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Foreword

This ETSI Technical Report (ETR) has been produced by the Electromagnetic compatibility and Radio spectrum Matters (ERM) Technical Committee of the European Telecommunications Standards Institute (ETSI).

ETRs are informative documents resulting from ETSI studies which are not appropriate for European Telecommunication Standard (ETS) or Interim European Telecommunication Standard (I-ETS) status. An ETR may be used to publish material which is either of an informative nature, relating to the use or the application of ETSs or I-ETSs, or which is immature and not yet suitable for formal adoption as an ETS or an I-ETS.

The present ETR is part 4 of a multi-part Technical Report (ETR) covering Electromagnetic compatibility and Radio spectrum Matters (ERM); Improvement of radiated methods of measurement (using test sites) and evaluation of the corresponding measurement uncertainties, as identified below:

Part 1-1: "Uncertainties in the measurement of mobile radio equipment characteristics; Sub-part 1: Introduction";

Part 1-2: "Uncertainties in the measurement of mobile radio equipment characteristics; Sub-part 2: Examples and annexes";

Part 2: "Anechoic chamber";

Part 3: "Anechoic chamber with a ground plane";

Part 4: "Open area test site";

Part 5: "Striplines";

Part 6: "Test fixtures";

Part 7: "Artificial human beings".

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1 Scope

This ETR covers the methods of radiated measurements on mobile radio equipment on an open area test site and applies to the assessment of the associated measurement uncertainties.

This ETR also provides the methods for evaluation and calculation of the measurement uncertainties for each of the measured parameters and the required corrections for measurement conditions and results.

2 References

Within this ETR the following references apply:

[1] ANSI C63.5-(1988): "Electromagnetic Compatibility-Radiated Emission Measurements in Electromagnetic Interference (EMI) Control - Calibration of Antennas".

[2] *Antenna theory*, C. Balanis, J. E. Wiley 1982.

[3] *"Calculation of site attenuation from antenna factors"* A. A. Smith Jr, RF German and J B Pate. IEEE transactions EMC. Vol. EMC 24 pp 301-316 Aug 1982.

[4] CCITT Recommendation O.41: "Psophometer for use on telephone-type circuits".

[5] CCITT Recommendation O.153: "Basic parameters for the measurement of error performance at bit rates below the primary rate".

[6] CISPR 16-1: "Specification for radio disturbance and immunity measuring apparatus and methods - Part 1: Radio disturbance and immunity measuring apparatus".

[7] *"Control of errors on Open Area Test Sites"*, A. A. Smith Jnr. EMC technology October 1982 page 50-58.

[8] EN 50147-2: "Anechoic chambers -- Part 2: Alternative test site suitability with respect to site attenuation".

[9] ETR 273-1-1: "Electromagnetic compatibility and Radio spectrum Matters (ERM); Improvement of radiated methods of measurement (using test sites) and evaluation of the corresponding measurement uncertainties; Part 1: Uncertainties in the measurement of mobile radio equipment characteristics; Sub-part 1: Introduction".

[10] ETR 273-1-2: "Electromagnetic compatibility and Radio spectrum Matters (ERM); Improvement of radiated methods of measurement (using test sites) and evaluation of the corresponding measurement uncertainties; Part 1: Uncertainties in the measurement of mobile radio equipment characteristics; Sub-part 2: Examples and annexes".

[11] "*The gain resistance product of the half-wave dipole*", W. Scott Bennet Proceedings of IEEE vol. 72 No. 2 Dec 1984 pp 1824-1826.

[12] "*The new IEEE standard dictionary of electrical and electronic terms*". Fifth edition, IEEE Piscataway, NJ USA 1993.

3 Definitions, symbols and abbreviations

3.1 Definitions

For the purposes of this ETR, the following definitions apply:

Audio Frequency (**AF) load**: Normally a resistor of sufficient power rating to accept the maximum audio output power from the EUT. The value of the resistor is normally that stated by the manufacturer and is normally the impedance of the audio transducer at 1 000 Hz.

NOTE 1: In some cases it may be necessary to place an isolating transformer between the output terminals of the receiver under test and the load.

AF termination: Any connection other than the audio frequency load which may be required for the purpose of testing the receiver. (i.e. in a case where it is required that the bit stream be measured, the connection may be made, via a suitable interface, to the discriminator of the receiver under test).

NOTE 2: The termination device is normally agreed between the manufacturer and the testing authority and details included in the test report. If special equipment is required then it is normally provided by the manufacturer.

A-M1: A test modulation consisting of a 1 000 Hz tone at a level which produces a deviation of 12 % of the channel separation.

A-M2: A test modulation consisting of a 1 250 Hz tone at a level which produces a deviation of 12 % of the channel separation.

A-M3: A test modulation consisting of a 400 Hz tone at a level which produces a deviation of 12 % of the channel separation. This signal is used as an unwanted signal for analogue and digital measurements.

antenna: That part of a transmitting or receiving system that is designed to radiate or to receive electromagnetic waves.

antenna factor: Quantity relating the strength of the field in which the antenna is immersed to the output voltage across the load connected to the antenna. When properly applied to the meter reading of the measuring instrument, yields the electric field strength in V/m or the magnetic field strength in A/m.

antenna gain: The ratio of the maximum radiation intensity from an (assumed lossless) antenna to the radiation intensity that would be obtained if the same power were radiated isotropically by a similarly lossless antenna.

bit error ratio: The ratio of the number of bits in error to the total number of bits.

combining network: A multipole network allowing the addition of two or more test signals produced by different sources for connection to a receiver input.

NOTE 3: Sources of test signals are normally connected in such a way that the impedance presented to the receiver is 50 Ω. Combining networks are so designed that the combining networks are designed so that effects of any intermodulation products and noise produced in the signal generators are negligible.

correction factor: The numerical factor by which the uncorrected result of a measurement is multiplied to compensate for an assumed systematic error.

confidence level: The probability of the accumulated error of a measurement being within the stated range of uncertainty of measurement.

directivity: The ratio of the maximum radiation intensity in a given direction from the antenna to the radiation intensity averaged over all directions (i.e. directivity = antenna gain + losses).

duplex filter: A device fitted internally or externally to a transmitter/receiver combination to allow simultaneous transmission and reception with a single antenna connection.

DM-0: A test modulation consisting of a signal representing an infinite series of "0" bits

DM-1: A test modulation consisting of a signal representing an infinite series of "1" bits

DM-2: A test modulation consisting of a signal representing a pseudorandom bit sequence of at least 511 bits in accordance with CCITT Recommendation O.153 [5].

DM-3: A test signal agreed between the testing authority and the manufacturer in the cases where it is not possible to measure a bit stream or if selective messages are used and are generated or decoded within an equipment

NOTE 4: The agreed test signal may be formatted and may contain error detection and correction. Details of the test signal should be supplied in the test report.

error of measurement (absolute): The result of a measurement minus the true value of the measurand.

error (relative): The ratio of an error to the true value.

estimated standard deviation: From a sample of n results of a measurement the estimated standard deviation is given by the formula:

$$\sigma = \sqrt{\frac{\sum_{i=1}^{n}(x_i - \bar{x})^2}{n-1}}$$

x_i being the i^{th} result of measurement (i = 1,2,3, ...,n) and $\bar{x}$ the arithmetic mean of the n results considered.

A practical form of this formula is:

$$\sigma = \sqrt{\frac{Y - \frac{X^2}{n}}{n-1}}$$

Where X is the sum of the measured values and Y is the sum of the squares of the measured values.

extreme test conditions: Conditions defined in terms of temperature and supply voltage. Tests are normally made with the extremes of temperature and voltage applied simultaneously. The upper and lower temperature limits are specified in the relevant testing standard. The test report states the actual temperatures measured.

error (of a measuring instrument): The indication of a measuring instrument minus the (conventional) true value.

free field: A field (wave or potential) which has a constant ratio between the electric and magnetic field intensities.

free Space: A region free of obstructions and characterized by the constitutive parameters of a vacuum.

impedance: A measure of the complex resistive and reactive attributes of a component in an alternating current circuit.

impedance (wave): The complex factor relating the transverse component of the electric field to the transverse component of the magnetic field at every point in any specified plane, for a given mode.

influence quantity: A quantity which is not the subject of the measurement but which influences the value of the quantity to be measured or the indications of the measuring instrument.

intermittent operation: Operation where the manufacturer states the maximum time that the equipment is intended to transmit and the necessary standby period before repeating a transmit period.

isotropic radiator: A hypothetical, lossless antenna having equal radiation intensity in all directions.

limited Frequency Range: A specified smaller frequency range within the full frequency range over which the measurement is made.

NOTE 5: The details of the calculation of the limited frequency range are normally given in the relevant testing standard.

maximum permissible frequency deviation: The maximum value of frequency deviation stated for the relevant channel separation in the relevant testing standard.

measuring system: A complete set of measuring instruments and other equipment assembled to carry out a specified measurement task.

measurement repeatability: The closeness of the agreement between the results of successive measurements of the same measurand carried out subject to all the following conditions:

- the same method of measurement;
- the same observer;
- the same measuring instrument;
- the same location;
- the same conditions of use;
- repetition over a short period of time.

measurement reproducibility: The closeness of agreement between the results of measurements of the same measurand, where the individual measurements are carried out changing conditions such as:

- method of measurement;
- observer;
- measuring instrument;
- location;
- conditions of use;
- time.

measurand: A quantity subjected to measurement.

noise gradient of EUT: A function characterizing the relationship between the RF input signal level and the performance of the EUT, e.g., the SINAD of the AF output signal.

nominal frequency: One of the channel frequencies on which the equipment is designed to operate.

nominal mains voltage: The declared voltage or any of the declared voltages for which the equipment was designed.

normal test conditions: The conditions defined in terms of temperature, humidity and supply voltage stated in the relevant testing standard.

normal deviation: The frequency deviation for analogue signals which is equal to 12 % of the channel separation.

psophometric weighting network: As described in CCITT Recommendation O.41 [4].

polarization: For an electromagnetic wave, the figure traced as a function of time by the extremity of the electric vector at a fixed point in space.

quantity (measurable): An attribute of a phenomenon or a body which may be distinguished qualitatively and determined quantitatively.

rated audio output power: The maximum audio output power under normal test conditions, and at standard test modulations, as declared by the manufacturer.

rated radio frequency output power: The maximum carrier power under normal test conditions, as declared by the manufacturer.

shielded enclosure: A structure that protects its interior from the effects of an exterior electric or magnetic field, or conversely, protects the surrounding environment from the effect of an interior electric or magnetic field.

SINAD sensitivity: The minimum standard modulated carrier-signal input required to produce a specified SINAD ratio at the receiver output.

stochastic (random) variable: A variable whose value is not exactly known, but is characterized by a distribution or probability function, or a mean value and a standard deviation (e.g. a measurand and the related measurement uncertainty).

test load: The test load is a 50 Ω substantially non-reactive, non-radiating power attenuator which is capable of safely dissipating the power from the transmitter.

test modulation: The test modulating signal is a baseband signal which modulates a carrier and is dependent upon the type of EUT and also the measurement to be performed.

trigger device: A circuit or mechanism to trigger the oscilloscope timebase at the required instant. It may control the transmit function or inversely receive an appropriate command from the transmitter.

uncertainty (random): A component of the uncertainty of measurement which, in the course of a number of measurements of the same measurand, varies in an unpredictable way.

uncertainty (systematic): A component of the uncertainty of measurement which, in the course of a number of measurements of the same measurand remains constant or varies in a predictable way.

uncertainty (limits of uncertainty of a measuring instrument): The extreme values of uncertainty permitted by specifications, regulations etc. for a given measuring instrument.

NOTE 6: This term is also known as "tolerance".

uncertainty (standard): The representation of each individual uncertainty component that contributes to the overall measurement uncertainty by an estimated standard deviation is termed the standard uncertainty.

uncertainty (combined standard): The combined standard uncertainty of a measurement is calculated by combining the standard uncertainties for each of the individual contributions identified.

NOTE 7: This combination is carried out by applying the Root of the Sum of the Squares (the RSS) method under the assumption that all contributions are stochastic i.e. independent of each other.

uncertainty (expanded): The combined standard uncertainty is multiplied by a constant to give the expanded uncertainty limits.

upper specified AF limit: The maximum audio frequency of the audio pass-band. It is dependent on the channel separation.

wanted signal level: For conducted measurements, a level of +6 dBµV emf referred to the receiver input under normal test conditions. Under *extreme test conditions* the value is +12 dBµV emf.

NOTE 8: For analogue measurements the wanted signal level has been chosen to be equal to the limit value of the measured usable sensitivity. For bit stream and message measurements the wanted signal has been chosen to be +3 dB above the limit value of measured usable sensitivity.

3.2 Symbols

For the purpose of this ETR, the following symbols apply:

β	2π/λ (radians/m)
γ	incidence angle with ground plane (°)
λ	wavelength (m)
ϕ_H	phase angle of reflection coefficient (°)
η	120π Ohms - the intrinsic impedance of free space (Ω)
μ	permeability (H/m)
AF_R	antenna factor of the receive antenna (dB/m)
AF_T	antenna factor of the transmit antenna (dB/m)
AF_{TOT}	mutual coupling correction factor (dB)
c	calculated on the basis of given and measured data
C_{cross}	cross correlation coefficient
d	derived from a measuring equipment specification
$D(\theta,\phi)$	directivity of the source
d	distance between dipoles (m)
δ	skin depth (m)
d_1	an antenna or EUT aperture size (m)
d_2	an antenna or EUT aperture size (m)
d_{dir}	path length of the direct signal (m)
d_{refl}	path length of the reflected signal (m)
E	electric field intensity (V/m)
E_{DH}^{max}	calculated maximum electric field strength in the receiving antenna height scan from a half wavelength dipole with 1 pW of radiated power (for horizontal polarization) (µV/m)
E_{DV}^{max}	calculated maximum electric field strength in the receiving antenna height scan from a half wavelength dipole with 1 pW of radiated power (for vertical polarization) (µV/m)
e_{ff}	antenna efficiency factor
ϕ	angle (°)
Δf	bandwidth (Hz)
f	frequency (Hz)
$G(\theta,\phi)$	gain of the source (which is the source directivity multiplied by the antenna efficiency factor)
H	magnetic field intensity (A/m)
I_0	the (assumed constant) current (A)
I_m	the maximum current amplitude
k	2π/λ
k	a factor from Student's t distribution
k	Boltzmann's constant (1,38 x 10-23 Joules/Kelvin)
K	relative dielectric constant
l	the length of the infinitesimal dipole (m)
L	the overall length of the dipole (m)
l	the point on the dipole being considered (m)
m	measured
λ	wavelength (m)

p	power
$Pe_{(n)}$	probability of error n
$Pp_{(n)}$	probability of position n
P_r	antenna noise power (W)
P_{rec}	power received (W)
P_t	power transmitted (W)
θ	angle (°)
ρ	reflection coefficient
r	rectangular distribution
r	the distance to the field point (m)
ρ_g	reflection coefficient of the generator part of a connection
ρ_l	reflection coefficient of the load part of the connection
R_s	equivalent surface resistance (Ω)
σ	conductivity (S/m)
σ	standard deviation
SNR_{b*}	Signal to noise ratio at a specific BER
SNR_b	Signal to noise ratio per bit
T_A	antenna temperature (Kelvin)
u	U-distribution
U	the expanded uncertainty corresponding to a confidence level of x %: $U = k \times u_c$
u_c	the combined standard uncertainty
u_i	general type A standard uncertainty
u_{i01}	random uncertainty
u_j	general type B uncertainty
u_{j01}	reflectivity of absorbing material: EUT to the test antenna
u_{j02}	reflectivity of absorbing material: substitution or measuring antenna to the test antenna
u_{j03}	reflectivity of absorbing material: transmitting antenna to the receiving antenna
u_{j04}	mutual coupling: EUT to its images in the absorbing material
u_{j05}	mutual coupling: de-tuning effect of the absorbing material on the EUT
u_{j06}	mutual coupling: substitution, measuring or test antenna to its image in the absorbing material
u_{j07}	mutual coupling: transmitting or receiving antenna to its image in the absorbing material
u_{j08}	mutual coupling: amplitude effect of the test antenna on the EUT
u_{j09}	mutual coupling: de-tuning effect of the test antenna on the EUT
u_{j10}	mutual coupling: transmitting antenna to the receiving antenna
u_{j11}	mutual coupling: substitution or measuring antenna to the test antenna
u_{j12}	mutual coupling: interpolation of mutual coupling and mismatch loss correction factors
u_{j13}	mutual coupling: EUT to its image in the ground plane
u_{j14}	mutual coupling: substitution, measuring or test antenna to its image in the ground plane
u_{j15}	mutual coupling: transmitting or receiving antenna to its image in the ground plane
u_{j16}	range length
u_{j17}	correction: off boresight angle in the elevation plane
u_{j18}	correction: measurement distance
u_{j19}	cable factor
u_{j20}	position of the phase centre: within the EUT volume
u_{j21}	positioning of the phase centre: within the EUT over the axis of rotation of the turntable
u_{j22}	position of the phase centre: measuring, substitution, receiving, transmitting or test antenna
u_{j23}	position of the phase centre: LPDA
u_{j24}	Stripline: mutual coupling of the EUT to its images in the plates
u_{j25}	Stripline: mutual coupling of the three-axis probe to its image in the plates
u_{j26}	Stripline: characteristic impedance

u_{j27}	Stripline: non-planar nature of the field distribution
u_{j28}	Stripline: field strength measurement as determined by the three-axis probe
u_{j29}	Stripline: transform Factor
u_{j30}	Stripline: interpolation of values for the transform factor
u_{j31}	Stripline: antenna factor of the monopole
u_{j32}	Stripline: correction factor for the size of the EUT
u_{j33}	Stripline: influence of site effects
u_{j34}	ambient effect
u_{j35}	mismatch: direct attenuation measurement
u_{j36}	mismatch: transmitting part
u_{j37}	mismatch: receiving part
u_{j38}	signal generator: absolute output level
u_{j39}	signal generator: output level stability
u_{j40}	insertion loss: attenuator
u_{j41}	insertion loss: cable
u_{j42}	insertion loss: adapter
u_{j43}	insertion loss: antenna balun
u_{j44}	antenna: antenna factor of the transmitting, receiving or measuring antenna
u_{j45}	antenna: gain of the test or substitution antenna
u_{j46}	antenna: tuning
u_{j47}	receiving device: absolute level
u_{j48}	receiving device: linearity
u_{j49}	receiving device: power measuring receiver
u_{j50}	EUT: influence of the ambient temperature on the ERP of the carrier
u_{j51}	EUT: influence of the ambient temperature on the spurious emission level
u_{j52}	EUT: degradation measurement
u_{j53}	EUT: influence of setting the power supply on the ERP of the carrier
u_{j54}	EUT: influence of setting the power supply on the spurious emission level
u_{j55}	EUT: mutual coupling to the power leads
u_{j56}	frequency counter: absolute reading
u_{j57}	frequency counter: estimating the average reading
u_{j58}	Salty man/Salty-lite: human simulation
u_{j59}	Salty man/Salty-lite: field enhancement and de-tuning of the EUT
u_{j60}	Test Fixture: effect on the EUT
u_{j61}	Test Fixture: climatic facility effect on the EUT
V_{direct}	received voltage for cables connected via an adapter (dBµV/m)
V_{site}	received voltage for cables connected to the antennas (dBµV/m)
W_0	radiated power density (W/m^2)

3.3 Abbreviations

For the purpose of this ETR, the following abbreviations apply:

AF	Audio Frequency
BER	Bit Error Ratio
dB	decibel
emf	Electromotive force
ERP	Effective Radiated Power
EUT	Equipment Under Test
FSK	Frequency Shift Keying
GMSK	Gaussian Minimum Shift Keying
GSM	Global System for Mobile telecommunication (Pan European digital telecommunication system)
LPDA	Log Periodic Dipole Antenna
IF	Intermediate Frequency
NaCl	Sodium chloride
NSA	Normalised Site Attenuation
RF	Radio Frequency
RMS	Root Mean Square

RSS	Root-Sum-of Squares
SINAD	Signal Noise And Distortion
TEM	Transverse ElectroMagnetic
VSWR	Voltage Standing Wave Ratio

4 Introduction

An open area test site comprises a turntable at one end and an antenna mast of variable height at the other set above a ground plane which, in the ideal case, is perfectly conducting and of infinite extent. In practice, whilst good conductivity can be achieved, the ground plane size has to be limited. A typical open area test site is shown in figure 1.

