:

a) Express the value of each contributing uncertainty as a one standard deviation figure, from knowledge of its numeric value and its distribution.

b) Combine all the one standard deviation figures as root-sum-squares, to give the one standard deviation value for the combined uncertainty.

c) Expand the combined uncertainty by a coverage factor, according to the tolerance interval required.

Provided that the contributing uncertainties have already been obtained using this method, using a coverage factor of 2, further stages of combination can be achieved by performing step b) alone, since steps a) and c) simply divide by 2 and multiply by 2 respectively.

The root-sum-squares method is therefore used to maintain the same tolerance interval for the combined uncertainty as is already specified for the contributing test system uncertainties. In some cases where correlation between contributing uncertainties has an adverse effect, the method is modified in accordance with clause 4.4.5 of the present document.

In each analysis, the uncertainties are assumed to be uncorrelated, and are added result root-sum-square unless otherwise stated.

The combination of uncertainties is performed using dB values for simplicity. It has been shown that using dB uncertainty values gives a slightly worse combined uncertainty result than using linear values for the uncertainties. The analysis method therefore errs on the safe side.

4.4 Correlation between uncertainties

The statistical (root-sum-square) addition of uncertainties is based on the assumption that the uncertainties are independent of each other. For realisable test systems, the uncertainties may not be fully independent. The validity of the method used to add uncertainties depends on both the type of correlation and on the way in which the uncertainties affect the test requirements.

Clauses 4.4.1 to 4.4.3 give examples to illustrate different types of correlation.

Clauses 4.4.4 to 4.4.7 show how the scenarios applicable to multi-cell RRM tests are treated.

4.4.1 Uncorrelated uncertainties

The graph shows an example of two test system uncertainties, A and B, which affect a test requirement. Each sample from a population of test systems has a specific value of error in parameter A, and a specific value of error in parameter B. Each dot on the graph represents a sample from a population of test systems, and is plotted according to its error values for parameters A and B.

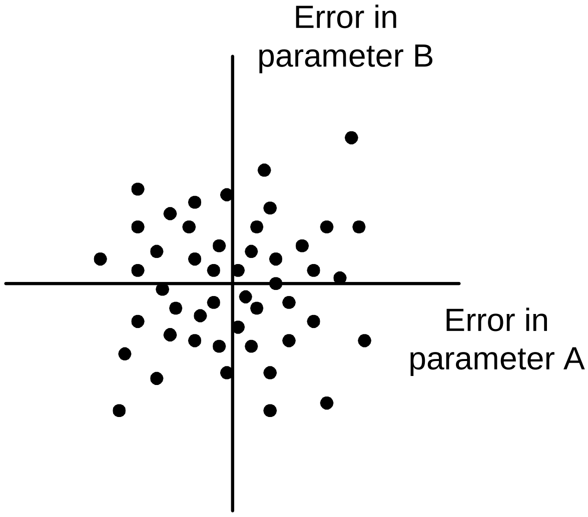

Figure 4.4.1-1: Example of two test system uncertainties affecting a test requirement

It can be seen that a positive value of error in parameter A, for example, is equally likely to occur with either a positive or a negative value of error in parameter B. This is expected when two parameters are uncorrelated, such as two uncertainties which arise from different and unrelated parts of the test system.

4.4.2 Positively correlated uncertainties

The graph shows an example of two test system uncertainties, A and B, which affect a test requirement. Each sample from a population of test systems has a specific value of error in parameter A, and a specific value of error in parameter B. Each dot on the graph represents a sample from a population of test systems, and is plotted according to its error values for parameters A and B.

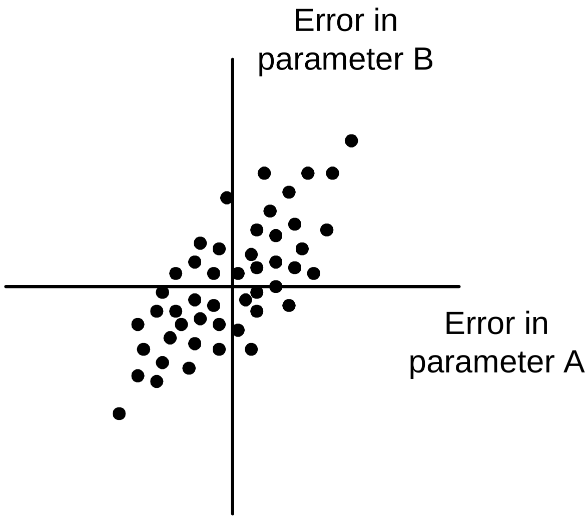

Figure 4.4.2-1: Example of two test system uncertainties affecting a test requirement

It can be seen that a positive value of error in parameter A, for example, is more likely to occur with a positive value of error in parameter B and less likely to occur with a negative value of error in parameter B. This can occur when the two uncertainties arise from similar parts of the test system, or when one component of the uncertainty affects both parameters in a similar way.

In an extreme case, if the error in parameter A and the error in parameter B came from the same sources of uncertainty, and no others, the dots would lie on a straight line of slope +1.

4.4.3 Negatively correlated uncertainties

The graph shows an example of two test system uncertainties, A and B, which affect a test condition. Each sample from a population of test systems has a specific value of error in parameter A, and a specific value of error in parameter B. Each dot on the graph represents a sample from a population of test systems, and is plotted according to its error values for parameters A and B.

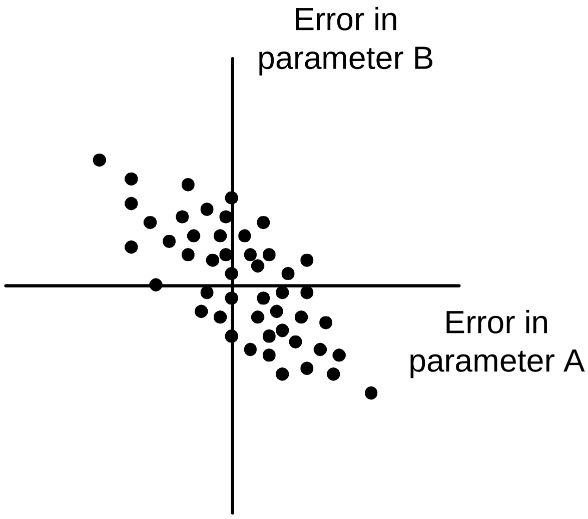

Figure 4.4.3-1: Example of two test system uncertainties affecting a test condition

It can be seen that a positive value of error in parameter A, for example, is more likely to occur with a negative value of error in parameter B and less likely to occur with a positive value of error in parameter B. This effect can theoretically occur, and is included for completeness, but is unlikely in a practical test system.

4.4.4 Treatment of uncorrelated uncertainties

If two uncertainties are uncorrelated, they are added statistically in the analysis. Provided that each uncertainty is already expressed as an expanded uncertainty with coverage factor 2, the contributing uncertainties are added root-sum-squares to give a combined uncertainty which also has coverage factor 2, and the 95% tolerance interval is maintained.