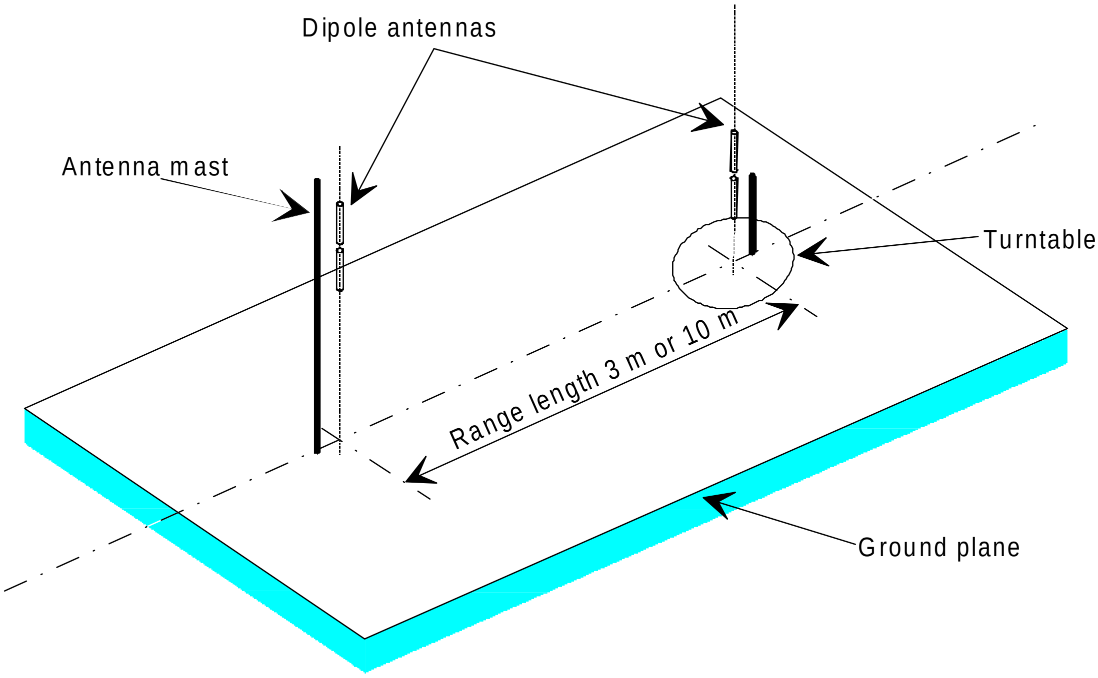

Figure 1: A typical open area test site

The ground plane creates a wanted reflection path, such that the signal received by the receiving antenna is the sum of the signals received from the direct and reflected transmission paths. The phasing of these two signals creates a unique received level for each height of the transmitting antenna (or EUT) and the receiving antenna above the ground plane.

In practice, the antenna mast provides a variable height facility so that the elevation of the test antenna can be optimized for maximum coupled signal in conjunction with the turntable for azimuth angle.

Both absolute and relative measurements can be performed on an open area test site. Where absolute measurements are to be carried out, or where the test site is to be used for accredited measurements, the open area test site should be verified. Verification involves comparison of the measured performance to that of an ideal theoretical site, with acceptability being decided on the basis of the differences not exceeding some pre-determined limits.

The open area test site has been, historically, the reference site upon which the majority, if not all, of the specification limits have been set. The ground plane was originally introduced to provide uniformity of ground conditions, between test sites, during testing.

5 Uncertainty contributions specific to an open area test site

5.1 Introduction

open area test site performance is dependant on many factors such as the size and shape of the ground plane, its surface material and roughness, edge termination, dielectric coverings, environmental conditions, weather protection, the size of the EUT, the type of test being carried out, the required frequency range, etc.

These are some of the factors that have to be evaluated to ensure optimum use of the open area test site. In this case "optimum use" refers to minimization of the uncertainty contributions.

5.2 Ground plane

A conducting ground plane should be made from metals preferably of a non ferrous nature such as copper or aluminium. It does not have to be constructed of solid sheet but can be perforated metal, welded mesh, metal gratings, etc., but wherever a gap or a void occurs within the screen, it should not measure more than $\lambda/10$ at the highest frequency of operation in any dimension. This maximum dimension applies equally to joints and seams between metal sheets/panels where these have been used to make the ground plane.

The main reflection comes from the ray which makes equal incident and reflected angles on the ground plane surface, although other areas within the plane contribute to the overall interference signal level coming from the ground. This is a result of diffraction. The resulting size of the ground plane for reliable measurements is subject to both calculation and practical experience and can vary depending on the profile of ground plane chosen i.e. there are different recommendations for elliptical and rectangular planes.

The size of the ground plane needs to be large enough to cover the entire area from which reflections will arise. ANSI use Fresnel ellipses on the reflecting surface (see figure 63) as a basis for determining the size, where the ellipse is defined by the locus of equal reflected path lengths from the EUT to the test antenna.

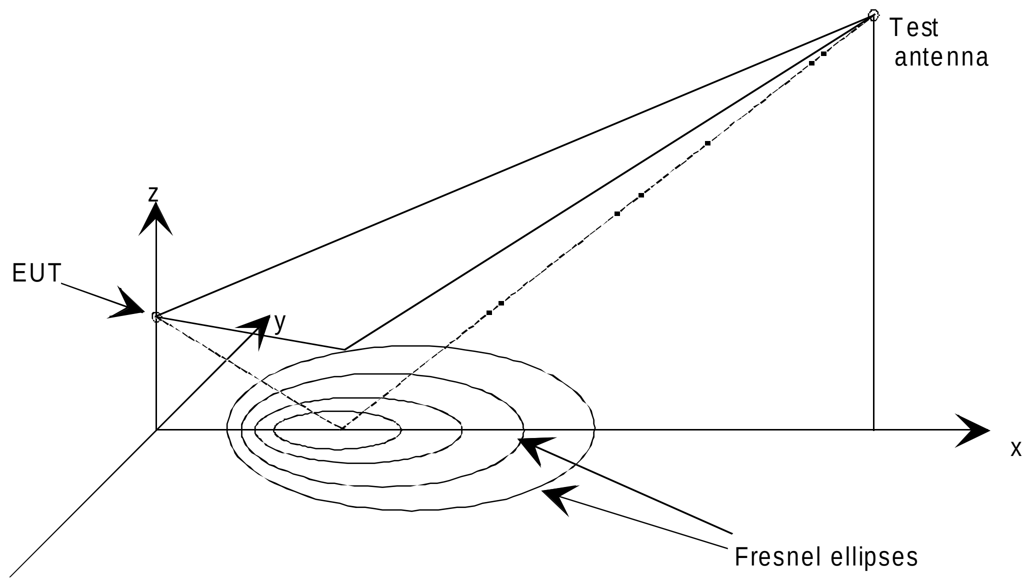

Figure 2: Fresnel ellipses drawn on the reflecting surface

The ellipse corresponding to the first Fresnel zone i.e. the one which gives a path length change of half a wavelength at the lowest frequency of operation, is the minimum size of ground plane they recommend. This is dependent on the test site geometry (i.e. measurement distance, source height, receive antenna height variation) and the wavelength of the lowest frequency.

It has been reported "*Control of errors on Open Area Test Sites*" [7] that simply increasing the ground plane size, in an attempt to improve its approximation to an infinite plane, may not always be beneficial. When the edge of the ground plane is not well terminated, the edge effects (i.e. the difference between theoretical and measured results for vertical polarization) can actually increase as the ground plane gets larger.

The smoothness of the reflecting surface is of importance and as a general rule of thumb, the surface roughness is taken to be less than $\lambda/10$ at the shortest wavelength of usage. For all tests under consideration here (where 12,75 GHz is the uppermost frequency of interest), this implies that the surface should smoother than 2,35 mm.

5.2.1 Coatings

Where thick dielectric coatings have been applied to a metal ground plane e.g. asphalt, gravel, concrete, etc.; or where a layer of snow has fallen, the nature of the reflection can be significantly changed, particularly for vertical polarization. This effect is illustrated in figure 3 where the patterns above ground of a vertical dipole are presented. The solid line represents the performance above a perfectly reflecting surface, whereas the dashed line is for the same antenna above a dielectric covered, reasonably conductive ground plane. The received signal levels consequently can show an enormous variation in level depending on the state of the reflecting surface when vertically polarized tests are being performed. The change in reflectivity for horizontal polarization is relatively minor in comparison.

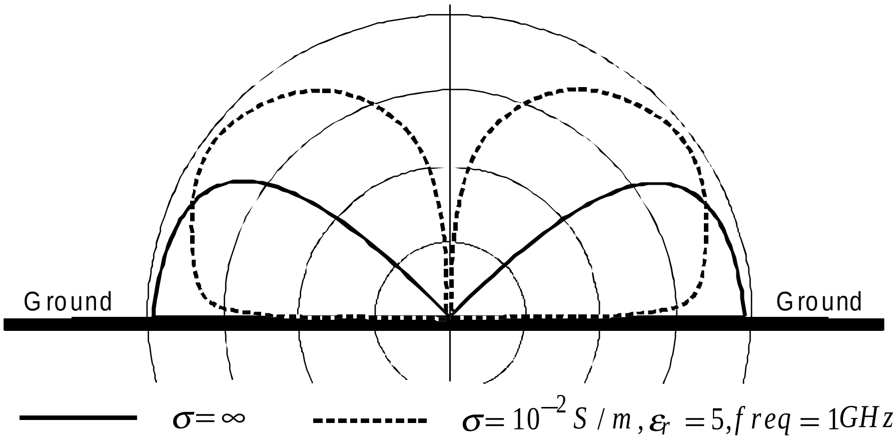

Figure 3: Patterns for vertical dipole above different ground planes

When comparing results from different sites, the reflection coefficient variations from one ground plane medium to another, even when measurement geometry remains the same, can produce significant differences in the measured results.

To minimize these uncertainties, the ground plane should be a highly conductive, relatively non ferrous metal with no dielectric coating.

5.2.2 Reflections from the ground plane

Far from a perfectly conducting ground plane, at a distance sufficient to make the difference between the direct and reflected path lengths negligible and the direct and reflected waves appear parallel to each other, the amplitude of the reflected wave is equal to the amplitude of the direct wave. When these two waves add "in phase" the electric field strength doubles (6 dB gain) whereas, at another point the two waves are "out of phase" and cancel entirely resulting in no net electric field. Therefore, over a perfectly conducting ground plane at infinite distance it is possible to obtain field strengths varying from + 6 dB to - ∞ dB relative to the free space field strength (see figure 4a).

In practice, the distance between the EUT and the test antenna is not infinite, the direct and reflected waves are not parallel and their path lengths can differ substantially. In this condition the field measured by the test antenna can alternate between peaks and nulls many times as the test antenna is raised and lowered through the available height range. The difference in path lengths, along with any directivity of the test antenna in the vertical plane result in the direct and reflected waves not being equal in amplitude. As a result, when they add "in phase" the peak will be less than + 6 dB and when they are out of phase their amplitudes do not fully cancel, resulting in an electric field greater than - ∞ dB (null filling) (see figure 4b).

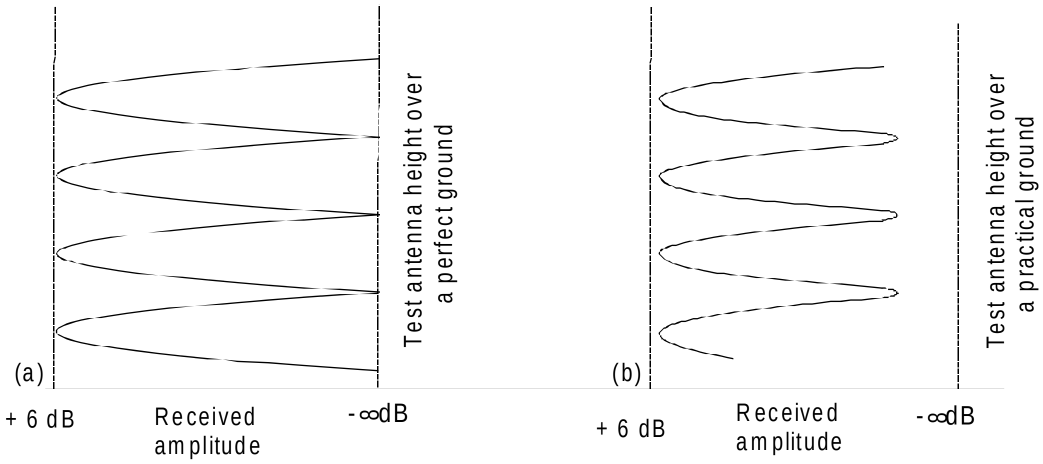

Figure 4: Comparison of the received amplitude for an ideal site against a practical site

For testing purposes, when it is necessary to generate a uniform field in, for example, immunity measurements, the region of interest is either a particular volume or area into which the EUT will be placed. The degree of uniformity of the fields within this volume is affected by many factors, such as the relative positions of the radiating antenna and the EUT, the radiation patterns, the size and construction of the EUT, etc.

The interaction of the direct and ground reflected waves produce regular sharp amplitude nulls in the volume occupied by the EUT or receiving/measuring antenna (see figure 5).

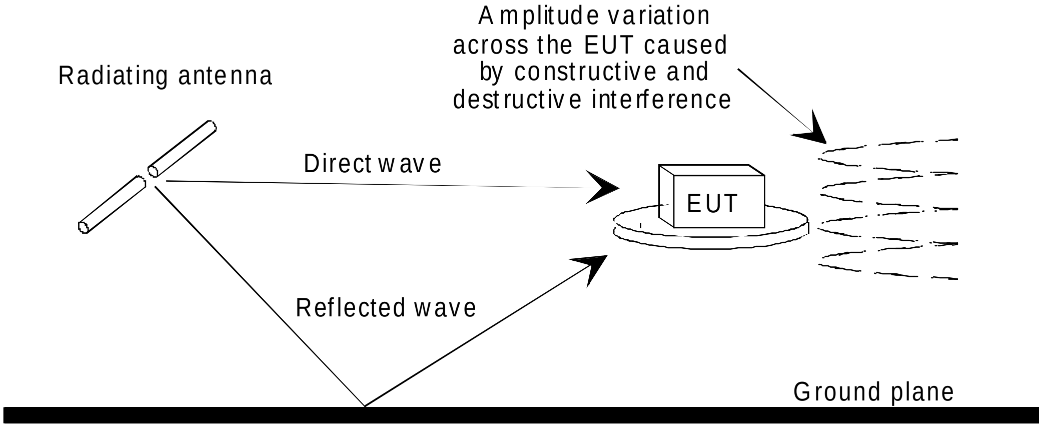

Figure 5: Amplitude variation in the test volume

The smaller the EUT the more uniform the field across it. As a general rule, for minimum measurement uncertainty during tests, its size should be significantly smaller than the distance between the nulls. The nulling effect is more severe in the vertical plane than the horizontal plane of the volume occupied by the EUT, and it is worst when the transmitting antenna is at its maximum height (4 m), and horizontally polarized (since the ground plane is fully illuminated by the omni-directional pattern of the dipole in this polarization). In this worst case, the maximum vertical dimension an EUT or receiving/measuring antenna can have on a 3 m test range is between 0,4 to 0,6 wavelengths (depending on the frequency, height on the mast, mutual coupling effects etc.) for the amplitude of the field across it to vary by no more than - 3 dB at its edges (relative to its centre).

The phase variation is not curved as in the case of a point source in free space, (see clause 6 ETR 273-1-1 [9]) but tends to be more linear with a tilt, relative to vertical, which is roughly equivalent to the angle at which a single source, placed midway between the real antenna on the mast and its image, would impinge on the receive aperture. If one were to impose, say, a phase variation across the receive aperture of no greater than 22,5°, the maximum size of an EUT would be much reduced (typically by a factor of at least 2) from the 0,4 to 0,6 wavelengths quoted, to a point where the test site would be virtually unusable at some frequencies.

5.2.3 Mutual coupling between antennas and in the ground plane

Mutual coupling is the mechanism which produces changes in the electrical behaviour of an EUT (or antenna) when placed close to a conducting surface, another antenna, etc. The changes can include detuning, gain variation and distortion of the radiation pattern.

To illustrate the effects of mutual coupling to the ground plane it is useful to start by considering the interaction between two closely spaced resonant dipoles in **free space** i.e. without a ground reflection. Some texts ("*Antenna theory*" [2]) show that in this condition, noticeable changes to a dipole's input impedance result for dipole to dipole spacing of up to 10 wavelengths (assuming side by side orientation).

In a transmit/receive system between two resonant dipoles the input impedance of the driven dipole (Z_{in1}) can be calculated as a combination of its own self impedance (Z_{11}), the self impedance of the other dipole (Z_{22}) and a contribution from the mutual interaction between them. The mutual interaction comprises both resistive (R_{12}) and reactive (X_{12}) components and the relationship between them can be show to be:

$$Z_{in1} = Z_{11} - \frac{(R_{12} + jX_{12})^2}{Z_{22}}$$

The variations with separation distance of the mutual resistance and reactance for two half wavelength dipoles are shown in figure 6.

EXAMPLE 1: If the range length is 3 m and the frequency is 30 MHz, from figure 6 R_{12} = 29,11 Ω and X_{12} = - 34,36 Ω. As a result, Z_{in1} = 88,32 + j 60,98 Ω whereas with no coupling it would be 73 + j 42,5 Ω.

EXAMPLE 2: The input impedance of the transmitting antenna for two half wavelength dipoles spaced half a wavelength apart, becomes 70 + j 30,5 Ω as a result of the mutual coupling.

Along with the change in input impedance arising from mutual coupling, there will be a signal strength loss due to the associated mismatch to the line. However, it is not only the dipole impedance that changes as a result of its proximity to another. The radiation pattern and gain (or antenna factor) will also change. Indeed, the gain change has been shown in "*Control of errors on Open Area Test Sites*" [7] to have an unexpected relationship with the radiation resistance - namely that their product remains constant no matter how much either quantity may vary. Specifically:

$$Gain = 120 / Resistance$$

As a result, for the first example above (30 MHz dipoles spaced 3 m apart) a gain loss of 0,83 dB occurs whilst for the second example of two dipoles half a wavelength apart an increase of 0,19 dB in the gain results. Simply increasing the range length to minimize mutual coupling, requires a receiver with sufficient sensitivity to cope with the increased path loss.

The magnitude of the effects on the electrical characteristics of the EUT or antenna due to the degree of mutual coupling between them are estimated in ETR 273-1-2 [10] annex A and the uncertainty contributions which result are given representative symbols as follows:

u_{j08} is used for the uncertainty contribution associated with the mutual coupling amplitude effect of the test antenna on the EUT in test methods;

u_{j09} is used for the uncertainty contribution associated with the de-tuning effect of the test antenna on the EUT in test methods;

u_{j10} is used for the uncertainty contribution associated with the mutual coupling between the transmitting antenna and the receiving antenna in the verification procedures;

u_{j11} is used for the uncertainty contribution associated with the mutual coupling between substitution or measuring antenna and the test antenna in test methods.

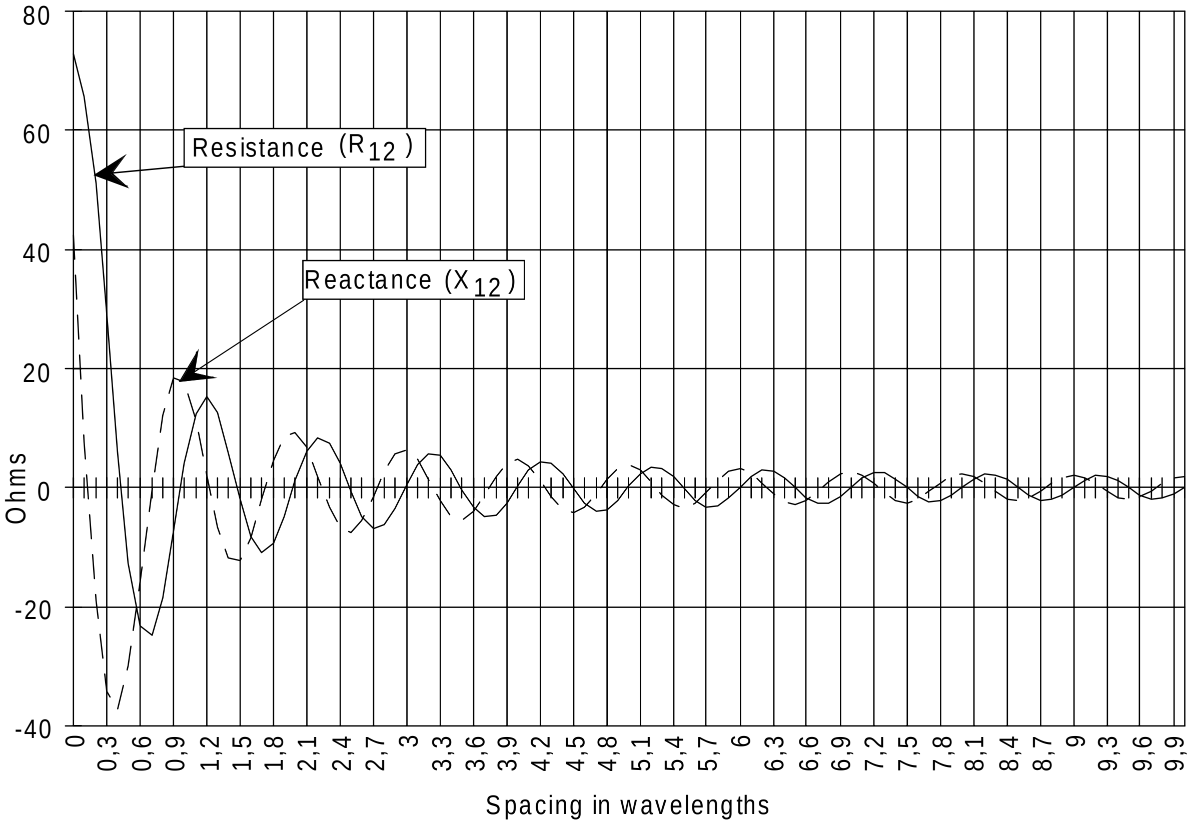

Figure 6: The mutual resistance and reactance of two side-by-side dipoles, each λ/2

Over a ground plane, this mutual coupling situation becomes further complicated by the creation of images of both antennas. Without giving a full analysis, it is indicative to look at the case of a single dipole and the effect its image (i.e. the presence of the ground plane) has on its performance. For this configuration, the orientation of the dipole is important. For a horizontal dipole, the input impedance can be shown to be:

$$Z_{in} = Z_{11} - Z_{12}$$

whereas for a vertical one,

$$Z_{in} = Z_{11} + Z_{12}$$

where $Z_{12} = R_{12} + jX_{12}$. Again, the gain of the dipole will change in line with its input resistance and for the worst case of a horizontal dipole, the variation in gain against height above the ground plane is given in figure 7. Even for a spacing above the ground plane of more than two wavelengths, the figure shows that the dipole's gain can vary by ± 0,5 dB with the ripple being slow to diminish even at spacing of five wavelengths.

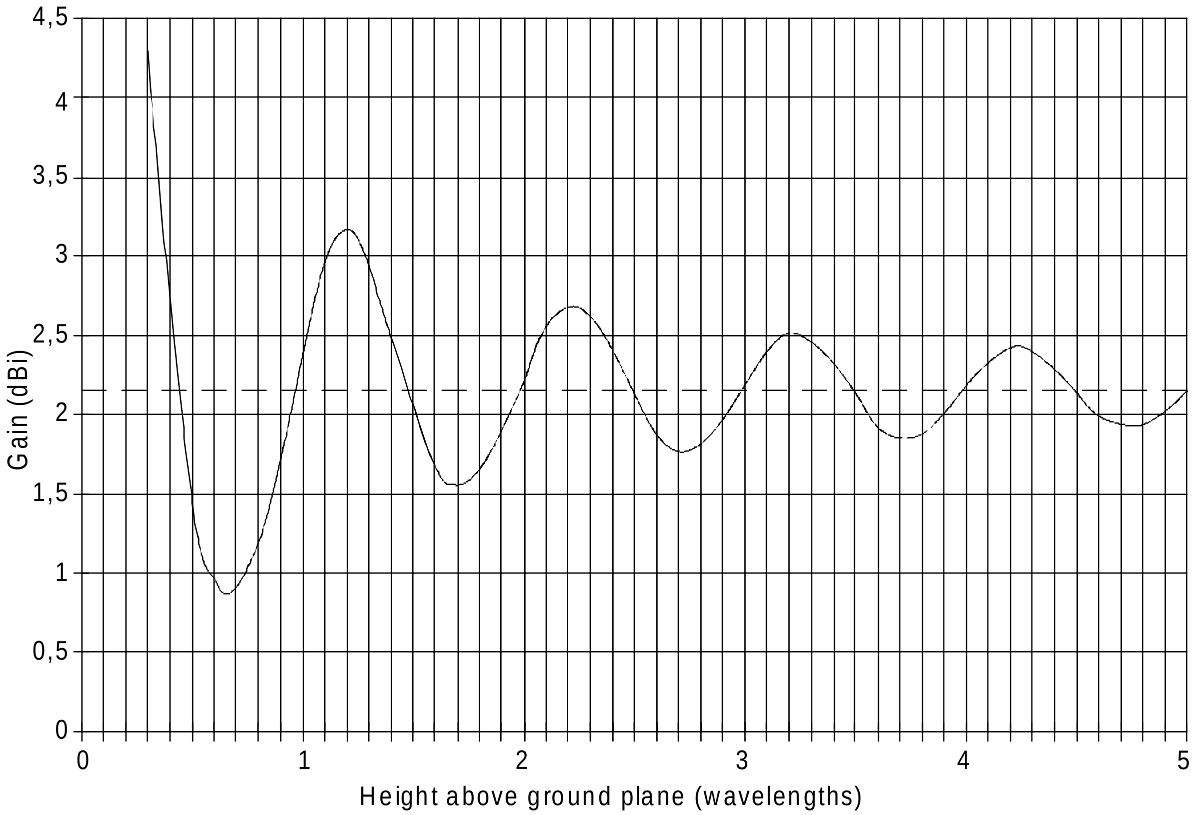

Figure 7: Gain variation of a horizontal half wavelength dipole above a ground plane

This real life testing situation is very much more involved than the theoretical coupled dipole examples given above since there is interaction not only between the transmitting and receiving devices and their own images (whether an EUT and antenna or two antennas) but also between each device and the image of the other and between images.

NOTE: The overall mutual coupling effect between two ANSI dipoles over a ground plane have been modelled and figures are provided as "Mutual coupling and mismatch loss" correction factors in the individual test procedures.

Furthermore, for an EUT, the magnitude of the overall effect will be dependant on its size, polarization, frequency, etc.

Mutual coupling to the ground plane for a typical test is illustrated in figure 8.

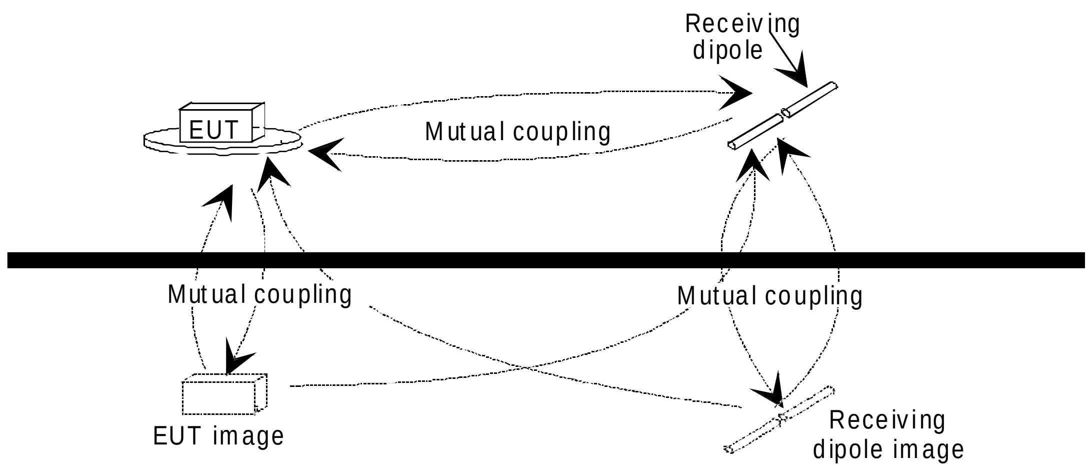

Figure 8: Mutual coupling in the ground plane

The magnitude of the effects on the electrical characteristics of an EUT or antenna due to the mutual coupling between them and/or the ground plane are estimated in ETR 273-1-1 [9] annex A and the uncertainty contributions which result are given representative symbols as follows:

u_{j12} is used for the uncertainty contribution associated with the interpolation of mutual coupling and mismatch loss correction factors (factors to allow for coupling between ANSI dipoles only).

u_{j13} is used for the uncertainty contribution associated with change in the gain/sensitivity of an EUT due to mutual coupling to its image in the ground plane in test methods;

u_{j14} is used for the uncertainty contribution associated with the change in gain/sensitivity of the substitution, measuring or test antenna to its image in the ground plane in test methods;

u_{j15} is used for the uncertainty contribution associated with the mutual coupling between the transmitting or receiving antenna and its image in the ground plane in verification procedures.

5.3 Other effects

5.3.1 Range length and measurement distance

Range length is defined as the horizontal distance between the phase centres (or volume centres) of the EUT and test antenna or between antennas. Measurement distance, on the other hand, is defined as the actual distance between the phase centres (or volume centres) of the EUT and test antenna. The distinction between the two parameters is illustrated in figure 9 where the test antenna is at 4 m.

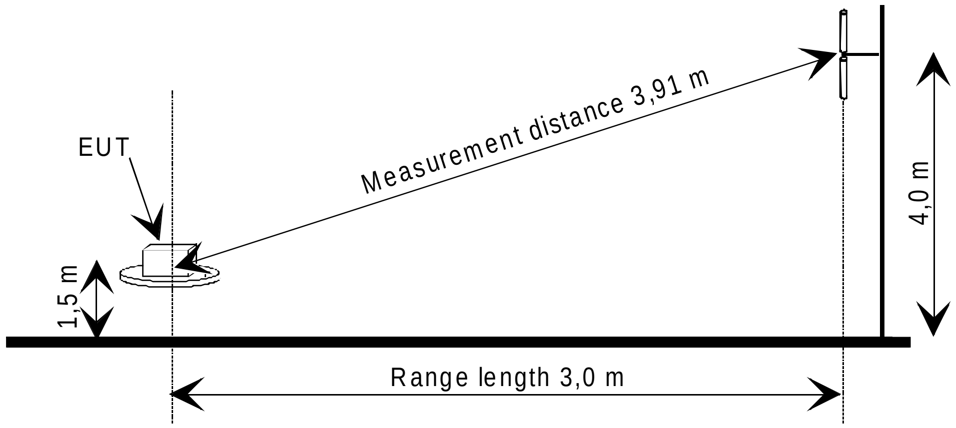

Figure 9: Range length and measurement distance

Measurement uncertainties are always encountered when measurements of any kind are made in the near-field. One of the main difficulties in testing is being able to define for an unknown emission, where the near-field conditions end and the far-field conditions start. There is a general zone, referred to as the transition zone, within which near-field or far-field conditions may exist, depending on the characteristics of the source.

In the near-field the electric and magnetic fields should be considered separately as the ratio of the two is not constant and, as a result, the wave impedance is not constant. In the far-field, however, they comprise a plane wave having an impedance of 377Ω. Therefore, when plane waves are discussed they are assumed to be in the far-field.

The range length over which any radiated test is carried out should always be adequate to enable far-field testing of the EUT i.e. range length should always be greater than or equal to:

$$\frac{2(d_1 + d_2)^2}{\lambda}$$

where:

d_1 is the largest dimension of the EUT/dipole after substitution (m);
d_2 is the largest dimension of the test antenna (m);
λ is the test frequency wavelength (m).

The uncertainty contribution which arises from the range length not satisfying the far-field range length is estimated in ETR 273-1-1 [9] annex A and is given the representative symbol as follows:

u_{j16} is used for the uncertainty contribution associated with the range length (when it does not meet the far-field requirement).

For distances equal to or less than $(d_1+d_2)^2/4\lambda$ the magnitude of the contribution is unspecified, since measurements should not be carried out at these separations (the uncertainty is too large).

The radiated test methods in this ETR all involve a substitution measurement. A substitution measurement always involves two stages. One stage is the measurement on the EUT, the other stage involves a similar measurement using a reference (normally a dipole) against which the first result can be compared and evaluated.

Complications arise when the radiated test is carried out over a reflective ground plane, since this requires the raising and lowering of the test antenna to maximize the received signal. Two uncertainties are introduced by this action.

The first uncertainty concerns the radiation pattern of the test antenna in the vertical plane. For a vertically polarized dipole, the directivity in the vertical plane means that the higher on the mast that the test antenna peaks, the larger the angle subtended to the device at the other end and hence the further down the side of the beam the illumination falls.

EXAMPLE 1: For a peak height of 1,5 m, the direct signal to the test device comes from the boresight of the beam, whereas for a peak height of 4 m, an angle of 39,8° is subtended over a 3 m range length. This corresponds to a fall off of 3,1 dB for a half wavelength dipole (see figure 10).

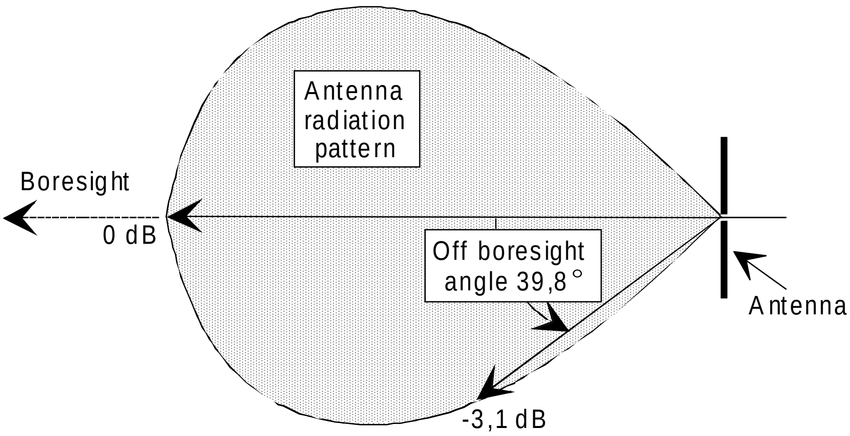

Figure 10: Signal loss due to off boresight angle

Whilst this is an over simplification of the case (no account has been paid to the reflected signal) nonetheless it illustrates the potential magnitude of the effect. It should be noted that this effect does not occur when dipoles or bicones are used in horizontal polarization. Corrections can be obtained for signal loss due to off boresight angles in the elevation plane (figure A.8 of ETR 273-1-1 [9]). There is, however, an uncertainty associated with this correction factor:

u_{j17} is used throughout all parts of ETR 273 for the uncertainty contribution associated with the correction factor for off boresight angle in the elevation plane due to signal attenuation with increasing elevation offset angle.

The second uncertainty is that a measurement distance error occurs when the peak position found on the mast during the substitution is at a different height to that for the measurement on the EUT.

EXAMPLE 2: Suppose a peak is found on the top of the mast (4,0 m) when measuring the EUT, (see figure 14), giving a measurement distance of 3,91 m. For the substitution measurement however the test antenna peaks at 1,5 m giving a measurement distance of 3,0 m. A graph is provided in ETR 273-1-2 [10] (figure A.7) for obtaining the correction to be applied.

There is, however, an uncertainty associated with this correction factor:

u_{j18} is used for the uncertainty contribution associated with the calculated correction factor for measurement distance.

5.3.2 Antenna mast, turntable and mounting fixtures

As the turntable and mounting fixtures are in close proximity to the EUT/antenna they can significantly change its performance. The antenna mast likewise for the test antenna. The antenna mast, turntable and mounting fixtures should, therefore, be constructed from non conducting, low relative dielectric constant plastics or wood to reduce reflections and interactions. Where wood is used, nails should not be used to join the sections - they should be jointed and glued. Table 1 gives examples of popularly used construction materials. It is recommended that materials with dielectric constants of less than 1,5 be used for all supporting structures.

Table 1: Dielectric data of constructional materials

Material	Dielectric constant	Frequency
Fibre Glass	4,8	100 MHz
Dry Oak	4,2	1 MHz
Douglas Fir	1,82	3 000 MHz
Balsawood	1,22	3 000 MHz
Polystyrene Foam	1,03	3 000 MHz
PTFE	2,1	3 000 MHz
Nylon	2,73	3 000 MHz

Wooden constructions needs to be protected, by some surface coating, from absorbing moisture. Either vanish or paint finishes can be used, but care should be exercised in selection so that low dielectric constant, low conductivity types are applied in order to minimize reflections.

The mast should be strong enough to raise and lower the antenna, its mount and feed cable. Its stability is an important aspect, particularly when the antenna is raised and lowered since it should do so in a straight vertical line. The rigidity of the antenna mast needs to be sufficient to prevent any angular errors in the pointing direction of the mounted antenna, in either horizontal or vertical planes, whatever load is placed on it. This is particularly important when tests are carried out on unprotected sites on windy days. Should the mast twist and the antenna's boresight be directed away from the EUT, then, unless the antenna's pattern is omni-directional in the horizontal plane, there will be an uncertainty in signal level. Similarly, should the antenna be deflected in the vertical plane, unless the pattern is omni-directional in that plane, the beam will either nod towards the ground (thereby increasing the ground illumination), or tilt upwards reducing the signal level directed at the EUT. This deflection will also change the measurement distance and additionally change the relative phasing of the direct and reflected signals (see figure 11).

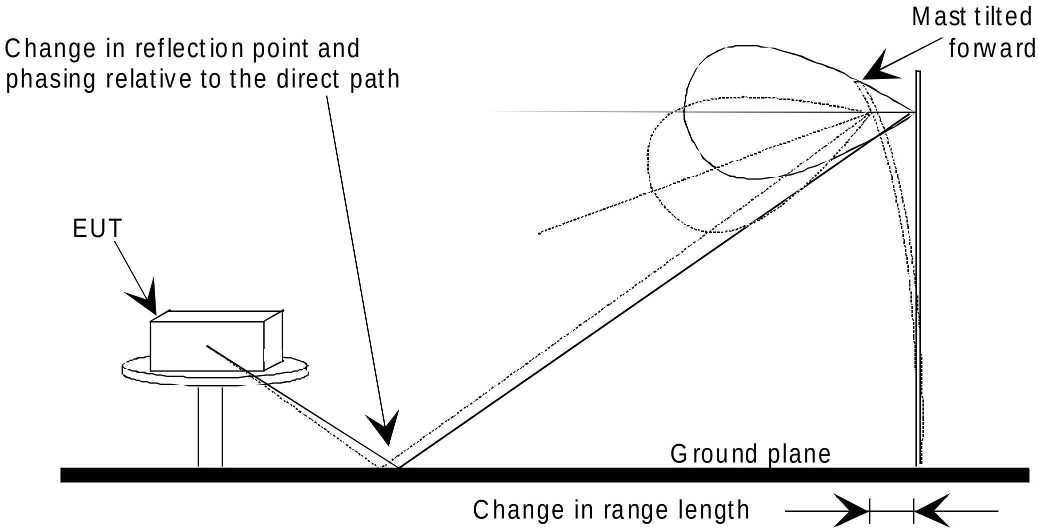

Figure 11: Mast stability

Similarly, if the antenna is allowed to rotate "off axis" due to a poorly anchored mast the signal level may also be reduced, see figure 12.