This is the default assumption.

4.4.5 Treatment of positively correlated uncertainties with adverse effect

If two test system uncertainties are positively correlated, and if they affect the value of a critical parameter in the same direction, the combined effect may be greater than predicted by adding the contributing uncertainties root-sum-squares.

In this scenario the two uncertainties are added worst-case in the analysis. Provided that each uncertainty is already expressed as an expanded uncertainty with coverage factor 2, the combined uncertainty will cover a 95% tolerance interval even when the two contributing uncertainties are fully correlated. If the two contributing uncertainties are less than fully correlated, the combined uncertainty will cover a tolerance interval greater than 95%.

4.4.6 Treatment of positively correlated uncertainties with beneficial effect

If two test system uncertainties are positively correlated, and if they affect the value of a critical parameter in opposite directions, the combined effect will be less than predicted by adding the contributing uncertainties root-sum-squares.

In this scenario the two uncertainties are added statistically in the analysis. Provided that each uncertainty is already expressed as an expanded uncertainty with coverage factor 2, the combined uncertainty will cover a 95% tolerance interval when the two contributing uncertainties are uncorrelated. If the two contributing uncertainties are positively correlated, the combined uncertainty will cover a tolerance interval greater than 95%.

4.4.7 Treatment of negatively correlated uncertainties

Negatively correlated uncertainties are excluded by the assumptions. This has been agreed as an acceptable restriction on practical test systems, as the mechanisms which produce correlation generally arise from similarities between two parts of the test system, and therefore produce positive correlation.

5 Determination of Test System Uncertainties

5.1 General

The uncertainty of a test system when making measurements reduces the ability of the test system to distinguish between conformant and non-conformant test subjects. The aim is therefore to minimise uncertainty, subject to a number of practical constraints:

a) A vendor's test system should be reproducible in the required quantities.

b) A choice of test systems should be available from different vendors.

c) The uncertainties should allow reasonable freedom of test system implementation

d) The test system can be run automatically

e) The test system may include several radio access technologies

f) It should be possible to maintain calibration of deployed test systems over reasonable spans of time and environmental conditions

In practice therefore within 3GPP the acceptable uncertainty of the test system is the smallest value that can be agreed between the test system vendors represented, consistent with the above constraints. The uncertainty will not therefore be as low as could be achieved, for example, by a national standards laboratory.

5.2 Uncertainty figures

The actual figures for the acceptable uncertainty of a test system are defined in [Annex TBD of 38.521-1, Annex TBD of 38.521-2, Annex TBD of 38.521-3, Annex TBD of TS 38.521-4 and Annex TBD of TS 38.533]. To avoid maintenance issues with figures in separate specifications, the uncertainties are not formally defined within the present document, but informative guidelines are provided in Annex B to Annex E of the present document.

6 Determination of Test Tolerances

6.1 General

The general principles given in the present document are applied to each test case, according to the applicable uncertainties and requirements to obtain a correct verdict.

The test cases which have been analysed to determine Test Tolerances are included the present document as .zip files. The name of the zip file indicates the specification and the test cases covered.

Annex A gives the rationale for their inclusion.

7 Grouping of test cases defined in TS 38.521-4

Editor's note: intended to capture grouping of demodulation test cases.

8 Grouping of test cases defined in TS 38.533

Editor's note: intended to capture grouping of RRM test cases.

Annex A: Derivation documents for test tolerance

The documents (and spreadsheets where applicable) used to derive the test tolerances for each test case are included in the present document as zip files.

The aim is to provide a reference to completed test cases, so that test tolerances for similar test cases can be derived on a common basis. The information on test case grouping in section 7 and 8 can be used to identify similarities.

Editor’s Note: This subclause is reserved for future Demodulation and RRM test cases. No .zip file is included in current version.

Annex B: Acceptable uncertainty of test system for test cases defined in TS 38.521-2 for radiative testing

This annex contains suggested uncertainties for each test case in TS 38.521-2.

B.1 Uncertainty budget calculation principle

B.1.1 Uncertainty budget calculation principle for DFF

The uncertainty tables should be presented with two stages:

- Stage 1: the calibration of the absolute level of the DUT measurement results is performed by means of using a calibration antenna whose absolute gain is known at the frequencies of measurement
- Stage 2: the actual measurement with the DUT as either the transmitter or receiver is performed.

The MU budget should comprise of a minimum 5 headings:

1) The uncertainty source,
2) Uncertainty value,
3) Distribution of the probability,
4) Divisor based on distribution shape,
5) Calculated standard uncertainty (based on uncertainty value and divisor).

B.1.2 Uncertainty budget calculation principle for IFF

The same as defined in B.1.1.

B.1.3 Uncertainty budget calculation principle for NFTF

The same as defined in B.1.1 with the exception of Stage 2, only the measurement of the DUT transmitter is performed.

B.2 Measurement error contribution descriptions

B.2.1 Measurement error contribution descriptions for DFF

B.2.1.1 Positioning misalignment

This contribution originates from the misalignment of the testing direction and the beam peak direction of the measurement antenna due to imperfect rotation operation. The pointing misalignment may happen in both azimuth and vertical directions and the effect of the misalignment depends highly on the beam width of the beam under test. The same level of misalignment results in a larger measurement error for a narrower beam.

B.2.1.2 Measure distance uncertainty

The cause of this uncertainty contributor is due to the reduction of distance between the measurement antenna and the DUT. If the distance of separation is $2D^2$/lambda based on D being the entire device size, then the phase variation is 22.5deg. Whether this is the minimum acceptable criteria of phase taper over the entire DUT is FFS. Any reduction in the distance of separation increases the phase variation and creates an error which is DUT dependant. Determination of limit of the error is FFS.

B.2.1.3 Quality of quiet zone

The quality of the quiet zone procedure characterizes the quiet zone performance of the anechoic chamber, specifically the effect of reflections within the anechoic chamber including any positioners and support structures. The MU term additionally includes the amplitude variations effect of offsetting the directive antenna array inside a DUT from the centre of the quiet zone as well as the directivity MU, i.e., the variation of antenna gains in the different direct line-of-sight links. An additional MU term related to phase variation and phase ripple effects which depends on measurement distance is FFS, this might require an augmentation of the quality of the quiet zone validation procedure.

B.2.1.4 Mismatch

Mismatch uncertainty occurs when;

- Changing the signal path between the measurement and calibration procedure
- Evaluating the insertion loss of a signal path

The mismatch uncertainty for a system consisting of a generator, a load and a component in between is defined as

$$\text{Mismatch contribution (standard deviation)} = \frac{|\Gamma_{generator}|\cdot|\Gamma_{load}|\cdot|S_{21}|\cdot|S_{12}|\cdot 100}{\sqrt{2}\cdot 11.5}\ \text{dB},$$

Where Γ denotes the reflection coefficient and S_{21} is the transmission coefficient, both in linear voltage ratios.