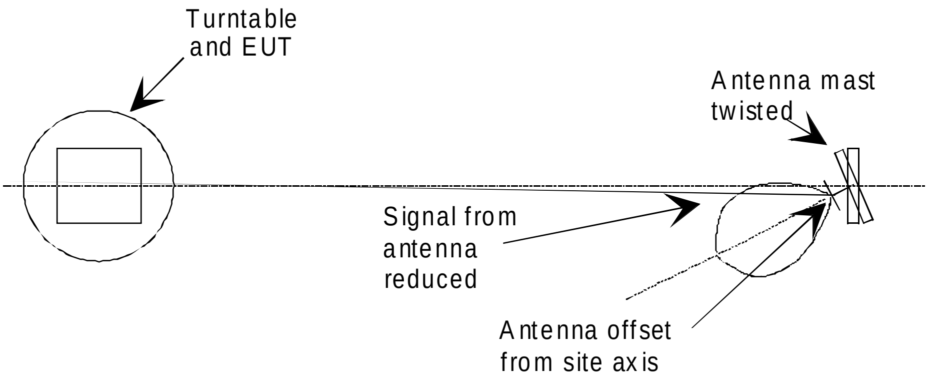

Figure 12: Signal reduction due to a twisted mast (plan view)

Accurate vertical positioning of the antenna is also important. The antenna supports should provide repeatable positioning and the limits of the weight capacities should not be exceeded. The stability of the turntable is important since an unstable, or non uniform turntable will also affect the measurement distance.

Controllers for both the mast and turntable should be carefully considered to avoid measurement uncertainties. For example, rapid changes in height or speed of rotation can lead to missing peak values. Settling times are important for measuring equipment. The controllers should, therefore, be designed with fixed, acceptable speeds which avoid these problems.

5.3.3 Test antenna height limitations

All tests on ground reflection sites are carried out so that the peak signal level is detected by varying the height of the antenna on the mast. For an EUT with an omni-directional pattern in the vertical plane above a **perfectly** conducting ground, theoretically, this peak for vertical polarization occurs on the surface of the ground plane. It is difficult to measure this precise peak with an antenna of any finite size although a fixed Monopole mounted on the ground plane could be used. Practically, this is not a viable solution and the antenna therefore has to be moved up the mast until the next peak in the vertical plane is located. With an upper limit of 4 m, the lowest frequency at which this next peak will appear on the mast is only achieved when the length of the reflected path is one wavelength longer than the direct path.

The situation regarding tests involving horizontal polarization is different since the phase of the ground reflection dictates a null appearing on the surface of the ground plane. To achieve a first peak on the mast for horizontal polarization therefore, the path difference between direct and reflected rays has only to be half a wavelength. Table 2 shows the lowest frequencies for different range lengths at which the difference in path lengths produces a peak on a mast offering a 1 to 4 m height scan.

Table 2: The lowest frequency at which a peak appears against range length

Range length (m)	Lowest frequency at which a peak appears on the 4 m mast (Vertical polarization)	Lowest frequency at which a peak appears on the 4 m mast (Horizontal polarization)
3,0	127,1 MHz	63,6 MHz
5,0	162,8 MHz	81,4 MHz
10,0	271,5 MHz	135,8 MHz
30,0	757,5 MHz	378,8 MHz
NOTE: The frequencies given in are, to an extent, dependant on the directivity of the antennas, but they are valid for the general case over a perfectly conducting ground plane. If the ground plane is not a perfect conductor these frequencies will differ.		

Taking the other extreme, when the source has high directivity (e.g. waveguide horn) and the angle of its first null (in the vertical plane) coincides with the angle of the reflected ray, the height of the maximum peak on the mast will be at the height of the source itself (usually 1,5 m) irrespective of polarization.

5.3.4 Test antenna cabling

There are radiating mechanisms by which RF cables can introduce uncertainties into radiated measurements:

- leakage;
- acting as a parasitic element to the test antenna;
- introducing common mode current to the balun of the test antenna.

Leakage allows electromagnetic coupling into the cables. Because the electromagnetic wave contains both electric and magnetic fields, mixed coupling can occur and the voltage induced is very dependant on the orientation, with respect to the cable, of the electric and magnetic fields. This coupling can have different effects depending on the length of the cable and where it is in the system. Cables are usually the longest part of the test equipment configuration and as such leakage can make them act as efficient receiving or transmitting antennas thereby contributing significantly to the uncertainty of a measurement.

The parasitic effect of the cable can potentially be the most significant of the three effects and can cause major changes to the antenna's radiation pattern, gain and input impedance. The common mode current problem has similar effects on the antenna's performance.

All three effects can be largely eliminated by routeing and loading the cables with ferrite beads as detailed in the test methods. A cable for which no precautions have been taken to prevent these effects can cause different results to be obtained simply by being repositioned.

u_{j19} is used for the uncertainty contribution associated with cable factor (the combined uncertainty which results from interaction between any antenna and its cable).

5.3.5 EUT supply and control cabling

EUT cable layout can contribute significantly to the uncertainty of the measurement. Large variations can occur when measuring spurious emissions for example, as a result of the positions of the supply and control cables.

These cables can act as parasitic elements and can receive radiated fields. The effects vary with cable type, the configuration and use, but they may strongly influence the outcome of a measurement. A number of schemes can be used to reduce these problems, amongst which are a total replacement by fibre optic cables and twisting wires together and loading them with ferrite beads.

u_{j55} is used for the uncertainty contribution which results from interaction between the EUT and the power leads.

5.3.6 Positioning of the EUT and antennas

The phase centre of an EUT or an antenna is the point within the EUT or antenna from which it radiates. If the EUT or antenna was rotated about this point, the phase of the received/transmitted signal would not change. For some test procedures, especially those which require an accurate knowledge of the measurement distance, it is vital to be able to identify the phase centre.

Where an EUT is being tested the uncertainty in the position of the phase centre of the source within the EUT volume can lead to signal level uncertainties since all calculations deriving emission levels will be based on the precise measurement distance.

u_{j20} is used for the uncertainty contribution associated with not knowing the exact position of the phase centre within the EUT volume in test methods.

The positioning, on the turntable, of the phase centre of the EUTs radiating source, can lead to uncertainties if it is offset from the tables axis of rotation. Any offset will cause the source to describe a circle about the axis as the EUT is rotated. Variations in path lengths (both direct and reflected) are thereby introduced leading directly to changes in the received/transmitted field strength.

u_{j21} is used for the uncertainty contribution associated with the positioning of the phase centre within the EUT over the axis of rotation of the turntable in test methods.

Dipoles and bicones have phase centres at their feed points, whilst that for a waveguide horn is in the centre of its open mouth. The phase centres do not change with frequency for these antennas.

u_{j22} is used for the uncertainty contribution associated with the position of the phase centre of the measuring, substitution, receiving, transmitting or test antenna.

Certain antennas, most notably the LPDA, possess a phase centre which is difficult to pin point at any particular frequency. Further, for this type of antenna the phase centre moves along the array with changing frequency resulting in a measurement distance uncertainty (e.g. an LPDA with a 0,3 m length contributes a standard uncertainty level due to range length uncertainty of u_j = 1,0 dB). To use such an antenna for site calibration, for example, could introduces large uncertainties.

u_{j23} is used for the uncertainty contribution associated with the position of the phase centre for LPDAs.

5.3.7 Electromagnetic environment

On a typical open area test site, ambient RF interference can add considerable uncertainty to the measurements. Such ambient interference can be from continuous sources e.g. commercial radio and television, link services, navigation etc. or intermittent ones e.g. CB, emergency services, DECT, GSM, paging systems, machinery and a variety of other sources (see figure 13). The interference can be either narrowband or broadband. Power and telephone lines can produce radiated noise, as can large machinery (e.g. lathes, etc.) in nearby premises. Nearby railway tracks (particularly electric) are other sources. All these noise sources add to the general background levels which can disturb measurements.

Where possible, an open area test site should be located in an area having low levels of radiated ambient signals and, for minimum uncertainty, emission tests on an EUT should be carried out at a time when the level of ambient signals does not exceed a certain specified level with respect to the maximum emission limits from the EUT (usually taken as 6 dB below). On a test site with high levels of these interference sources, it may be possible to choose a time slot for testing when the overall RF environment does meet the requirement as a result of the sources not being continuously active for 24 hours a day.

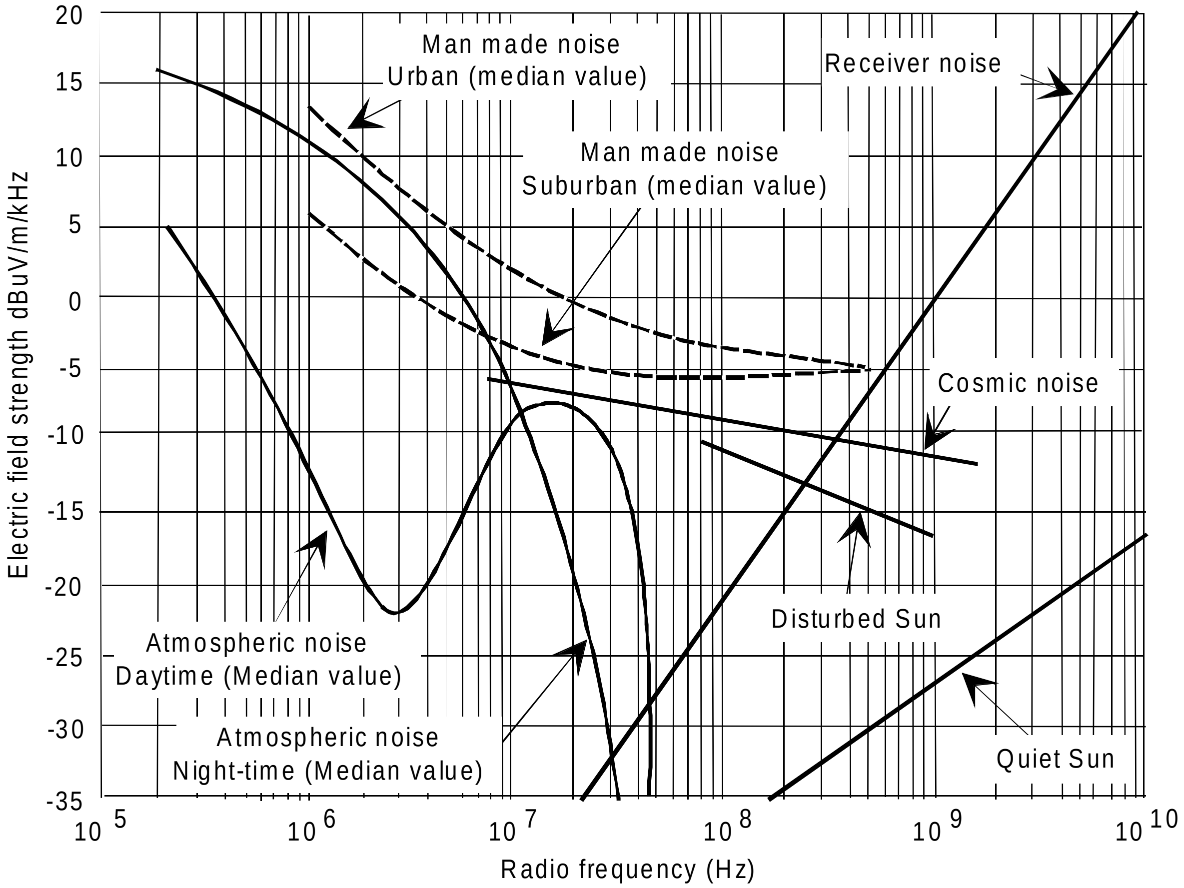

Figure 13: Electromagnetic noise sources and levels

More generally, spurious emission tests may be required from an open area test site for which the RF environment may not fully satisfy the ambient level requirements. In these cases, it is often helpful to perform preliminary tests within a shielded environment to identify which frequencies are radiated from within the EUT (a process termed "characterization"), without measuring their precise levels. Moving to the open area test site, the receiver system can be set up to these frequencies only, thereby avoiding the necessity of having to prove that every ambient does not originate from the EUT.

Whether the specified level of ambient signals is achieved or not, should the frequency of any particular ambient coincide exactly with an emission from an EUT, then the measured level of that emission will be in error, potentially putting the EUT outside its specification. In such cases, it may be possible to calculate a level for the emission by assuming that it adds, in phase, to the ambient. This is an assumption however and the resulting value possesses an associated uncertainty. Shortening the distance between the EUT and the measuring antenna can enhance the level of the emission with respect to the ambient although, should the near-field be entered, then the measurement will be further subjected to those uncertainties associated with the near-field. Within this ETR:

u_{j34} is used for the uncertainty contribution which results from local ambient signals raising the noise floor at the test frequency.

5.3.8 Extraneous reflections

Whilst an ideal open area test site should be completely clear of any possible reflecting objects, this is not very realistic in practise and items such as trees, buildings, movements of people, etc. will always be in the vicinity. Care should therefore be taken to ensure that the effects of such objects do not disturb the uniformity of the transmitted fields. Table 3 shows how much the received signal level can vary as a result of a single interfering signal.

Table 3: Uncertainty in received signal level due to a single unwanted interfering signal

Ratio of unwanted to wanted signal level	Received level uncertainty	Ratio of unwanted to wanted signal level	Received level uncertainty
- 30,0 dB	+0,27 -0,28 dB	- 9,0 dB	+2,64 -3,81 dB
- 25,0 dB	+0,48 -0,50 dB	- 8,0 dB	+2,91 -4,41 dB
- 20,0 dB	+0,83 -0,92 dB	- 7,0 dB	+3,21 -5,14 dB
- 17,5 dB	+1,09 -1,24 dB	- 6,0 dB	+3,53 -6,04 dB
- 15,0 dB	+1,42 -1,70 dB	- 5,0 dB	+3,88 -7,18 dB
- 14,0 dB	+1,58 -1,93 dB	- 4,0 dB	+4,25 -8,66 dB
- 13,0 dB	+1,75 -2,20 dB	- 3,0 dB	+4,65 -10,69 dB
- 12,0 dB	+1,95 -2,51 dB	- 2,0 dB	+5,08 -13,74 dB
- 11,0 dB	+2,16 -2,88 dB	- 1,0 dB	+5,53 -19,27 dB
- 10,0 dB	+2,39 -3,30 dB	0,0 dB	+6,04 -∞ dB

Since the magnitude of the field scattered from an object depends on many factors such as the object's size, its distance from the EUT, conductivity, permeability, permittivity, frequency, etc., it is not possible to specify a minimum obstruction-free area that is appropriate for all applications. The size and shape of the obstruction-free area is also dependant on whether or not the EUT will be rotated.

In practice, the creation of a stipulated obstruction-free zone has the added benefit of preventing any possible interference from people, cars, stored objects etc. This area should also be kept clear of accumulated litter and other objects capable of disturbing the generated fields. A past recommendation of the IEC was for a circular obstruction-free zone of diameter equal to eight times the range length on the basis that if all the energy were reflected back coherently from the boundary, the path loss involved would not allow the measurement uncertainty to exceed ± 1 dB. This size of clear area is only practical in a few cases.

An alternative scheme, proposed by ANSI, is to make the obstruction free area large enough so that the path length of a ray which hits a reflecting object on the boundary and is then received should be twice the direct path length. This ensures the magnitude of the reflection is attenuated by 6 dB compared to the direct ray.

Generally, actual obstructions only intercept a small portion of the energy and tend to scatter only a part of that back to the receiver. At low frequencies, therefore, small objects will have negligible effects. Above 1 GHz, and particularly towards the top end of the frequency band (12,75 GHz), even small objects can cause problems, however. Site verification procedures should be able to identify these and result in their removal.

The effects of trees have been looked at, "*Control of errors on Open Area Test Sites*" [7], and the results indicate that vertical polarization is effected more than horizontal. The tests were limited to a band of 30 MHz to 200 MHz and indicate that for trees 10 m away from the receiver, virtually no effects are observable. Site verification procedures should again prove helpful in determining tree effects at other frequencies, particularly those above 1 GHz.

A shielded room can be used for housing the test equipment and recording the test results and, from the point of view of cable loss and convenience, it is advisable to have this facility close to the test site. To prevent this room being a reflection source, it should be under the ground plane. If the site cannot be constructed in this fashion, the metallised room may cause reflection errors to be present during measurements. Alternatively a wooden or plastic hut could be used to reduce the reflection problems but it may allow radiated fields to permeate the test gear. Equally radiated signals generated by the test gear could produce additional ambient signals. Either way, an increase in measurement uncertainty is likely to result.

The presence of overhead power and telephone lines can cause reflections, particularly for horizontal polarization. Where these lines are services to the site they should be buried under the ground plane. External lines (national grids and national telephone lines) however, cannot be dealt with in this fashion. Railway lines are a slightly different problem in that, whilst the lines themselves are probably only minor sources of reflection, the passage of the trains and carriages can significantly disturb the test fields if they pass close to the test site. The effects of car and lorry traffic on roads running nearby test sites will be similar. Aircraft, particularly low flying military ones, can produce a momentary reflection, but in general, the path lengths involved will attenuate the magnitude to a very low level. The main problem with aircraft results from emissions of the "on board" avionics systems.

The open area test site may have to have a weather protective enclosure if it is to be used throughout the year in areas which experience unsettled weather. The protective enclosure may be constructed over part, or all of, the site. The RF transparency of materials being considered for permanent structures should be evaluated and the use of metal (for fixtures and fittings) above the ground plane should be avoided. In general, should metal objects be necessary, they should have dimensions of less than a tenth of a wavelength at the highest frequency of operation. The structure should additionally be shaped to allow for the easy removal of snow, ice or water. Such test sites employing "reflection-free" skins needs to have routine cleaning of the outer skin to prevent a build up of dirt, dust, etc., which could, if allowed to accumulate, become a reflection source.

6 Verification procedure for an open area test site

6.1 Introduction

The verification procedure is a process carried out on all open area test sites, Anechoic facilities (both with and without a ground plane) and Striplines to prove their suitability as free field test sites.

Anechoic facilities and open area test sites

For both types of Anechoic facility and **open area test site**s the procedure involves the transmission of a known signal level from one calibrated antenna (usually a dipole) and the measurement of the received signal level in a second calibrated antenna (also usually a dipole).

By comparison of the transmitted and received signal levels, an "insertion loss" can be deduced. After inclusion of any correction factors to the measurement, the figure of loss which results from the verification p rocedure, is known as "site attenuation".

Site attenuation is defined in "Fifth edition, IEEE Piscataway" [12] as: "The ratio of the power input of a matched, balanced, lossless, tuned dipole radiator to that at the output of a similarly matched, balanced, lossless, tuned dipole receiving antenna for specified polarization, separation and heights above a flat reflecting surface. It is a measure of the transmission path loss between two antennas".

As the definition states ".... above a flat reflecting surface", it is usual for the verification procedure to involve one antenna (the transmitting antenna) remaining fixed in height whilst a second antenna (the receiving antenna) is scanned through a specified height range looking for a peak in the received signal level.

The determination of site attenuation involves two different measurements of received signal level. The first is with all the items of test equipment connected directly together via an adapter, whilst the second involves the coaxial cables being connected to the antennas. The difference in received levels (after allowance for any correction factors which may be appropriate), for the same signal generator output level, is the site attenuation.

The verification procedure for an open area test site is based on EN 50147-2 [8], which itself is based on CISPR 16-1 [6], subclauses 15.4 to 16.6.3 inclusive. Both procedures call for the determination of Normalized Site Attenuation (NSA) which is equivalent to site attenuation after subtraction of the antenna factors. It should be noted that both publications EN 50147-2 [8] and CISPR 16-1 [6] only detail verification procedures in the 30 MHz to 1 000 MHz frequency band.

6.2 Normalized site attenuation

NSA is determined from the value of site attenuation by subtraction of the antenna factors and mutual coupling effects. The subtraction of the antenna factors makes NSA independent of antenna type.

NOTE: The uncertainty of the resulting value for NSA depends directly on the uncertainty with which the antenna factors are known.

Symbolically,

$$NSA = V_{direct} - V_{site} - AF_T - AF_R - AF_{TOT}$$

where: V_{direct} = received voltage for cables connected via the "in-line" adapter;
V_{site} = received voltage for cables connected to the antennas;
AF_T = antenna factor of the transmit antenna;
AF_R = antenna factor of the receive antenna;
AF_{TOT} = mutual coupling correction factor.

The verification procedure compares the measured NSA (after relevant corrections) against the theoretical figure calculated for an ideal open area test site. The difference between the two figures, when taken over the full range of frequencies for which the site is to be used, is a measure of the quality of the test facility.

In general, ANSI and CISPR consider a test site suitable for making measurements (both relative and absolute) if the measured normalized site attenuation differs by less than ± 4 dB (throughout the entire frequency range) from the theoretical values. However, for any absolute field strength measurements carried out on that test site, this magnitude of the difference would be automatically added to the uncertainties of the measurement.

The relevant theory for deriving the NSA of an ideal open area test site is given below and begins with analysis of an anechoic chamber whose six internal surfaces are covered with absorbing material.

6.2.1 Anechoic chamber

In an ideal anechoic chamber where there are:

- no unwanted reflections (ground reflected or others);
- no interaction between transmit and receive dipoles;
- no coupling of the dipoles to the absorbing material;
- and where perfectly aligned, loss-less, matched tuned dipoles are used.

The coupling between the dipoles (which are assumed to be half wavelength) is given by the Friis transmission equation (as derived in clause 7 of ETR 273-1-1 [9]):

$$P_{rec} = \left(\frac{\lambda}{4\pi d}\right)^2 1{,}643^2 \left(\frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta}\right)^2 \left(\frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta}\right)^2 P_t$$

where: P_t = power transmitted (W);
P_{rec} = power received (W);
λ = wavelength (m);
d = distance between dipoles (m),

and θ is a spherical co-ordinate, as shown in figure 14.

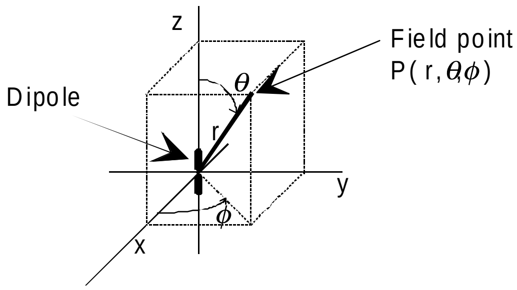

Figure 14: Spherical co-ordinates

For this ideal site, the site attenuation (the inverse of the Friis transmission equation) is given by:

$$\frac{P_t}{P_{rec}} = \left(\frac{4\pi d}{\lambda}\right)^2 \frac{1}{1{,}643^2} \left(\frac{\sin\theta}{\cos\left(\frac{\pi}{2}\cos\theta\right)}\right)^2 \left(\frac{\sin\theta}{\cos\left(\frac{\pi}{2}\cos\theta\right)}\right)^2$$

More usually, this formula is given in logarithmic (dB) terms as follows:

$$Site\ Attenuation = 17{,}67 + 20\log\left(\frac{d}{\lambda}\right) + 20\log\left(\frac{\sin\theta}{\cos\left(\frac{\pi}{2}\cos\theta\right)}\right) + 20\log\left(\frac{\sin\theta}{\cos\left(\frac{\pi}{2}\cos\theta\right)}\right)\ \mathrm{dB}$$

Since both transmit and receive antennas are assumed to be at the same height, $\theta=\pi/2$ and the formula reduces to:

$$site\ attenuation = 17{,}67 + 20\ log\ (d/\lambda)\ \mathrm{dB}$$

NOTE 1: In an actual measurement, the value of site attenuation is likely to be greater than given by this formula due to mismatch and resistive losses, mutual coupling effects, etc.

An alternative formulation for site attenuation, based on field strength (V/m) and antenna factors has been derived in EMC Vol. EMC 24 [3]. The resulting formulae are for use with ground reflection sites but they are easily adapted for the fully anechoic chamber.

The general formula given in EMC Vol. EMC 24 [3] for site attenuation, A, is:

$$A = \frac{279{,}1\ AF_T\ AF_R}{f_m E_{D(H\ or\ V)}^{\max}}$$

where: AF_T = antenna factor of the transmitting antenna (m^{-1});
AF_R = antenna factor of the receiving antenna (m^{-1});
f_m = frequency (MHz); and
$E_{D(H\ or\ V)}^{\max}$ = calculated maximum electric field strength (µV/m) in the receiving antenna height scan from a half wavelength dipole with 1 pW of radiated power;
$E_{D(H\ or\ V)}^{\max}$ = takes the form $E_{DH}^{\max}$ for horizontal polarization and $E_{DV}^{\max}$ for vertical polarization.

NOTE 2: The stipulations of a half wavelength dipole and 1 pW of radiated power in $E_{D\ (H\ or\ V)}^{max.}$ do not limit the use of the site attenuation equation to those conditions. The definition of $E_{D\ (H\ or\ V)}^{max.}$ in the text of [19] is for convenience only and the stipulated conditions cancel out in the final formulas for site attenuation and normalized site attenuation, both of which apply generally.

For the fully anechoic chamber, $E_{D(H\ or\ V)}^{max}$ (a term whose amplitude is generally peaked on a ground reflection range by height scanning on a mast) is simply replaced by $E_{D(H\ or\ V)}$ since no maximization is involved and both polarizations behave similarly. $E_{D(H\ or\ V)}$ can be shown to be:

$$E_{DH} = E_{DV} = 7{,}01/d$$

In decibel terms, the site attenuation formula becomes:

$$A = 48{,}92 + 20\log(AF_T) + 20\log(AF_R) - 20\log f_m - 20\log(7{,}01/d)\ \text{dB}$$

The formula for NSA then follows as:

$$NSA = A - 20\log(AF_T) - 20\log(AF_R)\ \text{dB}$$

$$\textit{i.e.}\qquad NSA = 48{,}92 - 20\log f_m - 20\log(7{,}01/d)\ \text{dB}$$

6.2.2 Open area test site

The formula for $E_{D(H\ or\ V)}$ in the site attenuation equation for the fully anechoic chamber, given above, is only applicable if no reflections (ground or otherwise) are present. For the open area test site the formula has to be modified to take the ground reflection into account. However, this situation is further complicated by:

- the ground reflected ray suffering a phase reversal at the metal/air boundary for the horizontally polarized case (vertically polarized signals suffer no phase change); and

- the radiation pattern of the dipole, (which is omni-directional in the H-plane and directional in the E-plane), resulting in received amplitudes which change with off-boresight angles in the E-plane for vertical polarization. This does not occur in the horizontally polarized case.

As a result, different formulae apply for horizontal and vertical polarizations and these are now derived. For both polarizations however, the basic formula for site attenuation remains as:

$$A = \frac{279{,}1\, AF_T\, AF_R}{f_m\, E_{D(H\ or\ V)}^{max}}$$

For the horizontal polarization case of the formula, the term $E_{D(H\ or\ V)}^{max}$ on an ideal open area test site using dipoles and optimized over the height scan range, is EMC Vol. EMC 24 [3]:

$$E_{DH}^{max} = \frac{7{,}01}{d_{dir} d_{refl}} \sqrt{d_{refl}^2 + |\rho_H|^2 d_{dir}^2 + 2 d_{dir} d_{refl} |\rho_H| \cos\left(\phi_H - \beta\left(d_{refl} - d_{dir}\right)\right)}$$

where: $$\rho_H = \frac{\sin\gamma - \left(K - j60\lambda\sigma - \cos^2\gamma\right)^{\frac{1}{2}}}{\sin\gamma + \left(K - j60\lambda\sigma - \cos^2\gamma\right)^{\frac{1}{2}}} = |\rho_H| e^{j\phi_H}\ ;$$

d_{dir}	= path length of the direct signal (m);	d_{refl}	= path length of the reflected signal (m);
β	= 2π/λ (radians/m);	K	= relative dielectric constant;
σ	= conductivity (Siemens/m);	ϕ_H	= phase angle of reflection coefficient;
γ	= incidence angle with ground plane.		

For a perfectly reflecting metallic ground plane, $|\rho_H|$=1,0 and $|\phi_H|$= 180°. As a result, the formula for $E_{DH}{}^{\max}$ reduces to:

$$E_{DH}{}^{\max} = \frac{7{,}01\sqrt{d_{refl}{}^2 + d_{dir}{}^2 - 2d_{dir}d_{refl}\cos\beta\left(d_{refl} - d_{dir}\right)}}{d_{dir}d_{refl}}$$

Figure 15 shows the geometry for horizontally polarized tests using dipoles above a reflecting surface.

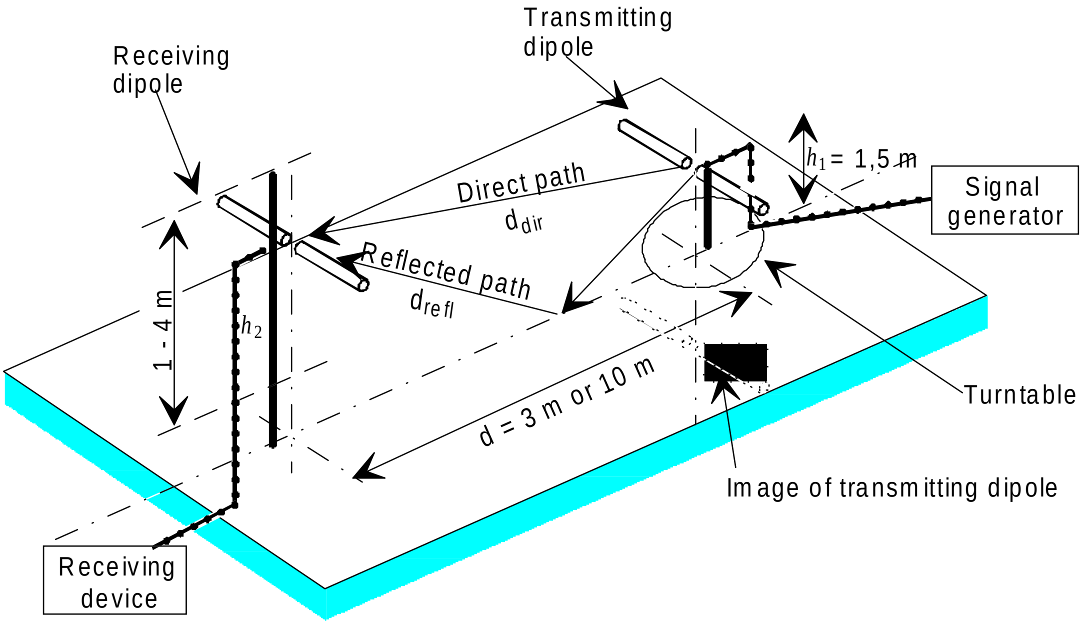

Figure 15: Ground reflection test site layout for horizontally polarized verification using dipoles

From figure 15 it can be seen that:

$$d_{dir} = \sqrt{(h_2 - h_1)^2 + d^2} \text{ and } d_{refl} = \sqrt{(h_1 + h_2)^2 + d^2}$$

For vertical polarization, a similar procedure is used to find $E_{DV}{}^{\max}$. However, in the vertical case, off boresight angles of incidence, shown in figure 16 introduce additional terms.

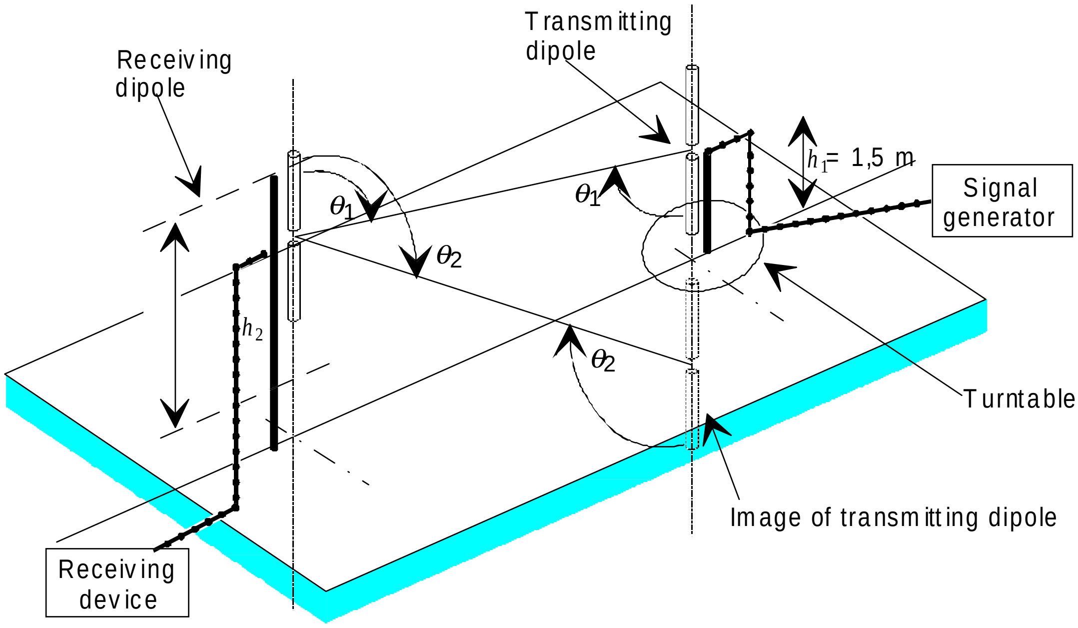

Figure 16: Off-boresight angles involved in verification using vertical polarization

This off boresight angle effect is accounted for in EMC Vol. EMC 24 [3] by giving the dipoles a "sin θ" pattern in the E-plane (the vertical plane as shown in figure 16).

Geometrically,

$$\sin\theta_1 = \frac{d}{d_{dir}} \quad \text{and} \quad \sin\theta_2 = \frac{d}{d_{refl}}$$

and incorporating these into the calculation of $E_{DV}{}^{max}$, optimized over the height scan range, produces:

$$E_{DV}{}^{max} = \frac{7{,}01\,d^2}{d_{dir}{}^3 d_{refl}{}^3}\sqrt{d_{refl}{}^6 + d_{dir}{}^6|\rho_V|^2 + 2d_{dir}{}^3 d_{refl}{}^3|\rho_V|\cos\left(\phi_V - \beta\left(d_{refl} - d_{dir}\right)\right)}$$

where:

$$\rho_V = \frac{(K - j60\sigma)\sin\gamma - \left(K - j60\lambda\sigma - \cos^2\gamma\right)^{\frac{1}{2}}}{(K - j60\sigma)\sin\gamma + \left(K - j60\lambda\sigma - \cos^2\gamma\right)^{\frac{1}{2}}} = |\rho_V|e^{j\phi_V}$$

For a perfectly reflecting metallic ground plane, $|\rho_V|$=1,0 and ϕ_V = 0°. As a result, the formula for $E_{DV}{}^{max}$ reduces to:

$$E_{DV}{}^{max} = \frac{7{,}01\,d^2}{d_{dir}{}^3 d_{refl}{}^3}\sqrt{d_{refl}{}^6 + d_{dir}{}^6 + 2d_{dir}{}^3 d_{refl}{}^3\cos\beta\left(d_{refl} - d_{dir}\right)}$$

It is important, on ground reflection sites, to state again that the received signal level needs to be peaked by varying the height of the receive antenna on the antenna mast (usually from 1 to 4 m) for these formulae to be used correctly.

6.2.3 Improvements to the formulae for E_{DH}^{max} and E_{DV}^{max}

In the verification procedure for an open area test site, the performance is measured for a number of transmitting dipole positions within a specified volume. This results in several positions for which off-boresight angles of incidence occur. As a consequence, the formula for E_{DH}^{max} has to be modified. However, so too does E_{DV}^{max} since the angles involved are no longer simple as considered above but are compound.

Further modifications to the formulae for E_{DH}^{max} and E_{DV}^{max} have also been made to more accurately represent the patterns of the dipoles. A better approximation to the nearly half wavelength dipoles of:

$$\frac{\cos\left(\frac{\pi}{2}\cos(\theta)\right)}{\sin\theta}$$

has been used, resulting in the following formulae.

For horizontal polarization:

$$E_{DH}^{max} = \frac{7{,}01}{YZ}\sqrt{d_{dir}^2 Z^2 \cos^4\alpha_1 + d_{refl}^2 Y^2 \cos^4\alpha_2 - 2 d_{dir} d_{refl} YZ \cos^2\alpha_1 \cos^2\alpha_2 \cos\beta\left(d_{refl} - d_{dir}\right)}$$

where $\alpha_1 = \frac{\pi}{2}\frac{y_{offset}}{d_{dir}}$ (radians), where y_{offset} is given in figure 17;

$\alpha_2 = \frac{\pi}{2}\frac{y_{offset}}{d_{refl}}$ (radians);

$Y = d_{dir}^2 - y_{offset}^2$ (m^2);

$Z = d_{refl}^2 - y_{offset}^2$ (m^2).

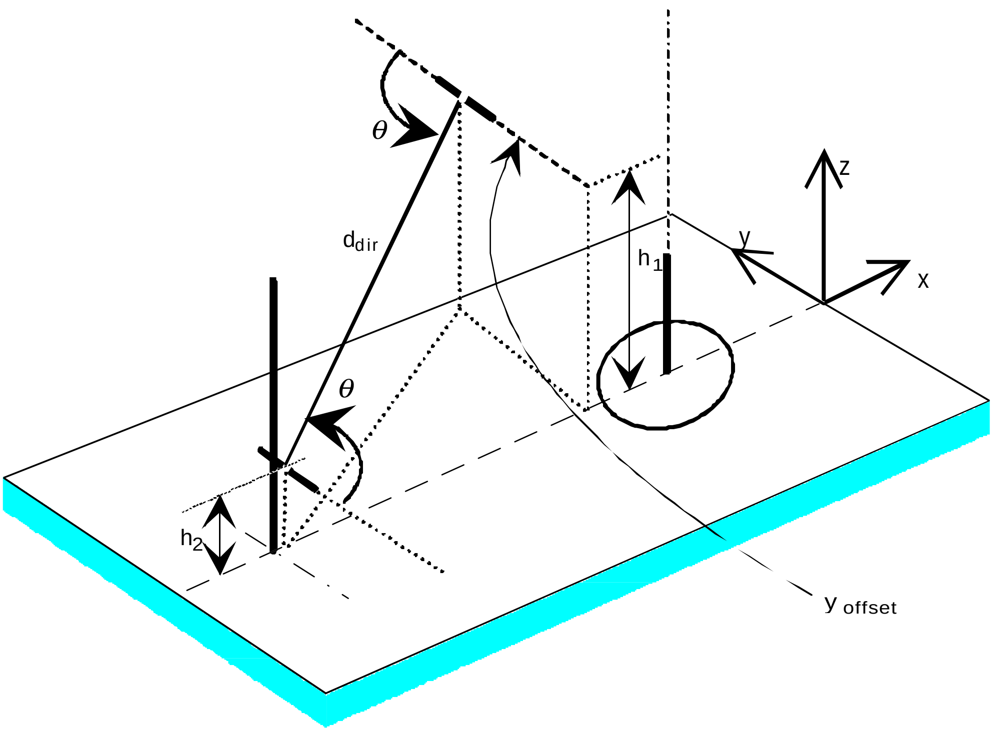

Figure 17: Geometry of the verification set-up for horizontal polarization

For vertical polarization, a similar procedure results in:

$$E_{DV}{}^{\max} = \frac{7{,}01}{D}\sqrt{d_{dir}{}^2 \cos^4 \delta_1 + d_{refl}{}^2 \cos^4 \delta_2 + 2 d_{dir} d_{refl} \cos^2 \delta_1 \cos^2 \delta_2 \cos\beta\left(d_{refl} - d_{dir}\right)}$$

where $\delta_1 = \frac{\pi}{2}\frac{(h_2 - h_1)}{d_{dir}}$ (radians); $\delta_2 = \frac{\pi}{2}\frac{(h_2 + h_1)}{d_{refl}}$ (radians);

and $D = d^2 + y_{offset}{}^2$ (m^2).