For a cascade of several components, the interactions between all components have to be evaluated. For example, for four devices in a row (shown in Figure B.2.1.4-1) the following contributions have to be accounted for: AB, BC, CD, ABC, BCD, ABCD. The term ABCD represents the interaction between A and D (generator and load) with the components B and C in between.

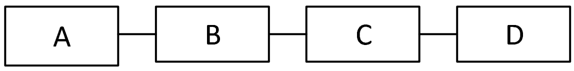

Figure B.2.1.4-1: Cascade of components

The combined mismatch uncertainty is given by the root sum square of the individual contributions:

$$combined\ mismatch\ uncertainty = \sqrt{(AB)^2 + (BC)^2 + (CD)^2 + (ABC)^2 + (BCD)^2 + (ABCD)^2}$$

In an optimized test procedure, the overall mismatch uncertainty is smaller when matching pairs of mismatches exist in the calibration and measurement stage since these pairs cancel each other out. Figure B.2.1.4-2 displays a calibration setup, where device D is replaced by device F. The mismatch contributions for this path are AB, BC, CE, ABC, BCE and ABCE. For a result based on the measurement and calibration stage, the mismatch contributions AB, BC, and ABC are matching pairs as they occur both in the measurement and calibration stage. Thus, they can be eliminated [11], and the system mismatch uncertainty is obtained as $\sqrt{(CD)^2 + (CE)^2 + (BCD)^2 + (BCE)^2 + (ABCD)^2 + (ABCE)^2}$

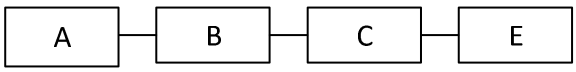

Figure B.2.1.4-2: Sketch of a calibration path

In the following, an example mismatch uncertainty calculation for a TX/RX patch from the measurement equipment to the measurement antenna is performed for a frequency of 43.5GHz. The example path under investigation consists of four SPDT switches, one SP6T switch and one DPDT switch and microwave cable interconnects with PC2.4 mm connectors. The attenuation and reflectance of typical components suitable for frequencies ranging up to 43.5 GHz have been considered in the calculation of the mismatch uncertainty.

Figure B1.1.4.4-3 shows a sample system setup for an EIRP/EIS test case with rather simple complexity of the switch box similar to a current sub 6GHz test setup. It should be noted that the switch unit is significantly less complex than a state-of-the-art switch unit currently used for conformance tests.

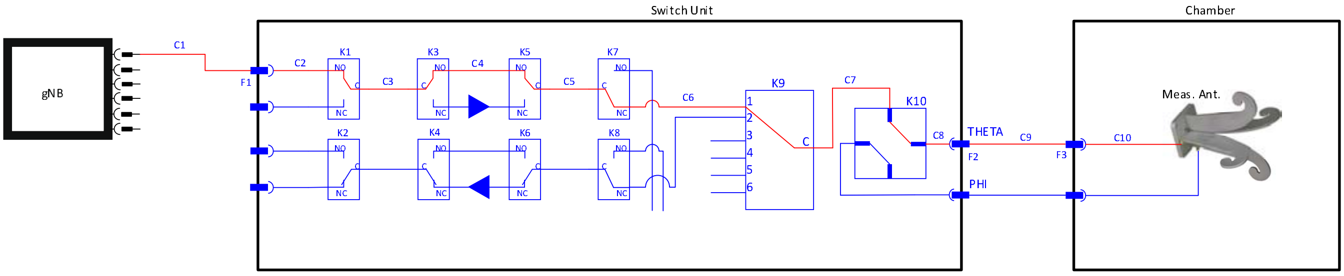

Figure B.2.1.4-3: Block Diagram of an EIRP/EIS test case with components from the gNB to the antenna (only portion of switch unit shown)

Table B.2.1.4-1: comprises the reflection and transmission properties of the components of the example path at a frequency of 43.5 GHz

Device / Component	VSWR	Transmission (dB)	Identifier in Figure B.2.1.4-3	Additional Comment/ Assumption
System Simulator	3.5		gNB	
Cable	1.5	-5.38	C1	Length: 1.5m Loss: 3.59dB/m
Cable	1.5	-0.61	C2, C3, C4, C5, C6, C7, C8	Length: 0.17m Loss: 3.59dB/m
Cable	1.5	-7.18	C9, C10	Length: 2.0m Loss: 3.59dB/m
Feedthrough	1.3	-0.66	F1, F2, F3	
SPDT switch	1.9	-1.10	K1, K3, K5, K7	
SP6T switch	2.2	-1.20	K9	
Transfer switch	2.0	-1.10	K10	
Antenna	2.0		Meas. Ant.	

The calculation of the overall mismatch uncertainty for a frequency of 43.5 GHz results in a value of 2.7 dB for the standard deviation, i.e., the expanded uncertainty is 5.3 dB.

Figure B.2.1.4-4 depicts a possible calibration for a part of the setup.

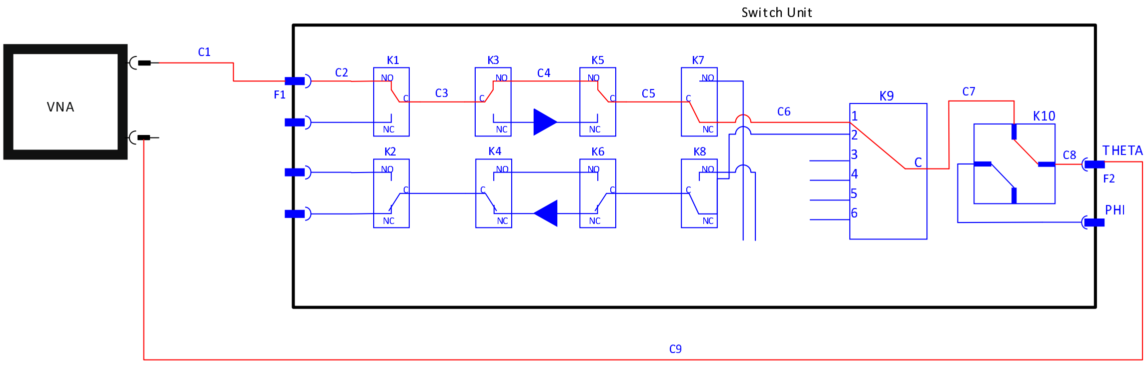

Figure B.2.1.4-4: Block Diagram of the calibration stage

For the VNA a return loss of 30 dB is assumed after a full two-port calibration. The calculation of the system mismatch uncertainty applying the elimination of matching pairs results in a value of 1.0 dB (standard deviation) with an expanded value of 1.9 dB.

Since the overall mismatch uncertainty value is already a standard deviation, which is RSS of values divided by the divisor (√2), the overall mismatch uncertainty value should be divided by actual divisor 1 when calculating total mismatch.