To derive NSA, these figures (maximized within the height scan limits) are inserted into:

$$NSA = 20\ \log\left(\frac{279{,}1}{f_m\, E_{D(H\ or\ V)}{}^{\max}}\right)\ \text{dB}$$

i.e.: $NSA = 48{,}92 - 20\log f_m - 20\ \log E_{D(H\ or\ V)}{}^{\max}$ dB

It is this formula for NSA which has been used to calculate the performance of an ideal open area test site against which the measured results of the verification procedure are compared.

6.2.4 Mutual coupling

Mutual coupling may exist between the antennas during the verification procedure. This will serve to modify the results since it can change input impedance/voltage standing wave ratio, radiation patterns and gain/antenna factors of both dipoles.

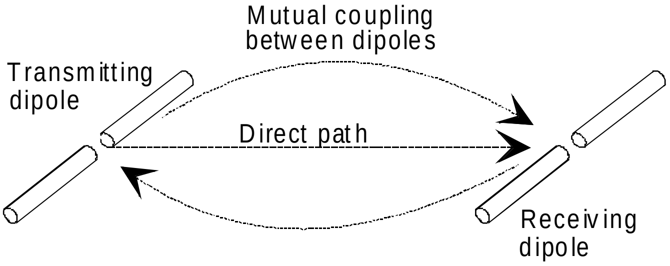

Figure 18: Direct path and mutual coupling

Figure 18 shows schematically mutual coupling as it occurs between dipoles in a reflection-free environment (i.e. an ideal anechoic chamber).

The situation is more complex for the open area test site, since the ground plane acts like a mirror, imaging each dipole in the ground. Because of this imaging there are, in effect, four dipoles to be considered. The transmitting dipole "sees" its own image in the ground as well as the real receiving dipole and its image. Similarly, the receiving dipole "sees" its own image in the ground along with the transmitting dipole and its image. Mutual coupling can exist between all these dipoles, whether real or imaginary. This is shown in figure 19b alongside the ideal model in figure 19a.

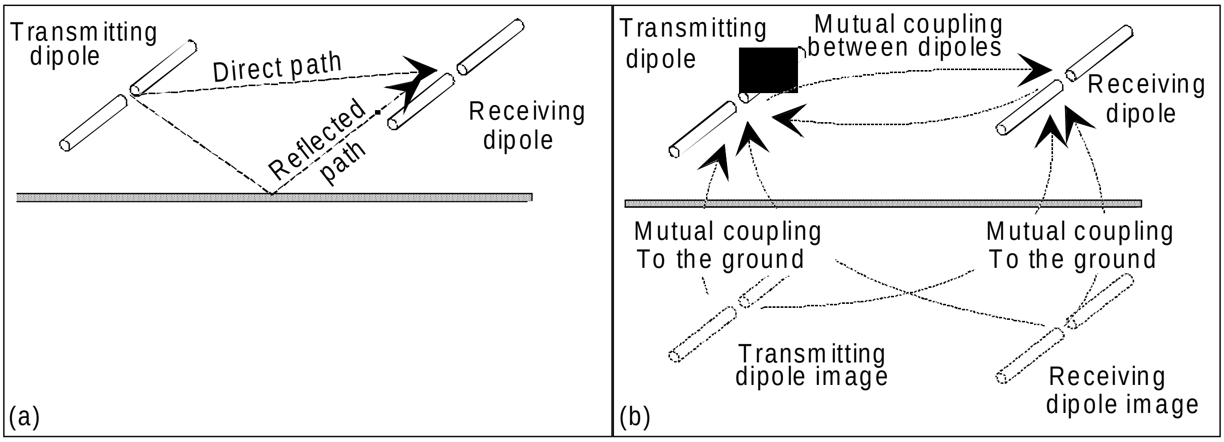

Figure 19: (a) Ideal model of an open area test site and (b) Mutual coupling effects on a real site

A further complication is that for fixed geometries the mutual coupling effects vary with frequency. The actual situation when horizontally polarized NSA is measured is shown schematically in figure 20.

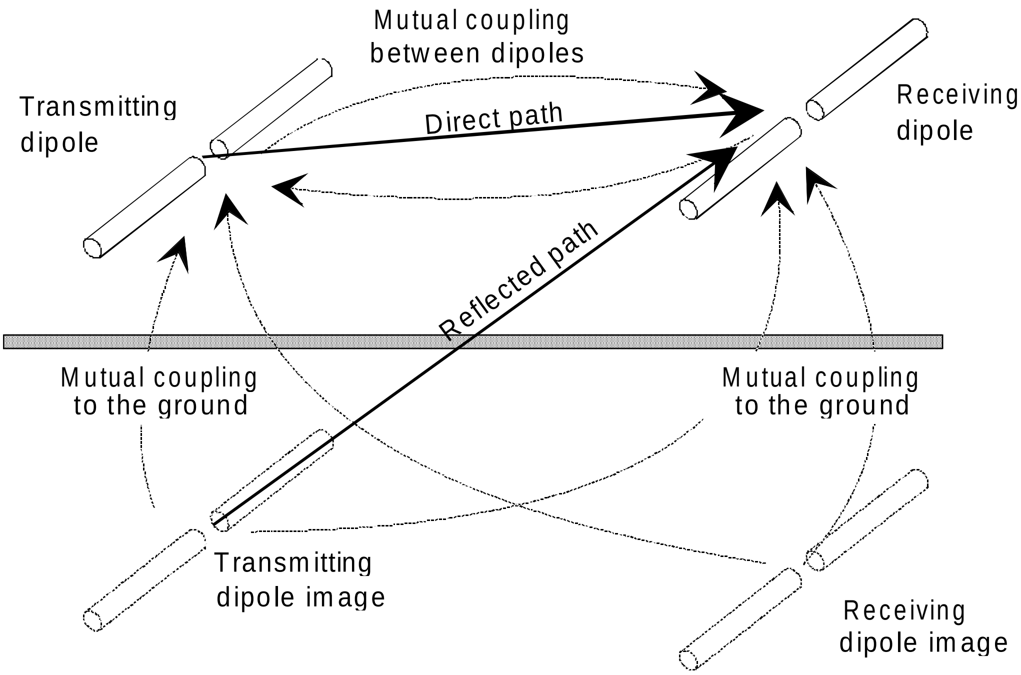

Figure 20: Mutual coupling during a site attenuation measurement

For accurate determination of NSA these additional effects needs to be taken into consideration and correction factors should be applied to the measured results to compensate.

In the verification procedure that follows, tables of correction factors are provided for mutual coupling between dipoles, where appropriate, for 3 m and 10 m range lengths.

6.3 Overview of the verification procedure

The first steps in the verification procedure are the gathering of all the appropriate test equipment (subclause 6.3.1) and preparation of the site (subclause 6.3.2).

The test equipment should then be configured (subclause 6.3.3), and the verification procedure carried out (subclause 6.4).

On completion of the verification procedure, the results need to be processed (subclause 6.5) so that at each test frequency a figure for the deviation of the open area test site from the ideal can be calculated and plotted (figure 23) and the measurement uncertainties calculated (subclauses 6.6 and 6.7).

The verification procedure (subclause 6.4) recommends an antenna scheme in the 30 MHz to 1 000 MHz frequency band which uses tuned, half wavelength dipoles for all frequencies in the range 80 MHz to 1 000 MHz and shortened dipoles (subclause 6.3.3) below 80 MHz.

NOTE: For cases in which this is not suitable, an alternative scheme using dipoles and bicones (possibly also LPDAs) is suggested in subclause 6.4.2. It should be noted that measurement uncertainty is likely to be degraded if the recommended dipole scheme is not used.

For the 1 to 12,75 GHz band, broadband antennas (LPDAs) are recommended.

Throughout the whole band of 30 MHz to 12,75 GHz, the procedure involves discrete frequencies only. For the frequency range 30 MHz to 1 000 MHz, the frequencies have been taken from CISPR 16-1 [6] annex G.

Figure 14 shows a typical verification testing arrangement of antennas (for the lower band) and test equipment.

In the following procedures, the position of the transmitting antenna is specified whilst the height of the receiving antenna is varied over 1 m to 4 m, so that the maximum received signal level is obtained. This maximum occurs when the direct signal and the signal reflected from the ground plane are in phase at the receiving antenna, or, in cases where this condition cannot be met within the height scan at the highest or lowest extremes of the height scan.

The following verification procedures require the full 1 m to 4 m height scan range to be available - values given in the text for ideal received signal levels are only valid under this condition. Therefore if the full 4 m height is not available, the results of the verification procedure will not be valid and the procedure should not be carried out.

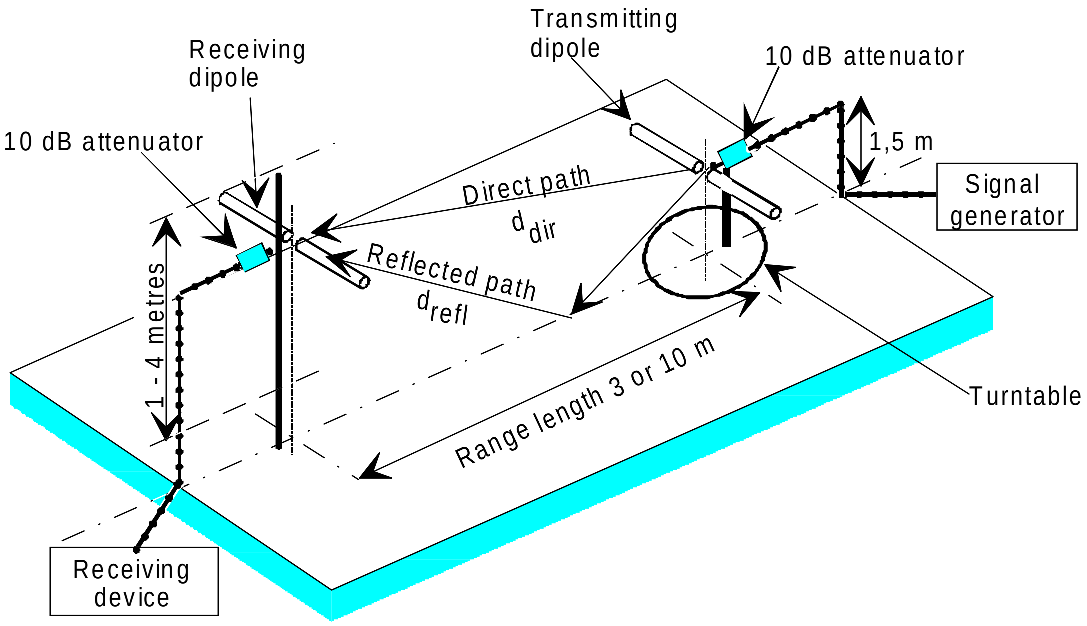

Figure 21: Open area test site layout for horizontally polarized tests using dipoles

6.3.1 Apparatus required

- Attenuator pads, 10 dB;
- connecting cables;
- ferrite beads;
- receiving device (measuring receiver or spectrum analyser);
- signal generator;
- transmit antenna;
- receive antenna.

For frequencies from 30 MHz to 1 000 MHz:

- transmit antenna (half wavelength dipoles as detailed in ANSI C63.5 [1] recommended);
- receive antenna (half wavelength dipoles as detailed in ANSI C63.5 [1] recommended).

NOTE 1: Alternatively dipoles plus bicones or dipoles plus bicones and LPDAs may be used.

NOTE 2: The reference dipole antennas, incorporating matching/transforming baluns, for the procedure are available in the following bands: 20 MHz to 65 MHz, 65 MHz to 180 MHz, 180 MHz to 400 MHz, 400 MHz to 1 000 MHz. Constructional details are contained in ANSI C63.5 [1]. In the recommended antenna scheme for verification in this band, a shortened dipole is used at all frequencies from 30 MHz to 70 MHz inclusive.

For frequencies above 1 000 MHz:

- transmit antenna (LPDA 1 GHz to 12,75 GHz);
- receive antenna (LPDA 1 GHz to 12,75 GHz).

The type and serial numbers of all items of test equipment should be recorded in the results sheet relevant to the frequency band i.e. Table 7 for the 30 MHz to 1 000 MHz band, table 8 for the 1 GHz to 12,75 GHz band.

6.3.2 Site preparation

Prior to the start of the verification procedure, system checks should be made on the equipment to be used. All items of test equipment, where appropriate, should be connected to power supplies, switched on and allowed adequate time to stabilize, as recommended by the manufacturers. Where a stabilization period is not given by the manufacturer, 30 minutes should be allowed.

The cables for both ends of the test site should be routed behind and away from the antennas, parallel to the ground plane for a minimum of 2 m. They should then be allowed to drop vertically towards the ground plane, through which they should pass to the test equipment.

These cables should be dressed with ferrite beads, spaced 0,15 m apart for their entire lengths above the ground plane. The cables, their routeing and dressing should be the same as for the normal operation of the open area test site.

NOTE: Where a cable drum is incorporated with the antenna mast, the routeing requirement and ferrite beading of the cables may be impossible to comply with. In such cases, increased measurement uncertainty results.

Calibration data for all items of test equipment should be available and valid. For all non-ANSI dipoles, the data should include VSWR and antenna factor (or gain) against frequency. The calibration data for all cables and attenuators should include insertion loss and VSWR throughout the entire frequency range of the tests. Where any correction factors/tables are required, these should be immediately available.

6.3.3 Measurement configuration

For the frequency band 30 MHz to 1 000 MHz, both antennas should be tuned half-wavelength dipoles (constructed as detailed in ANSI C63.5 [1]) aligned for the same polarization.

NOTE 1: Due to size constraints a shortened dipole is used over part of this frequency band. For uniformity of verification procedure across open area test sites and both types of anechoic chamber, the shortened dipole is used from 30 MHz to 70 MHz inclusive. At all these frequencies the 80 MHz arm length (0,889 metres) is used attached to the 20 MHz to 65 MHz balun for all test frequencies in the 30 - 60 MHz band and to the 65 MHz to 180 MHz balun for 70 MHz. Tuned half wavelength dipoles, attached to their matching baluns are used for all frequencies in the band 80 MHz to 1 000 MHz inclusive. Table 4 details dipole arm lengths (as measured from the centre of the balun block) and balun type against frequency.

Table 4: Dipole arm length and balun type against frequency

Frequency (MHz)	Dipole arm length (m)	Balun type
30	0,889	20 MHz to 65 MHz
35	0,889	
40	0,889	
45	0,889	
50	0,889	
60	0,889	
70	0,889	65 MHz to 180 MHz
80	0,889	
90	0,791	
100	0,714	
120	0,593	
140	0,508	

Frequency (MHz)	Dipole arm length (m)	Balun type
160	0,440	65 MHz to 180 MHz
180	0,391	
200	0,352	180 MHz to 400 MHz
250	0,283	
300	0,235	
400	0,175	
500	0,143	400 MHz to 1 000 MHz
600	0,117	
700	0,102	
800	0,089	
900	0,079	
1 000	0,076	

For both bands the transmitting antenna is placed in 10 different positions for each polarization, as shown in figures 15 and 16. Correction factors (where appropriate) and NSA data are supplied for all positions.

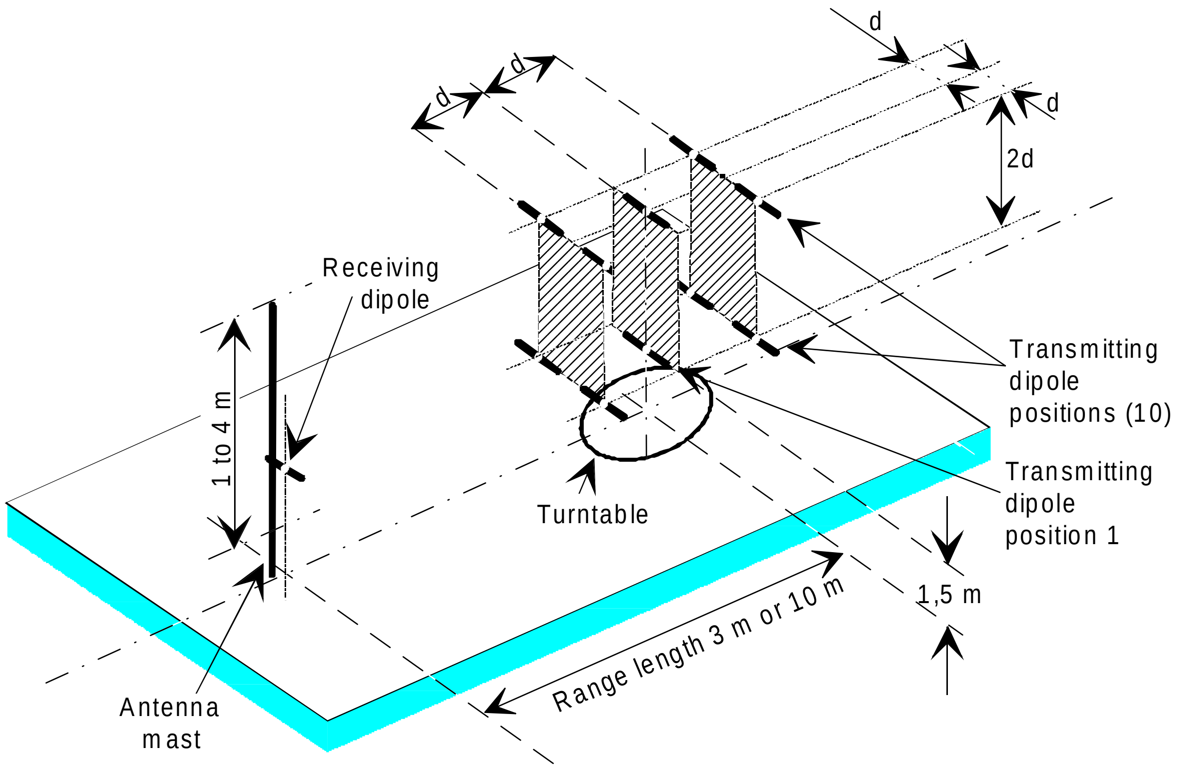

Figure 22: Antenna arrangements for horizontal polarization

Whilst figures 15 and 16 show the 30 MHz to 1 000 MHz scheme for dipoles, the same antenna positions/ polarization scheme is used in the 1 GHz to 12,75 GHz band for which both antennas should be LPDAs.

NOTE 2: When the transmitting LPDA is used at positions other than on the centre line of the open area test site, the transmitting and receiving antennas should be aligned in azimuth, but not in elevation (i.e. they should point directly towards each other keeping their long central axes parallel to the ground plane).

For both bands, the measured NSA is determined for all positions/polarizations.