B.2.1.5 Standing Wave Between the DUT and measurement antenna

This uncertainty term is related to the amplitude ripple coming from the standing waves between the DUT and measurement antenna. If this term is not considered to be negligible one method to obtain this value is to slide the DUT lambda/4 towards the measurement antenna while measuring the amplitude. The uncertainty term can be derived by performing the standard deviation on the results.

B.2.1.6 Uncertainty of the RF power measurement equipment

The receiving device is used to measure the received signal level in the EIRP tests as an absolute level. These receiving devices are spectrum analysers, communication analysers, or power meters. The uncertainty value will be indicated in the manufacturer's data sheet. It needs to be ensured that appropriate manufacturer's uncertainty contributions are specified for the settings used such as bandwidth and absolute level. If a power meter is used zero offset, zero drift and measurement noise need to be included.

B.2.1.7 Phase curvature

This contribution originates from the finite far field measurement distance, which causes phase curvature across the antenna of UE/reference antenna. At a measurement distance of $2D^2$/lambda the phase curvature is 22.5 degrees. The impact of this factor is FFS.

B.2.1.8 Amplifier uncertainties

Any components in the setup can potentially introduce measurement uncertainty. It is then needed to determine the uncertainty contributors associated with the use of such components. For the case of external amplifiers, the following uncertainties should be considered but the applicability is contingent to the measurement implementation and calibration procedure.

- Stability
    - An uncertainty contribution comes from the output level stability of the amplifier. Even if the amplifier is part of the system for both measurement and calibration, the uncertainty due to the stability shall be considered. This uncertainty can be either measured or determined by the manufacturers' data sheet for the operating conditions in which the system will be required to operate.
- Linearity
    - An uncertainty contribution comes from the linearity of the amplifier since in most cases calibration and measurements are performed at two different input/output power levels. This uncertainty can be either measured or determined by the manufacturers' data sheet.
- Noise Figure
    - When the signal goes into an amplifier, noise is added so that the SNR at the output is reduced with regard to the SNR of the signal at the input. This added noise introduces error on the signal which affects the Error Rate of the receiver thus the EVM (Error Vector Magnitude). An uncertainty can be calculated through the following formula:

$$\varepsilon_{EVM} = 20\log_{10}\left(1 + 10^{\frac{-SNR}{20}}\right)$$

    - Where SNR is the signal to noise ratio in dB at the signal level used during the sensitivity measurement.
- Mismatch
    - If the external amplifier is used for both stages, measurement and calibration the uncertainty contribution associated with it can be considered systematic and constant -> 0dB. If it is not the case, the mismatch uncertainty at its input and output shall be either measured or determined by the method described in [12].
- Gain

- If the external amplifier is used for both stages, measurement and calibration the uncertainty contribution associated with it can be considered systematic and constant -> 0dB. If it is not the case, this uncertainty shall be considered.

B.2.1.9 Random uncertainty

This contribution is used to account for all the unknown, unquantifiable, etc. uncertainties associated with the measurements.

Random uncertainty MU contributions are normally distributed. [Note: this is different from "Miscellaneous uncertainty" or "Residual uncertainty" which can include unknown systematic errors which may not be normally distributed.]

The random uncertainty term, by definition, cannot be measured, or even isolated completely. However, past system definitions provide an empirical basis for a value. Current LTE SISO OTA measurements have random uncertainty contributions of ~0.2dB. A value of 0.5dB is suggested due to increased sensitivity to random effects in more complex, higher frequency NR test systems.

B.2.1.10 Influence of the XPD

This factor takes into account the uncertainty caused due to the finite cross polar discrimination (XPD) between the two polarization ports of the measurement probe. The XPD of the probe antenna is TBD, as defined in antenna datasheet.

A typical probe antenna can have XPD of 30dB

For example if a linearly-polarized sine wave is input to the measurement antenna with a gradient of 45 degrees like the case in the following figure, then a signal level of V-antenna and H antenna are equal.

When we consider a leakage from V to H, or H to V, they can be described with the following equations.

$$ReceivedSignal@Ant(V) = A\sin(2\pi ft) + LeakageComponentFromH$$

$$\mathrm{ReceivedSignal@Ant(V)} = A \cdot sin(2\pi ft) + LeakageComponentFromH \quad (1)$$

$$\mathrm{ReceivedSignal@Ant(H)} = A \cdot sin(2\pi ft) + LeakageComponentFromV$$

$$ReceivedSignal@Ant(H) = A\sin(2\pi ft) + LeakageComponentFromV \quad (2)$$

Worst case can be assumed as the case that the phase of signal and leakage are same, and it can be shown as follows

$$LeakageComponentFromH = A \cdot sin(2\pi ft) \cdot 10^{\frac{XPD}{20}} \; LeakageComponentFromH = A\sin(2\pi ft) + 10^{\frac{XPD}{20}} \quad (3)$$

If we put equations (1) and (2) in (3), we get following 2 equations.

$$ReceivedSignal@Ant(V) = A\sin(2\pi ft) + LeakageComponentFromH$$

$$ReceivedSignal@Ant(V) = A\sin(2\pi ft) + LeakageComponentFromH$$

Difference of amplitude between the case that there is a leakage and not can be calculated as follows.

- Amplitude when there is not the leakage: A
- Amplitude when there is the leakage (Worst): $A\left(1 + 10^{\frac{XPD}{20}}\right) A \cdot \left(1 + 10^{\frac{XPD}{20}}\right)$

$$MUbyXPD = 20\log_{10}\left(\frac{A\left(1 + 10^{\frac{XPD}{20}}\right)}{A}\right) = 20\log_{10}\left(1 + 10^{\frac{XPD}{20}}\right)$$

For example, if the XPD = -30dB, the calculated value can be as follows.

$$MUbyXPD = 20\log_{10}\left(1 + 10^{\frac{-30}{20}}\right) = 0.27\ [dB]$$

B.2.1.11 Insertion loss Variation

This uncertainty contribution comes from introducing an additional cable which is not present for both the calibration and DUT measurement. If the cables remain the same for the calibration and DUT measurement, then the contribution should be set to zero.

If an additional cable is added for one part of the test, the insertion loss must be accounted for in the measurement results. If the insertion loss is measured the uncertainty contribution will be the combined uncertainty related to the insertion loss measurement. The insertion loss can also be taken from the datasheet and assumed to have a rectangular distribution.

B.2.1.12 RF leakage (from measurement antenna to receiver/transmitter)

This contribution denotes noise leaking in to connector and cable(s) between measurement antenna and receiving/transmitting equipment. The contribution also includes the noise leakage between the connector and cable(s) between reference antenna and transmitting equipment for the calibration phase.

B.2.1.13 Misalignment of positioning System

This contribution originates from uncertainty in sliding position and turn table angle/tilt accuracy. If the calibration antenna is aligned to the beam peak this contribution can be considered negligible and therefore set to zero.