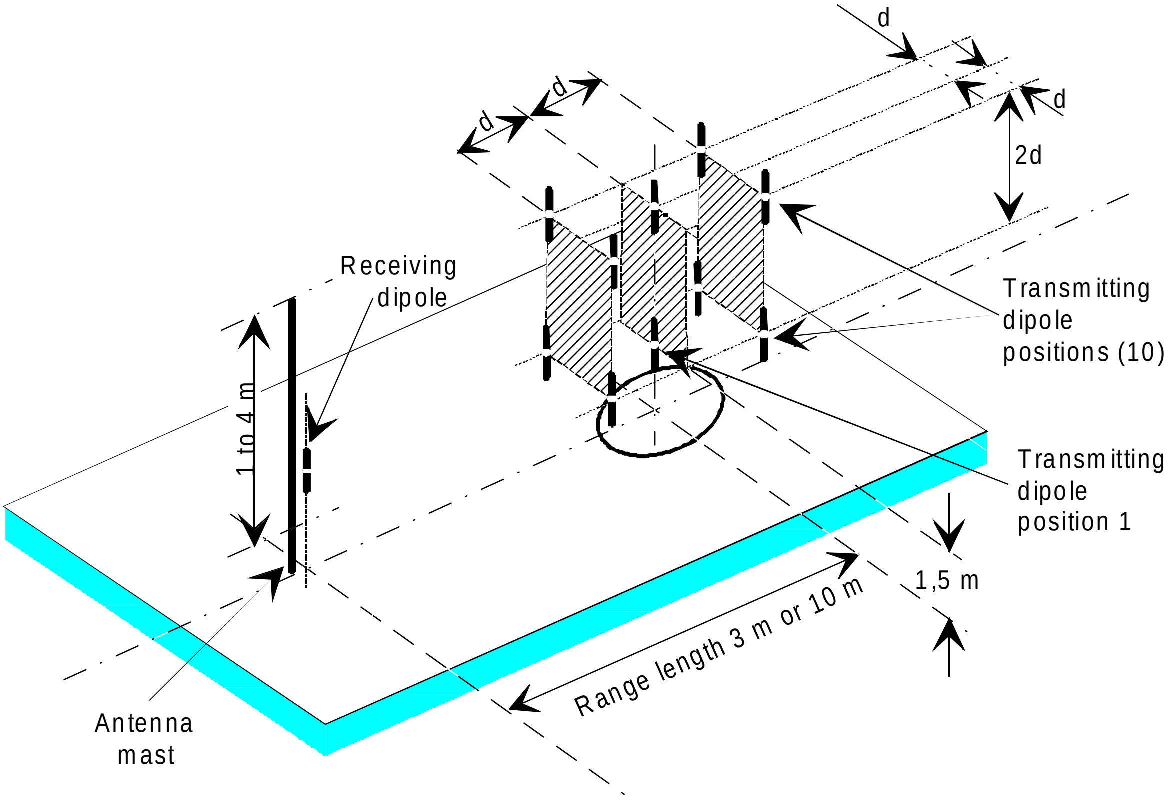

Figure 23: Antenna arrangements for vertical polarization

6.3.4 What to record

During the course of the procedure, the ambient temperature and relative humidity should be recorded.

Also during the course of the procedure, the output level of the signal generator, the received level, the tuned frequency and polarization of the antennas should be recorded along with ALL equipment used - signal generator, receiver, cables, connectors, etc. An example of the results sheet is shown in table 5. A set of 20 results sheets, one corresponding to each position/polarization of the transmitting antenna, should be completed for each frequency band.

NOTE: The results sheet for 1,0 GHz to 12,75 GHz verification is identical to table 5 except for renaming of the "Dipole Height" column to "LPDA Height" and the omission of the column for mutual coupling correction factor AF_{TOT}. Where LPDAs are used, no corrections for mutual coupling are necessary.

Table 5: Example of an open area test site verification results sheet

Open area test site verification procedure results sheet										**30 to 1 000 MHz**
Range length: 3m **Ambient temperature 20°C**			**Polarization: Horizontal** **Position Number 1**				**Date:** **Relative humidity 60 %**			
Freq. (MHz)	**Direct** V_{direct} **(dBμV)**	**Dipole height (m)**	**Site** V_{site} **(dBμV)**	**Transmit Antenna factor** AF_T **(dB)**	**Receive Antenna factor** AF_R **(dB)**	**Mutual coupling correction** AF_{TOT} **(dB)**	**Overall value (dB)**	**Ideal value (dB)**	**Differ-ence (dB)**	
Transmit antenna: Dipole S/No. D 001 Transmit antenna cable: Ref. No. C 128 Signal generator: Ref. No. SG 001 Attenuator: S/No. AT 01 Ferrite type: Worry beads					Receive antenna: Dipole S/No. D 002 Receive antenna cable: Ref. No. C 129 Receiving device: Ref. No. SA 001 Attenuator: S/No. At 02 Ferrite manufacturer: Rusty co. Ltd.					

6.4 Verification procedure

Introduction

Two different procedures, one for each band, are involved in verifying the performance of an open area test site which is used for the band 30 MHz to 12,75 GHz. The first procedure covers 30 MHz to 1 000 MHz and the second covers 1 GHz to 12,75 GHz.

6.4.1 Procedure 1: 30 MHz to 1 000 MHz

Direct attenuation

1) The two antenna cables should be connected together, via attenuator pads and an "in line" adapter as shown in figure 24. Alternatively, if this is not practical, a calibrated cable may be used instead of the adapter.

   NOTE 1: The use of a cable will increase the overall measurement uncertainty.

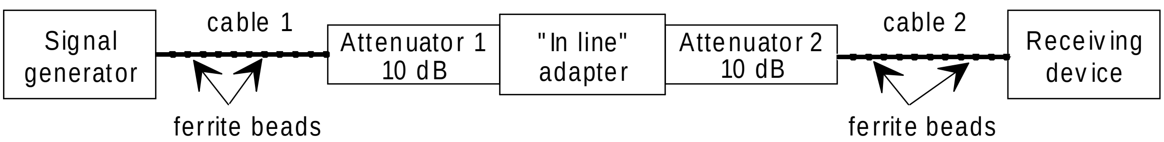

Figure 24: Initial equipment arrangement for the verification procedure

2) The output of the signal generator should be adjusted to an appropriate level. The minimum acceptable level for any frequency in the band of interest may be calculated from:

   20 dB above the maximum expected radiated path loss (20 log ((4π range length)/λ)), plus the ambient noise floor, the value of the attenuator pads and the cable losses, minus the antenna gains.

   NOTE 2: For practical purposes it is advisable to set a single output level for all frequencies in the band, since this avoids level changes during the verification. Therefore this calculation should be evaluated at 30 MHz, the worst frequency, since the reduced sensitivity of the shortened dipoles at this frequency requires an enhanced signal level 53 dB above that required for tuned half wavelength dipoles. Table 6 indicates the enhancement required for other frequencies where shortened dipoles are used.

EXAMPLE: 20 dB + 22 dB (radiated path loss) - 110 dBm (ambient noise floor) + 20 dB (attenuator pads) + 1 dB (cable losses) - 4 dB (antenna gains) + 53 dB (enhancement) = + 2 dBm (109 dBμV).

Table 6: Enhancement figures for shortened dipoles

Frequency (MHz)	Enhancement (dB)
30	53
35	48
40	43
45	38
50	32
60	19
70	4

If the calculated level is not available then the verification cannot proceed.

Once set, this signal generator output level should not be adjusted again for the entire duration of the verification procedure.

3) The receiving device and signal generator should be tuned to the appropriate frequency (starting at the first frequency given in the result sheet shown in table 7). The output level of the signal generator should be checked (to be certain that the original set level has been maintained) and the received level on the receiving device should be noted. For each frequency, the value to be entered in the column headed "Direct" on the results sheet is the sum of this received level plus the loss of the "in-line" adapter or cable at this frequency i.e.:

"Direct" value = received level + loss of "in-line" adapter or cable

4) Step 3 should be repeated for all the frequencies on the results sheet shown in table 7.

Radiated attenuation: Horizontal polarization

5) The adapter used to make the direct connection between the attenuator pads should be removed and the transmit and receive dipoles connected as shown schematically in figure 25.

6) The signal generator, receiving device and dipoles should be tuned to the appropriate frequency (starting at the top of the results sheet shown in table 7).

NOTE 3: For all frequencies below 80 MHz, a shortened dipole (as defined in subclause 6.2.3) should be used. The dipole arm length is defined as the measured distance from the centre of the balun block to the tip of the arm. From a fully extended state, each telescopic element, in turn, should be "pushed in" from the tip until the required length is obtained. The outermost section needs to fully compress before any of the others and so on.

7) The receiving dipole should be mounted on the antenna mast and oriented for horizontal polarization. The mast should allow the height of the antenna above the ground plane to be varied, subject to the restriction that no part of the antenna should be less than 0,25 m away from the ground plane, between 1 m and 4 m. The procedure should not be carried out on an open area test site that cannot provide the full 4 m height scan.

Table 7: Results sheet for 30 to 1 000 MHz verification of an open area test site.

Open area test site verification procedure results sheet									30 to 1 000 MHz
Range length:.........m Ambient temperature:........°C			Polarization: .... Position Number:.........			Date:………….. Relative humidity:.........%			
Freq. (MHz)	Direct V_{direct} (dBμV)	Dipole height (m)	Site V_{site} (dBμV)	Transmit Antenna factor AF_T (dB)	Receive Antenna factor AF_R (dB)	Mutual coupling correction AF_{TOT} (dB)	Overall value (dB)	Ideal value (dB)	Differ-ence (dB)
30									
35									
40									
45									
50									
60									
70									
80									
90									
100									
120									
140									
160									
180									
200									
250									
300									
400									
500									
600									
700									
800									
900									
1 000									
Transmit antenna: Dipole S/No. D 001 Transmit antenna cable: Ref. No. C 128 Attenuator: Ref. No. AT 01 Signal generator: Ref. No. SG 001 Ferrite type: Worry beads					Receive antenna: Dipole S/No. D 002 Receive antenna cable: Ref. No. C 129 Attenuator: Ref. No. AT 02 Receiving device: Ref. No. SA 001 Ferrite manufacturer: Rusty co. Ltd.				

8) The range length (3 m or 10 m) is defined as the horizontal distance between the receiving dipole and the axis of rotation of the turntable. This should be set to an accuracy of ± 0,01 m.

9) The transmitting antenna should be mounted in position 1 as shown in figure 22 and figure 26 and oriented for horizontal polarization. It should be positioned with its phase centre:

a) 1,5 metres above the ground plane;
b) on the axis of rotation of the turntable.

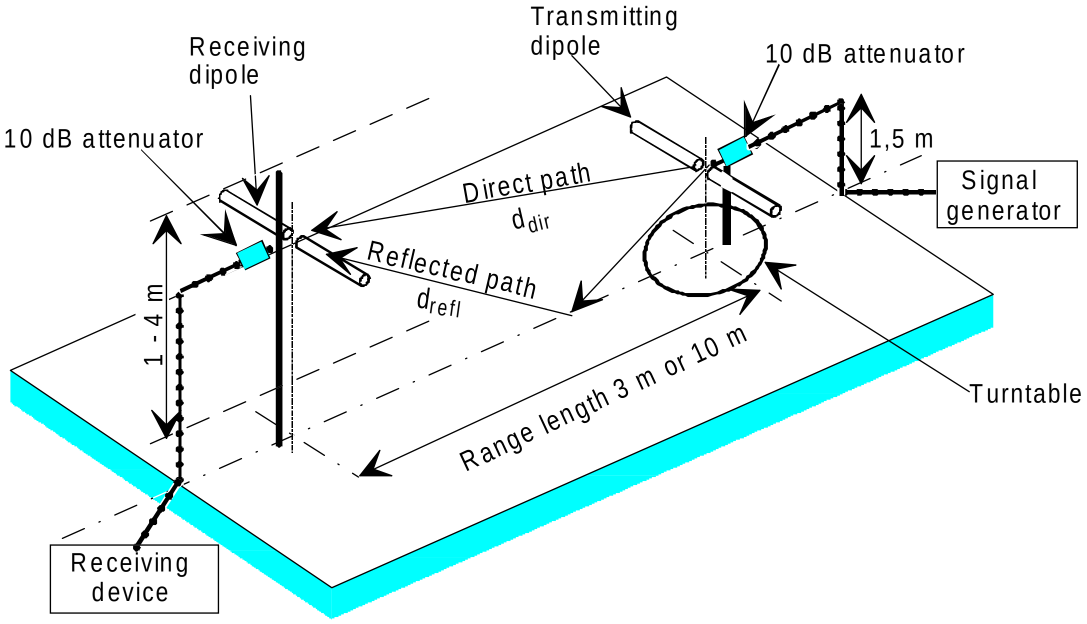

Figure 25: Equipment configuration for open area test site verification

10) The position of the receiving dipole should be varied over the 1 m to 4 m height range whilst monitoring the level of the received signal. The receiving dipole should then be positioned at the height of maximum received signal and the height recorded under "Dipole height" in the results sheet (table 7).

NOTE 4: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level will be at the top of the height range.

11) The output level of the signal generator should be checked (to ensure that an inadvertent change to the original set level has not occurred) and the received level on the receiving device should be noted. This value should be entered in the results sheet (table 7) under the column headed "Site".

12) Steps 6 to 11 should be repeated until all the frequencies in the results sheet have been completed, changing the dipoles as appropriate.

13) Steps 6 to 12 should be repeated with the transmitting dipole at the nine other positions as shown in figure 22 and figure 26.

NOTE 5: In figure 22 and figure 26, for both 3 and 10 m range verification, d = 0,7 m. The positioning accuracy all positions relative to position 1 should be ± 0,01 m.

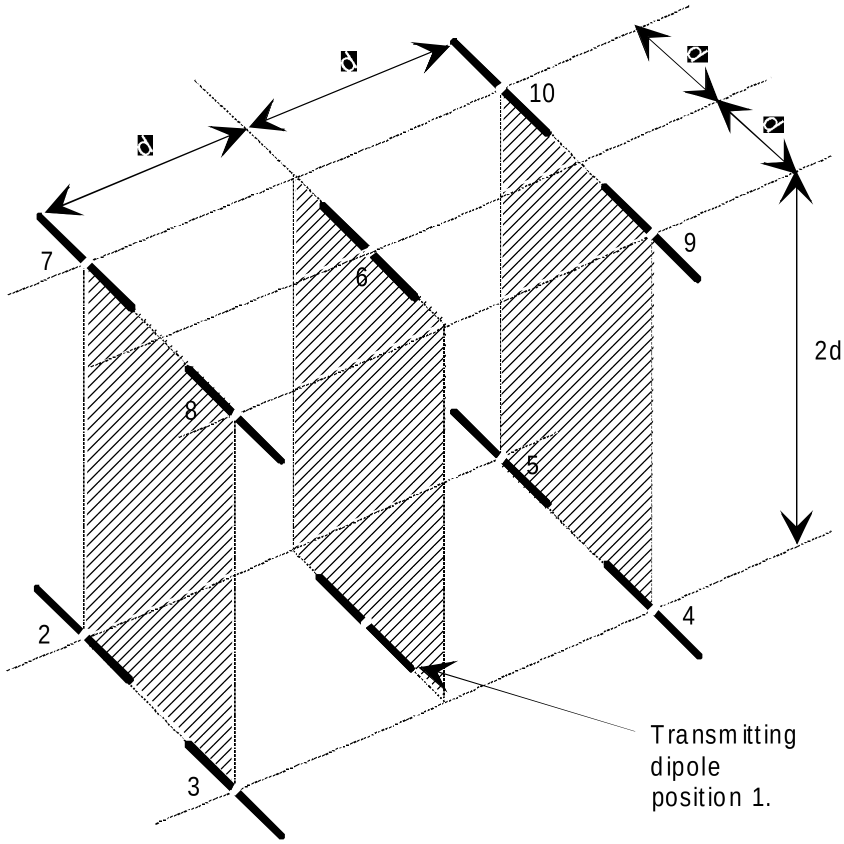

Figure 26: Expanded view of the 10 transmitting dipole positions

Radiated attenuation: Vertical polarization

14) The equipment should be connected as shown in figure 25 with the dipoles vertically polarized.

15) The signal generator, receiving device and dipoles should be tuned to the appropriate frequency (starting at the top of the results sheet shown in table 7).

NOTE 6: For all frequencies below 80 MHz, a shortened dipole (as defined in subclause 6.3.3) should be used. The dipole arm length is defined as the measured distance from the centre of the balun block to the tip of the arm. From a fully extended state, each telescopic element, in turn, should be "pushed in" from the tip until the required length is obtained. The outermost section needs to fully compress before any of the others and so on.

16) The antenna mast should allow the height of the dipole above the ground plane to be varied between 1 m and 4 m.

NOTE 7: No part of the receiving dipole should come within 0,25 m of the ground plane. This latter condition will limit the height scanning range in vertically polarized verification procedures for frequencies from 30 MHz up to 90 MHz inclusive.

17) The range length (3 m or 10 m) is defined as the horizontal distance between the receiving dipole and the axis of rotation of the turntable. This should be set to an accuracy of ± 0,01 m.

18) The transmitting dipole should be mounted in position 1 as shown in figure 23 and figure 26 and oriented for vertical polarization. It should be positioned with its centre 1,5 m above the ground plane. The axis of the dipole should lie on the axis of rotation of the turntable.

19) The receiving dipole should be raised and lowered through the specified range of heights (with the strict limitation that its lowest point should never be less than 0,25 m above the ground plane), whilst

monitoring the level of the received signal. The receiving dipole should then be positioned at the height of maximum received signal and the height recorded under "Dipole height" in the results table.

NOTE 8: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level may be at the top of the height range. Alternatively, due to the 0,25 m limitation on the spacing away from the ground plane, the true maximum may be below the lowest possible height, in which case the maximum received level will be at the lowest point in the available height range.

20) The output level of the signal generator should be checked (to ensure that an inadvertent change to the original set level has not occurred) and the received level on the receiving device should be noted. This value should be entered in the results sheet (table 7) under the column headed "Site".

21) Steps 15 to 20 should be repeated until all the frequencies in the results table have been completed, changing the dipoles as appropriate.

22) Steps 15 to 21 should be repeated with the transmitting dipole at the 9 other positions as shown in figures 23 and 26.

NOTE 9: In figures 23 and 26, for both 3 m and 10 m range length verifications, d = 0,7 m. The positioning accuracy of all positions relative to position 1 should be ± 0,01 m.

6.4.2 Alternative Procedure 1: 30 MHz to 1 000 MHz

The procedure contained in subclause 6.3.1 is the most accurate procedure considered for verification in the 30 MHz to 1 000 MHz band - the use of ANSI C63.5 [1] dipoles enabling precise correction figures for mutual coupling to be incorporated into the results. The procedure can be very time consuming however and, as a quicker, alternative scheme, the following less accurate procedure could be adopted.

1) The procedure as detailed in subclause 6.4.1 should be completed for the transmitting dipole in position 1 for both horizontal and vertical polarization.

2) Both transmitting and receiving dipoles should be replaced with bicones for the full 30 MHz to 1 000 MHz band.

NOTE 1: As a further alternative, bicones 30 MHz to 200 MHz (possibly 300 MHz) can be used with LPDAs for the rest of the band. Note, however, that the range length uncertainty associated with the moving phase centre of the latter can significantly increase measurement uncertainty (e.g. a typical design of LPDA with length approximately 1 m, could contribute a range length uncertainty of u_j = 1,73 dB over a 3 m range length. This would reduce to u_j = 0,5 dB for a 10 m range length but would remain a significant contribution to the uncertainty).

CAUTION: For reduced uncertainty in the verification procedure, measurements using alternative antennas should be carried out in their far-fields (of clause 7 of ETR 273-1-1 [9]). For a typical bicone of length 1,315 metres, far-field conditions over a 3 m range length only exist from 30 MHz to 60 MHz and not at 70 MHz or above. For a 10 m range length, the corresponding usable frequency range is 30 MHz to 270 MHz.

3) The entire verification procedure as described in steps 1 to 22 should be repeated, including position 1 for the transmitting antenna.

NOTE 2: This alternative procedure does not include any correction factors to account for mutual coupling effects. Whilst these effects are smaller for broadband antennas than for dipoles, there will be increased uncertainty in this alternative verification process because the effects cannot be calculated out of the measurements.

6.4.3 Procedure 2: 1 GHz to 12,75 GHz

Direct attenuation

1) The two antenna cables should be connected together, via attenuator pads and an "in line" adapter as shown in figure 27. Alternatively, if this is not practical, a calibrated cable may be used instead of the adapter.

NOTE 1: The use of a cable will increase the overall measurement uncertainty.