B.2.1.14 Uncertainty of the Network Analyzer

This contribution originates from all uncertainties involved transmission magnitude measurement (including drift and frequency flatness) with a network analyser. The uncertainty value will be indicated in the manufacturer's data sheet. It needs to be ensured that appropriate manufacturer's uncertainty contribution is specified for the absolute levels measured.

B.2.1.15 Uncertainty of the absolute gain of the calibration antenna

The calibration antenna only appears in Stage 2. Therefore, the gain uncertainty has to be taken into account. This uncertainty will come from a calibration report with traceability to a National Metrology Institute with measurement uncertainty budgets generated following the guidelines outlined in internationally accepted standards.

B.2.1.16 Positioning and pointing misalignment between the reference antenna and the measurement antenna

This contribution originates from reference antenna alignment and pointing error. In this measurement if the maximum gain direction of the reference antenna and the transmitting antenna are aligned to each other, this contribution can be considered negligible and therefore set to zero.

B.2.1.17 gNB emulator uncertainty

gNB emulator is used to drive a signal to the horn antenna (via multiple external components such as a switch box, an amplifier and a circulator, etc.) in sensitivity tests either as an absolute level or as a relative level. Receiving device used is typically a UE/phablet/tablet/FWA. Generally there occurs uncertainty contribution from absolute level accuracy, non-linearity and frequency characteristic of the gNB emulator.

For practical reasons, in a case that a VNA is used as calibration equipment, gNB emulator is connected to the system after the calibration measurement (Stage 2) is performed by the VNA. Hence, the uncertainty on the absolute level of gNB emulator (transmitter device) cannot be assumed as systematic. This uncertainty should be calculated from the manufacturer's data in logs with a rectangular distribution, unless otherwise informed. Furthermore, the uncertainty of the non-linearity is included in the absolute level uncertainty.

B.2.1.18 Phase centre offset of calibration

Gain is defined at the phase centre of the antenna. If the phase centre of the calibration antenna is not aligned at the centre of the set up during the calibration, then there will be uncertainty related to the measurement distance.

The phase centre of a horn antenna moves with frequency along the taper length of the antenna therefore during the calibration the phase centre of all frequencies will not be aligned with the setup centre. The associated uncertainty term can be estimated using the following formula [15]:

$$\pm 20\log_{10}\left(\frac{d_m - d_p}{d_m}\right)$$

+/-20log((measurement distance – d)/measurement distance) [15]

Where d_m is the measurement distance and d_p is the maximum positional uncertainty. For a Horn antenna this is equal to 0.5 the length of the taper. This uncertainty is considered to have a rectangular distribution so the standard uncertainty is calculated by dividing the uncertainty by √3.

The same equation applies to log periodic antennas with d_m being 0.5 the length of the boom.

For a dipole antenna, given that the phase centre of the antenna is easily aligned with the centre of the set up the measurement uncertainty is zero.

If the calibration antenna (i.e. horn) is adjusted during the calibration to align the phase centre to the setup centre then this uncertainty term can be considered to be zero.

As an example a horn with a taper length of 50 mm, at 43.5 GHz and a measurement distance of 72.55 cm the uncertainty term is 0.62, with a rectangular distribution the standard uncertainty is 0.358 dB.

For DFF systems this uncertainty contribution must be included.

B.2.1.19 Quality of quiet zone for calibration process

During the calibration process the calibration antenna will be placed at the centre of the quiet zone. Therefore, only point P1 from the procedure outlined in B.2.1.3 needs to be considered for the quality of the quiet zone validation measurement.

For gain calibrations, the standard uncertainty of the EIRP results obtained following the method outlined in 2.10 shall be used. For efficiency calibrations, the standard uncertainty of the TRP result obtained following the method outlined in 2.9 shall be used.

B.2.1.20 Standing wave between reference calibration antenna and measurement antenna

This term comes from the amplitude ripple caused by the standing waves between the reference antenna and measurement antenna. This value can be captured by sliding (lambda/4) the reference antenna towards the measurement antenna as the standing waves go in and out of phase causing a ripple in amplitude. The uncertainty term can be derived by performing the standard deviation on the results.

B.2.1.21 Influence of the calibration antenna feed cable (Flexing cables, adapters, attenuators, connector repeatability)

During the calibration measurement a cable (adapters, attenuators) is used to feed the calibration antenna. This uncertainty captures any influence the cable may have on the measurements result. This term can be assessed by repeating measurements while flexing the cables and rotary joints and using the largest difference between the results as the uncertainty. For some calibration test configurations this uncertainty can be considered to be zero.

B.2.1.22 Influence of TRP measurement grid

This contributor describes the uncertainty of the measured TRP value due to the finite number of measurement grid points.

B.2.1.23 Influence of beam peak search grid

This contributor describes the uncertainty of absolute TX power beam peak measurements, e.g., EIRP in beam peak direction, due to the finite number of measurement points in the beam peak search grid.

B.2.1.24 Mean error related to TRP calculation applying sin(θ)-weighting

When calculating TRP making use of sin(θ)-weighting of constant step size data, a mean error shall be taken into account. The value of this contributor depends on the number of measurement grid points.

No mean error has to be taken into account for constant density approach (using the charged particle or the golden spiral implementation) for non-sparse antenna arrays.

This measurement uncertainty contributor represents a systematic uncertainty and must not be root sum squared with contributors described by standard deviation.

B.2.2 Measurement error contribution descriptions for IFF

B.2.2.1 Positioning misalignment

See B.2.1.1.

B.2.2.2 Measure distance uncertainty

See B.2.1.2. For IFF1 this can be considered to be zero.

B.2.2.3 Quality of Quiet Zone

See B.2.1.3.

B.2.2.4 Mismatch

See B.2.1.4.

B.2.2.5 Standing wave between DUT and measurement antenna

See B.2.1.5.

B.2.2.6 Uncertainty of the RF power measurement equipment

See B.2.1.6.

B.2.2.7 Phase Curvature

See B.2.1.7. For IFF1 this can be considered to be zero.

B.2.2.8 Amplifier Uncertainties

See B.2.1.8.

B.2.2.9 Random uncertainty

See B.2.1.9.

B.2.2.10 Influence of XPD

See B.2.1.10.

B.2.2.11 Insertion Loss Variation

See B.2.1.11.

B.2.2.12 RF leakage (from measurement antenna to receiver/transmitter)

See B.2.1.12.

B.2.2.13 Misalignment of positioning system

See B.2.1.13.

B.2.2.14 Uncertainty of the Network Analyzer

See B.2.1.14.

B.2.2.15 Uncertainty of the absolute gain of the calibration antenna

See B.2.1.15.

B.2.2.16 Positioning and pointing misalignment between the reference antenna and the measurement antenna

See B.2.1.16.

B.2.2.17 gNB emulator uncertainty

See B.2.1.17.

B.2.2.18 Phase centre offset of calibration

See B.2.1.18. For IFF1 this can be considered to be zero.

B.2.2.19 Quality of the Quiet Zone for Calibration Process

See B.2.1.19.

B.2.2.20 Standing wave between reference calibration antenna and measurement antenna

See B.2.1.20.

B.2.2.21 Influence of the calibration antenna feed cable (Flexing cables, adapters, attenuators, connector repeatability)

See B.2.1.21.

B.2.2.22 Influence of TRP measurement grid

See B.2.1.22.

B.2.2.23 Influence of beam peak search grid

See B.2.1.23.

B.2.2.24 Mean error related to TRP calculation applying sin(θ)-weighting

See B.2.1.24.

B.2.3 Measurement error contribution descriptions for NFTF

B.2.3.1 Axes Alignment

Includes the following mechanical alignment errors:

- The uncertainty related with the lateral displacement between the horizontal and vertical axes of the DUT positioner.
- The differences from 90° of the angle between the horizontal and vertical axes.

- The horizontal mis-pointing of the horizontal axis to the probe reference point for Theta=0°.

These mechanical errors can result in sampling the field on a non-ideal sphere. This uncertainty can be considered to have a normal distribution.

B.2.3.2 Measurement Distance uncertainty

See B.2.1.2.

B.2.3.3 Quality of the Quiet Zone

See B.2.1.3.

B.2.3.4 Mismatch

See B.2.1.4.

B.2.3.5 Multiple Reflections: Coupling Measurement Antenna and DUT

The multiple reflections occur when a portion of the transmitted signal is reflected form the receiving antenna back to the transmitting antenna and re-reflected by the transmitting antenna back to the receiving antenna. This uncertainty can be determined by multiple measurements of the DUT when at different distance from the probes. This uncertainty is assumed to have a U-shaped distribution.

B.2.3.6 Uncertainty of the RF power measurement equipment

See B.2.1.6.

B.2.3.7 Phase curvature

See B.2.1.7.

B.2.3.8 Amplifier uncertainties

See B.2.1.8.

B.2.3.9 Random uncertainty

See B.2.1.9.

B.2.3.10 Influence of the XPD

Refer to B.2.1.10. If the Probe Polarization Amplitude and Phase is measured and corrected for then this uncertainty term can be considered to be zero.

B.2.3.11 NF to FF truncation

The measured near field is expanded using a finite set of spherical modes. The number of modes is linked to number of samples. The filtering effect generated by the finite number of modes can improve measurement results by removing signals from outside the physical area of the DUT. Care must be taken in order to make sure the removed signals are not from the DUT itself. This term also includes the uncertainty related to the scan area truncation. This uncertainty is usually negligible. This uncertainty is assumed to have a normal distribution.

B.2.3.12 Probe Polarization Amplitude and Phase

The amplitude and phase of the probe polarization coefficients should be measured. This uncertainty is assumed to have a normal distribution.

B.2.3.13 Probe Array Uniformity (for multi-probe systems only)

This is the uncertainty due to the fact that different probes are used for each physical position. Different probes have different radiation patterns. Generally, the probe array is calibrated so that the uniformity of the probes is achieved. This uncertainty term must be considered if the amplitude and phase of each probe is not identical or corrected for. This uncertainty is assumed to have a normal distribution

B.2.3.14 Uncertainty of the Network Analyzer

See B.2.1.14.

B.2.3.15 Uncertainty of the absolute gain of the calibration antenna

See B.2.1.15.

B.2.3.16 Phase Recovery Non-Linearity over signal bandwidth

This uncertainty originates from the non-linearity of the phase recovery for wide band signal. The phase recovery can be due to either phase non-linearity of the receiver and/or the DUT itself. The method to quantify the non-linarites is FFS.

B.2.3.17 Probe Pattern Effect

The probe/s pattern/s is assumed to be known so that the DUT measurement in near field can be corrected when performing the near field to far field transform. If the probe pattern is known, then the uncertainty term is zero. There is no direct dependence between the DUT pattern and the probe pattern in near field measurements. This uncertainty is assumed to have a normal distribution.

B.2.3.18 Phase centre offset of calibration

See B.2.1.18.

B.2.3.19 Quality of the Quiet Zone for Calibration Process

See B.2.1.19.

B.2.3.20 Phase Drift and Noise

This uncertainty is due to the noise level and drift of the test range and should be determined or measured at the DUT location. The noise level is usually measured with a Spectrum Analyzer. This uncertainty is assumed to have a normal distribution.

B.2.3.21 Mismatch in the connection of the calibration antenna

See B.2.1.4.

B.2.3.22 Influence of TRP measurement grid

See B.2.1.22.

B.2.2.23 Influence of beam peak search grid

See B.2.1.23.

B.2.2.24 Mean error related to TRP calculation applying sin(θ)-weighting

See B.2.1.24.

B.2.3.25 Leakage and Crosstalk

This uncertainty can be addressed by measurements on the actual system setup. The leakage and crosstalk cannot be separated from the random amplitude and phase errors so that the relative importance should be determined. This uncertainty is assumed to have a normal distribution.

B.3 UE maximum output power

Following tables summarize the MU threshold for EIRP and TRP measurements for UE maximum output power. The origin MU values for different test setups with varies parameters can be found in following subclauses.

Table B.3-1: MU threshold for EIRP measurement for UE maximum output power

Frequency	MBW	Power	Aperture size	MU value
22.65GHz <= f <= 31.1GHz	BW <= 400MHz	P = Max Output Power	D <= 5cm	FFS
			5cm < D <= 15cm	FFS
31.1GHz < f <= 45.1GHz			D <= 5cm	FFS
			5cm < D <= 15cm	FFS

Table B.3-2: MU threshold for TRP measurement for UE maximum output power

FFS

B.3.1 Uncertainty budget format and assessment for DFF

The uncertainty contributions that may impact the overall MU value are listed in Table B.3.1-1.

Table B.3.1-1: Uncertainty contributions for EIRP and TRP measurement

UID	Description of uncertainty contribution	Details in annex
Stage 2: DUT measurement		
1	Positioning misalignment	B.2.1.1
2	Measure distance uncertainty	B.2.1.2
3	Quality of quiet zone	B.2.1.3
4	Mismatch	B.2.1.4
5	Standing Wave Between the DUT and measurement antenna	B.2.1.5
6	Uncertainty of the RF power measurement equipment	B.2.1.6
7	Phase curvature	B.2.1.7
8	Amplifier uncertainties	B.2.1.8
9	Random uncertainty	B.2.1.9
10	Influence of the XPD	B.2.1.10
11	Insertion Loss Variation	B.2.1.11
12	RF leakage (from measurement antenna to the receiver/transmitter)	B.2.1.12
13	Influence of TRP measurement grid	B.2.1.22
14	Influence of beam peak search grid	B.2.1.23
Stage 1: Calibration measurement		
15	Mismatch	B.2.1.4
16	Amplifier uncertainties	B.2.1.8
17	Misalignment of positioning System	B.2.1.13
18	Uncertainty of the Network Analyzer	B.2.1.14
19	Uncertainty of the absolute gain of the calibration antenna	B.2.1.15
20	Positioning and pointing misalignment between the reference antenna and the measurement antenna	B.2.1.16
21	Phase centre offset of calibration antenna	B.2.1.18
22	Quality of quiet zone for calibration process	B.2.1.19
23	Standing wave between reference calibration antenna and measurement antenna	B.2.1.20
24	Influence of the calibration antenna feed cable	B.2.1.21
Systematic uncertainties		
25	Mean error related to TRP calculation applying sin(θ)-weighting	B.2.1.24

The uncertainty assessment tables are organized as follows:

- For the purpose of uncertainty assessment, the radiating antenna aperture of the DUT is denoted as D

- The uncertainty assessment has been derived for the case of D = [5 cm], f = {22.65GHz, 31.1GHz, 45.1GHz}, P = [maximum output power].

- The uncertainty assessment for EIRP and TRP is provided in Table B.3.1-2.

Table B.3.1-2: Uncertainty assessment for EIRP and TRP measurement (f=TBD, D=TBD)

UID	Uncertainty source	Uncertainty value	Distribution of the probability	Divisor	Standard uncertainty (σ) [dB]
Stage 2: DUT measurement					
1	Positioning misalignment				
2	Measure distance uncertainty				
3	Quality of quiet zone (NOTE 2)				
4	Mismatch (NOTE 3)				
5	Standing Wave Between the DUT and measurement antenna				
6	Uncertainty of the RF power measurement equipment (NOTE 4)				
7	Phase curvature				
8	Amplifier uncertainties				
9	Random uncertainty				
10	Influence of the XPD				
11	Insertion Loss Variation				
12	RF leakage (from measurement antenna to the receiver/transmitter)				
13	Influence of TRP measurement grid (NOTE 5)	0.25	Actual	1	0.25
14	Influence of beam peak search grid (NOTE 6)	0.5	Actual	1	0.5
Stage 1: Calibration measurement					
15	Mismatch				
16	Amplifier uncertainties				
17	Misalignment of positioning System				
18	Uncertainty of the Network Analyzer				
19	Uncertainty of the absolute gain of the calibration antenna				
20	Positioning and pointing misalignment between the reference antenna and the measurement antenna				
21	Phase centre offset of calibration antenna				
22	Quality of quiet zone for calibration process (NOTE 2)				
23	Standing wave between reference calibration antenna and measurement antenna				
24	Influence of the calibration antenna feed cable				
	Systematic uncertainties (NOTE 7)				**Value**
25	Mean error for constant step size grid (NOTE 5)				0.34
Total measurement uncertainty					**Value**
EIRP Expanded uncertainty (1.96σ - confidence interval of 95 %) [dB]					
TRP Expanded uncertainty (1.96σ - confidence interval of 95 %) [dB]					

NOTE 1: The impact of phase variation on EIRP is FFS.
NOTE 2: The quality of quiet zone is different for EIRP and TRP. For TRP, the standard uncertainty is FFS; for EIRP, the standard uncertainty of quiet zone is FFS.
NOTE 3: The analysis was done only for the case of operating at max output power, in-band, non-CA.
NOTE 4: The assessment assumes maximum DUT output power.
NOTE 5: This contributor shall only be considered for TRP measurements.
NOTE 6: This contributor shall only be considered for EIRP measurements.
NOTE 7: In order to obtain the total measurement uncertainty, systematic uncertainties have to be added to the expanded root sum square of the standard deviations of the Stage 1 and Stage 2 contributors.

B.3.2 Uncertainty budget format and assessment for IFF

The uncertainty contributions that may impact the overall MU value are listed in Table B.3.2-1.

Table B.3.2-1: Uncertainty contributions for EIRP and TRP measurement

UID	Description of uncertainty contribution	Details in annex
Stage 2: DUT measurement		
1	Positioning misalignment	B.2.2.1
2	Measure distance uncertainty	B.2.2.2
3	Quality of Quiet Zone	B.2.2.3
4	Mismatch	B.2.2.4
5	Standing wave between the DUT and measurement antenna	B.2.2.5
6	Uncertainty of the RF power measurement equipment	B.2.2.6
7	Phase curvature	B.2.2.7
8	Amplifier uncertainties	B.2.2.8
9	Random uncertainty	B.2.2.9
10	Influence of the XPD	B.2.2.10
11	Insertion Loss Variation	B.2.2.11
12	RF leakage (from measurement antenna to the receiver/transmitter)	B.2.2.12
13	Influence of TRP measurement grid	B.2.2.22
14	Influence of beam peak search grid	B.2.2.23
Stage 1: Calibration measurement		
15	Mismatch	B.2.2.4
16	Amplifier Uncertainties	B.2.2.8
17	Misalignment of positioning System	B.2.2.13
18	Uncertainty of the Network Analyzer	B.2.2.14
19	Uncertainty of the absolute gain of the calibration antenna	B.2.2.15
20	Positioning and pointing misalignment between the reference antenna and the measurement antenna	B.2.2.16
21	Phase centre offset of calibration antenna	B.2.2.18
22	Quality of quiet zone for calibration process	B.2.2.19
23	Standing wave between reference calibration antenna and measurement antenna	B.2.2.20
24	Influence of the calibration antenna feed cable	B.2.2.21
Systematic uncertainties		
25	Mean error related to TRP calculation applying sin(θ)-weighting	B.2.2.24

The uncertainty assessment tables are organized as follows:

- For the purpose of uncertainty assessment, the radiating antenna aperture of the DUT is denoted as D
- The uncertainty assessment has been derived for the case of D = [15 cm], f = {22.65GHz, 31.1GHz, 45.1GHz}, [P = maximum output power].
- The uncertainty assessment for EIRP and TRP is provided in Table B.3.2-2.

Table B.3.2-2: Uncertainty assessment for EIRP and TRP measurement (f=TBD, DUT size = TBD)

UID	Uncertainty source	Uncertainty value	Distribution of the probability	Divisor	Standard uncertainty (σ) [dB]
Stage 2: DUT measurement					
1	Positioning misalignment				
2	Measure distance uncertainty				
3	Quality of Quiet Zone (NOTE 1)				
4	Mismatch (NOTE 2)				
5	Standing wave between the DUT and measurement antenna				
6	Uncertainty of the RF power measurement equipment (NOTE 3)				
7	Phase curvature				
8	Amplifier uncertainties				
9	Random uncertainty				
10	Influence of the XPD				
11	Insertion Loss Variation				
12	RF leakage (from measurement antenna to the receiver/transmitter)				
13	Influence of TRP measurement grid (NOTE 4)	0.25	Actual	1	0.25
14	Influence of beam peak search grid (NOTE 5)	0.5	Actual	1	0.5
Stage 1: Calibration measurement					
15	Mismatch				
16	Amplifier Uncertainties				
17	Misalignment of positioning System				
18	Uncertainty of the Network Analyzer				
19	Uncertainty of the absolute gain of the calibration antenna				
20	Positioning and pointing misalignment between the reference antenna and the measurement antenna				
21	Phase centre offset of calibration antenna				
22	Quality of quiet zone for calibration process (NOTE 1)				
23	Standing wave between reference calibration antenna and measurement antenna				
24	Influence of the calibration antenna feed cable				
	Systematic uncertainties (NOTE 6)				**Value**
25	Mean error for constant step size grid (NOTE 4)				0.34
Total measurement uncertainty					**Value**
EIRP Expanded uncertainty (1.96σ - confidence interval of 95 %) [dB]					
TRP Expanded uncertainty (1.96σ - confidence interval of 95 %) [dB]					

NOTE 1: The quality of quiet zone is different for EIRP and TRP. For TRP, the standard uncertainty is FFS; for EIRP FFS
NOTE 2: The analysis was done only for the case of operating at max output power, in-band, non-CA.
NOTE 3: The assessment assumes maximum DUT output power.
NOTE 4: This contributor shall only be considered for TRP measurements.
NOTE 5: This contributor shall only be considered for EIRP measurements.
NOTE 6: In order to obtain the total measurement uncertainty, systematic uncertainties have to be added to the expanded root sum square of the standard deviations of the Stage 1 and Stage 2 contributors.

B.3.3 Uncertainty budget format and assessment for NFTF

The uncertainty contributions that may impact the overall MU value are listed in Table B.3.3-1.

Table B.3.3-1: Uncertainty contributions for EIRP and TRP measurement

UID	Description of uncertainty contribution	Details in paragraph
	Stage 2: EIRP Near Field Radiation Pattern Measurement and EIRP Near Field DUT power measurement	
1	Axis Alignment	B.2.3.1
2	Measurement Distance Uncertainty	B.2.3.2
3	Quality of the Quiet Zone	B.2.3.3
4	Mismatch	B.2.3.4
5	Multiple Reflections: Coupling between Measurement Antenna and DUT	B.2.3.5
6	Uncertainty of the RF power measurement equipment	B.2.3.6
7	Phase curvature	B.2.3.7
8	Amplifier uncertainties	B.2.3.8
9	Random uncertainty	B.2.3.9
10	Influence of the XPD	B.2.3.10
11	NF to FF truncation	B.2.3.11
12	Probe Polarization Amplitude and Phase	B.2.3.12
13	Probe Array Uniformity (for multi-probe systems only)	B.2.3.13
14	Phase Recovery Non-Linearity over signal bandwidth	B.2.3.16
15	Probe Pattern Effect	B.2.3.17
16	Phase Drift and Noise	B.2.3.20
17	Leakage and Crosstalk	B.2.3.25
	Stage 1: Calibration measurement	
18	Mismatch	B.2.3.4
19	Amplifier uncertainties	B.2.3.8
20	Uncertainty of the Network Analyzer	B.2.3.14
21	Uncertainty of the absolute gain of the calibration antenna	B.2.3.15
22	Phase centre offset of calibration	B.2.3.18
23	Quality of the Quiet Zone for Calibration Process	B.2.3.19
24	Mismatch in the connection of the calibration antenna	B.2.3.21

The uncertainty assessment table is organized as follows:

- For the purpose of uncertainty assessment, the radiating antenna aperture of the DUT is denoted as D
- The uncertainty assessment has been derived for the case of D = [5 cm], f = {22.65GHz, 31.1GHz, 45.1GHz}, P = [maximum output power].
- The uncertainty assessment for EIRP and TRP is provided in Table B.3.1-2.

Table B.3.3-2: Uncertainty assessment for EIRP and TRP measurement (f=TBD, D=TBD)

UID	Description of uncertainty contribution	Uncertainty Value	Distribution of the probability	Divisor	Standard uncertainty (σ) [dB]
	Stage 2: EIRP Near Field Radiation Pattern Measurement and EIRP Near Field DUT power measurement				
1	Axis Alignment				
2	Measurement Distance Uncertainty				
3	Quality of the Quiet Zone				
4	Mismatch				
5	Multiple Reflections: Coupling between Measurement Antenna and DUT				
6	Uncertainty of the RF power measurement equipment				
7	Phase curvature				
8	Amplifier uncertainties				
9	Random uncertainty				
10	Influence of the XPD				
11	NF to FF truncation				
12	Probe Polarization Amplitude and Phase				
13	Probe Array Uniformity (for multi-probe systems only)				
14	Phase Recovery Non-Linearity over signal bandwidth				
15	Probe Pattern Effect				
16	Phase Drift and Noise				
17	Leakage and Crosstalk				
	Stage 1: Calibration measurement				
18	Mismatch				
19	Amplifier uncertainties				
20	Uncertainty of the Network Analyzer				
21	Uncertainty of the absolute gain of the calibration antenna				
22	Phase centre offset of calibration				
23	Quality of the Quiet Zone for Calibration Process				
24	Mismatch in the connection of the calibration antenna				
EIRP Expanded uncertainty (1.96σ - confidence interval of 95 %) [dB]					
TRP Expanded uncertainty (1.96σ - confidence interval of 95 %) [dB]					
NOTE 1: The impact of phase variation on EIRP is FFS. NOTE 2: The quality of quiet zone is different for EIRP and TRP. For TRP, the standard uncertainty is FFS; for EIRP FFS. NOTE 3: The analysis was done only for the case of operating at max output power, in-band, non-CA, NOTE 4: The assessment assumes maximum DUT output power. NOTE 5: The Phase Recovery Non-Linearity over signal bandwidth is FFS.					

Annex C: Acceptable uncertainty of test system for test cases defined in TS 38.521-3 for radiative testing

FFS

Annex D: Acceptable uncertainty of test system for test cases defined in TS 38.521-4 for radiative testing

FFS

Annex E: Acceptable uncertainty of test system for test cases defined in TS 38.533 for radiative testing

FFS

Annex F: Change history

Change history							
Date	**Meeting**	**TDoc**	**CR**	**Rev**	**Cat**	**Subject/Comment**	**New version**
2017-09	RAN5 #76	R5-174706				Initial skeleton	0.0.1
2018-04	RAN5 #2-5G-NR-Adhoc	R5-182093				Implementation of pCRs to TS 38.903 V0.0.1	0.1.0
2018-05	RAN5#79	R5-182670				Editorial update of TR 38.903.	0.2.0
2018-09	RAN5#80	R5-185213				Making Measurement Uncertainty Terms Common between methods in TR 38.90	1.0.0
2018-09	RAN5#80	R5-185214				TP on Measurement Uncertainty Contributions in FR2	1.0.0
2018-09	RAN5#80	R5-185212				Adding MU values for EIRPTRP measurements with Near Field test range (NFTF) at mmWave	1.0.0
2018-09	RAN#81	-	-	-	-	raised to v15.0.0 with editorial changes only	15.0.0

History

Document history		
V15.0.0	October 2018	Publication