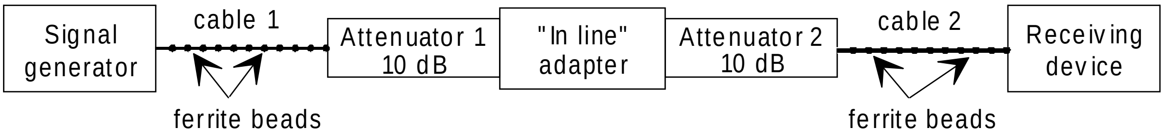

Figure 27: Initial equipment arrangement for the verification tests

2) The output level of the signal generator should be adjusted to an appropriate level. The minimum acceptable level for any frequency in the band of interest may be calculated from:

- 20 dB above the maximum expected radiated path loss (20 log ((4π range length)/λ)), plus the ambient noise floor, the value of the attenuator pads and the cable losses, minus the antenna gains.

NOTE 2: For practical purposes, it is advisable to set a single output level for all frequencies in the band, since this avoids level changes during the verification.

EXAMPLE: 20 dB + 75 dB (maximum expected path loss) + (- 110 dB) (ambient noise floor) + 20 dB (attenuator pads) + 15 dB (cable losses) - 10 dB (antenna gains) = + 10 dBm (117 dBμV).

If the calculated level is not available then the verification cannot proceed.

Once set, this signal generator output level should not be adjusted again for the entire duration of the verification procedure.

3) The receiving device and signal generator should be tuned to the appropriate frequency (starting at the first frequency given in the result sheet shown in table 8). The output level of the signal generator should be checked (to be certain that the original set level has been maintained) and the received level on the receiving device should be noted. For each frequency, the value to be entered in the column headed "Direct" on the results sheet is the sum of this received level plus the loss of the "in-line" adapter or cable i.e.:

"Direct" value = received level + loss of "in-line" adapter or cable

4) Step 3 should be repeated for all frequencies in the results sheet shown in table 8.

Radiated attenuation: Horizontal polarization

5) The adapter used to make the direct connection between the attenuator pads should be removed and the transmit and receive antennas should be connected connected as shown in figure 28 with the LPDAs horizontally polarized.

NOTE 3: In order to minimize the uncertainty in range length which results from using LPDAs (the radiating phase centre moves with frequency), the radiating phase centre is defined, for the purposes of this procedure, as the point on the LPDAs central axis where its thickness is 0,08 m. This is shown in figure 29.

6) The receiving antenna should be mounted on the antenna mast and oriented for horizontal polarization. The mast should allow the height of the antenna above the ground plane to be varied between 1 m and 4 m. The central axis of the LPDA should lie parallel to the ground plane.

7) The horizontal spacing between the phase centre of the receiving LPDA and the axis of rotation of the turntable is the range length. This should be set to an accuracy of ± 0,01 m.

8) The transmitting antenna should be mounted in position 1 as shown in figures 22 and 26, with its central axis 1,5 m above the ground plane. The central axis of the transmitting antenna should lie parallel to the ground plane. The phase centre of the transmitting antenna should lie on the axis of rotation of the turntable.

9) The signal generator and receiving device should be tuned to the appropriate frequency (starting at the top of the results sheet shown in table 8).

10) The position of the receiving antenna should be varied over the 1 m to 4 m height range, whilst monitoring the level of received signal. The receiving antenna should then be positioned at the height of maximum received signal and the height recorded under "LPDA height" in the results sheet (table 8).

NOTE 4: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level will be at the top of the height range.

11) The output level of the signal generator should be checked (to ensure that an inadvertent change to the original set level has not occurred) and the received level on the receiving device should be noted. This value should be entered in the results sheet (table 8) under the column headed "Site".

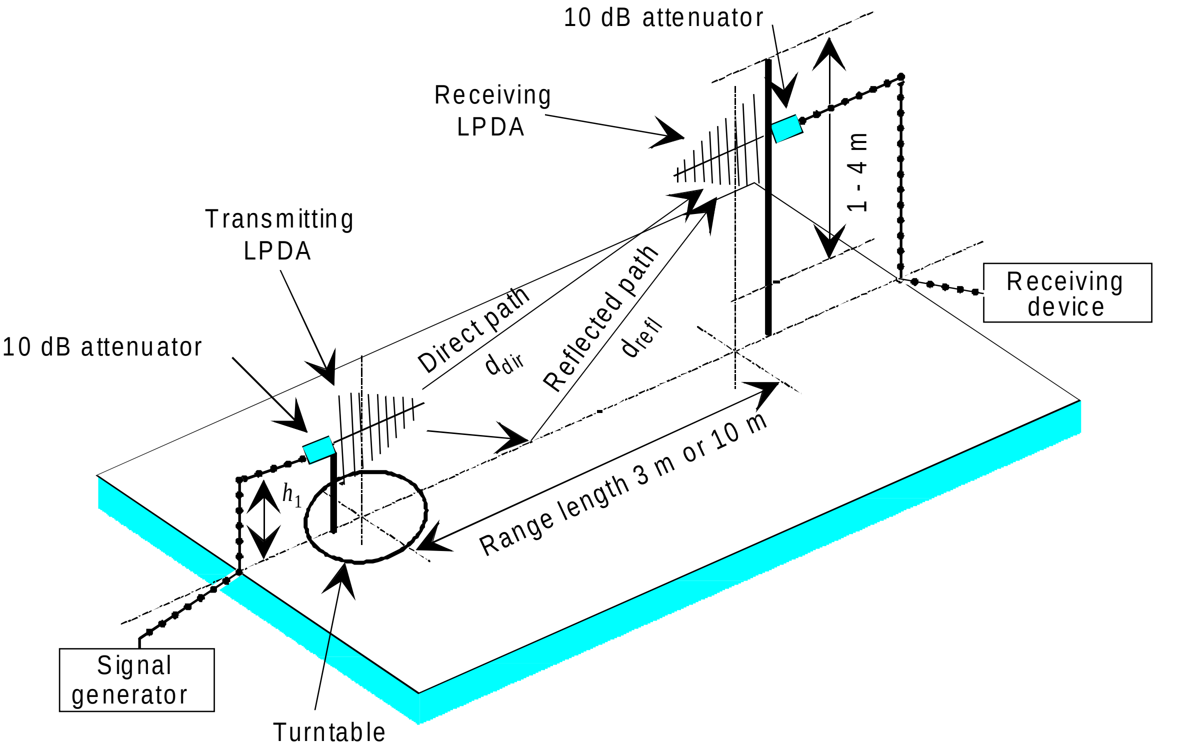

Figure 28: Open area test site layout for verification with LPDAs

12) Steps 9, 10 and 11 should be repeated until all the frequencies in the results sheet (table 8) have been completed.

13) Steps 9, 10, 11 and 12 should be repeated with the transmitting antenna at the 9 other positions as shown in figures 22 and 26.

NOTE 5: In figures 22 and 26, for both 3 m and 10 m range length verifications, d = 0,7 m. The positioning accuracy of the phase centres for all positions relative to position 1 should be ± 0,01 m.

NOTE 6: For all positions, both antennas needs to point directly towards each other, consistent with keeping their central axes parallel to the ground plane. For all transmitting positions other than 1 and 6 in figures 22 and 26, this will involve small angle rotation of both receiving and transmitting antennas. For both antennas, this rotation should be about the phase centre.

Radiated attenuation: Vertical polarization

14) The equipment should be connected as shown in figure 28.

NOTE 7: In order to minimize the uncertainty in range length which results from using LPDAs (the radiating phase centre moves with frequency), the radiating phase centre is defined, for the purposes of these measurements, as the point on the LPDAs central axis where its thickness is 0,08 m. This is shown in figure 29.

15) The receiving antenna should be oriented for vertical polarization. The mast should allow the height of the antenna above the ground plane to be varied between 1 m and 4 m subject to the restriction that no part of the antenna should be less than 0,25 m away from the ground plane. The central axis of the receiving LPDA should lie parallel to the ground plane.

16) The horizontal spacing between the phase centre of the receiving antenna and the axis of rotation of the turntable is the range length. This should be set to an accuracy of ± 0,01 m.

17) The transmitting antenna should be mounted in position 1 as shown in figures 23 and 26, with its central axis 1,5 m above the ground plane. The central axis of the log periodic dipole array should lie parallel to the ground plane. The phase centre of the transmitting antenna should lie on the axis of rotation of the turntable. The transmitting antenna should be oriented for vertical polarization.

18) The signal generator and the receiving device should be tuned to the appropriate frequency (starting at the top of the results sheet shown in table 8).

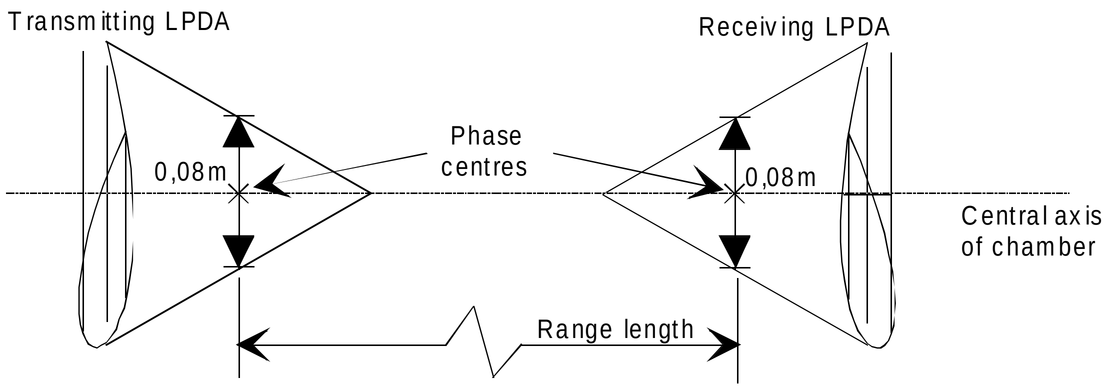

Figure 29: Definition of phase centres of the log periodic dipole array

19) The position of the receiving antenna should be varied over the 1 to 4 m height range, whilst monitoring the level of received signal. The receiving antenna should then be positioned at the height of maximum received signal and the height recorded under "LPDA height" in the results table.

NOTE 8: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level may be at the top of the height range.

20) The output level of the signal generator should be checked (to ensure that an inadvertent change to the original set level has not occurred) and the received level on the receiving device should be noted. This value should be entered in the relevant table under the column headed "Site".

21) Steps 18, 19 and 20 should be repeated until all the frequencies in the results sheet (table 8) have been completed.

Table 8: Open area test site verification results sheet (1 GHz to 12,75 GHz)

Open area test site verification procedure results sheet								**1 - 12,75 GHz**
Range length:.........m			**Polarization: ....**			**Date:………………..**		
Ambient temperature:........°C			**Position Number:.........**			**Relative humidity:.........%**		
Freq. (GHz)	**LPDA height (m)**	**Direct V_{direct} (dBμV)**	**Site V_{site} (dBμV)**	**Transmit Antenna factor AF_T (dB)**	**Receive Antenna factor AF_R (dB)**	**Overall value (dB)**	**Ideal value (dB)**	**Difference (dB)**
1,0								
1,25								
1,5								
1,75								
2,0								
2,25								
2,5								
2,75								
3,0								
3,25								
3,5								
3,75								
4,0								
4,5								
5,0								
5,5								
6,0								
6,5								
7,0								
7,5								
8,0								
8,5								
9,0								
9,5								
10,0								
10,5								
11,0								
11,5								
12,0								
12,75								
Transmit antenna				Receive antenna:				
Transmit antenna cable:				Receive antenna cable:				
Signal generator:				Receiving device:				
Attenuator:				Attenuator:				
Ferrite type:				Ferrite manufacturer:				

22) Steps 18, 19, 20 and 21 should be repeated with the transmitting antenna at the nine other positions as shown in figures 16 and 19.

NOTE 9: In figures 16 and 19, for both 3 m and 10 m range length verifications, d = 0,7 m. The positioning accuracy of the phase centres of all positions relative to position 1 should be ± 0,01 m.

NOTE 10: For all positions, both antennas needs to point directly towards each other, consistent with keeping their central axes parallel to the floor. For all transmitting positions other than 1 and 6 in figures 23 and 26, this will involve small angle rotation of both receiving and transmitting antennas. For both antennas, this rotation should be about the phase centre.

6.5 Processing the results of the verification procedure

6.5.1 Introduction

Having carried out the verification procedures as detailed in subclause 6.3 the results sheets should have values filling the first four columns, namely those headed "Freq", "Dipole height" or "LPDA height", "Direct" and "Site". This section details the values to be incorporated in all the remaining columns. The processing of the results finally reveals how well the measured performance of the open area test site compares to the ideal case.

Firstly, the figures for entering under the column headings of "Transmit Antenna factor, AF_T" and "Receive Antenna factor, AF_R" are discussed and values are provided. Secondly, for the 30 to 1 000 MHz verification procedure only, correction factors are provided for the recommended antenna scheme (ANSI C63.5 [1] dipoles) to allow for the effects of mutual coupling and mismatch loss. These effects are regarded as not significant at frequencies above 180 MHz and enable the column headed "Mutual coupling correction, AF_{TOT}" to be completed. The "Overall value" column can then be calculated. This column reveals the measured NSA for the open area test site.

Finally, having extracted the relevant figures (from tables provided) to complete the "Ideal value" column, the difference between the measured performance and the ideal can be calculated by simple subtraction of the values in the columns "Overall value" and "Ideal value".

6.5.2 Procedure 1: 30 MHz to 1 000 MHz

Antenna factors

For dipoles, the antenna factor of each dipole is given by:

$$\text{Antenna factor} = 20 \log f - 31{,}4 \text{ dB}$$

where f is the frequency in MHz.

NOTE 1: A resistive loss of 0,5 dB is incorporated into this formula.

Whilst the above formula for antenna factor applies only to a tuned half wavelength dipole, it should still be used in this verification procedure, even where shortened dipoles have been used (the 30 MHz to 70 MHz band). Table 11 gives the values at the test frequencies. The relevant values should be entered in the verification results sheet (table 9) in the columns headed "Transmit Antenna factor AF_T" and "Receive Antenna factor AF_R".

NOTE 2: Table 11 applies for both horizontal and vertical polarization.

Table 9: Antenna factor for a dipole used in the verification procedure.

Frequency (MHz)	Antenna factor (dB)
30	-1,9
35	-0,5
40	0,6
45	1,7
50	2,6
60	4,2
70	5,5
80	6,7
90	7,7
100	8,6
120	10,2
140	11,5

Frequency (MHz)	Antenna factor (dB)
160	12,7
180	13,7
200	14,6
250	16,6
300	18,1
400	20,6
500	22,6
600	24,2
700	25,5
800	26,7
900	27,7
1 000	28,6

When antennas other than dipoles are used, antenna factors are usually provided by the manufacturers. Where gain figures, rather than antenna factors, have been given, these can be converted into antenna factor by the following equation:

$$Antenna\ factor = 20\log\left(\frac{9{,}734}{\lambda\sqrt{G}}\right)\ \mathrm{dB}$$

where:

λ is the wavelength (m);
G is the numeric gain.

NOTE 3: The gain figure to be used should be relative to an isotropic radiator - not relative to a dipole.

Mutual coupling and mismatch loss correction factors

Tables 10 and 11 give the factors necessary to correct the measured figures for not only mutual coupling, but also for mismatch transmission loss - this being the dominant term for frequencies up to 70 MHz. Table 10 applies for horizontal polarization, table 11 for vertical polarization.

NOTE 4: Particularly at low frequencies (i.e. up to 180 MHz) the performance of each antenna used in the verification procedure is affected by the presence of the other antenna and the ground plane. These interactions are termed mutual coupling and have been modelled by computer simulation for the recommended antenna scheme (ANSI dipoles) only.

For the recommended dipole antenna scheme only, the relevant figures should be taken from tables 10 or 11 and entered in the results sheet (table 7) in the column headed "Mutual coupling correction AF_{TOT}". For all frequencies above 180 MHz, the correction factor should be taken as 0,0 dB.

For the alternative antenna schemes (bicones only or bicones and LPDAs) all entries in the "Mutual coupling correction AF_{TOT}" column should be 0,0 dB.

Table 10: Mutual coupling correction factors for horizontal polarization

	Receiving height scan: 1 m to 4 m AF_{TOT} (dB)											
	Range length: 3m Various positions						Range length: 10m Various positions					
Freq: (MHz)	1	2 3	4 5	6	7 8	9 10	1	2 3	4 5	6	7 8	9 10
30	53,23	53,49	52,36	52,93	52,91	52,18	51,59	51,64	51,51	51,61	51,57	51,50
35	47,76	47,80	47,05	47,50	47,39	47,03	46,50	46,54	46,43	46,55	46,59	46,48
40	42,51	42,42	41,93	42,37	42,18	41,97	41,41	41,44	41,45	41,56	41,56	41,52
45	37,06	37,03	36,60	37,05	36,89	36,73	36,21	36,13	36,16	36,44	36,40	36,44
50	31,40	31,24	30,86	31,48	31,27	31,23	30,40	30,42	30,47	30,78	30,79	30,82
60	18,56	18,72	17,93	18,89	18,52	18,65	17,88	17,86	17,87	17,93	17,92	17,96
70	3,99	4,39	3,59	3,72	3,72	3,37	4,42	4,46	4,44	2,79	2,60	2,95
80	0,61	0,64	1,02	1,72	1,70	0,73	0,81	0,81	0,77	0,35	0,45	0,22
90	0,24	-0,38	-0,13	1,87	1,34	0,61	0,37	0,22	0,26	0,50	0,40	0,28
100	-0,29	-1,16	-1,15	1,23	0,00	0,50	-0,04	-0,14	0,01	0,14	0,04	-0,08
120	-2,27	-0,99	-1,60	-0,65	-0,38	-0,28	-1,31	-1,35	-1,34	-0,48	-0,68	-0,79
140	-0,89	-1,14	-1,30	0,61	0,03	0,91	-0,53	-0,50	-0,48	0,43	0,32	0,31
160	-0,17	-0,04	0,04	-0,52	-0,35	-0,03	0,44	0,37	0,50	-0,20	-0,30	-0,41
180	-0,18	-0,09	-0,23	-0,15	-0,13	0,51	0,40	0,43	0,45	0,10	-0,11	-0,22

Table 11: Mutual coupling correction factors for vertical polarization

	Receiving height scan : limited (30 MHz to 90 MHz) : 1 m to 4 m (100 MHz to 180 MHz) AF_{TOT} (dB)											
	Range length: 3m Various positions						Range length: 10m Various positions					
Freq: (MHz)	1	2 3	4 5	6	7 8	9 10	1	2 3	4 5	6	7 8	9 10
30	50,79	50,72	50,83	50,78	51,40	50,24	51,04	51,00	51,04	50,90	50,87	50,94
35	45,54	45,45	45,70	46,08	46,89	45,16	46,03	46,04	46,03	45,90	45,86	45,93
40	40,44	40,35	40,74	41,64	42,42	40,24	41,07	41,07	41,08	40,94	40,90	40,97
45	35,26	35,06	35,49	37,12	37,83	35,39	35,96	35,95	35,97	35,78	35,74	35,82
50	29,78	29,56	30,04	32,11	32,61	30,13	30,50	30,49	30,50	30,25	30,21	30,29
60	17,50	17,36	17,73	19,50	19,68	19,06	18,26	18,24	18,28	17,79	17,74	17,82
70	3,20	3,35	3,71	4,35	4,65	4,55	4,09	4,12	4,11	3,75	3,70	3,80
80	0,00	-0,33	0,30	1,12	1,04	1,06	0,42	0,51	0,45	0,82	0,84	0,92
90	-0,19	-0,78	-0,25	0,53	0,19	1,30	0,09	0,10	0,02	0,59	0,61	0,58
100	-0,55	-0,43	-0,28	0,26	0,04	0,04	0,01	0,00	0,06	0,46	0,37	0,41
120	-0,53	1,44	-0,52	-0,22	0,80	0,18	0,03	-0,03	-0,02	0,06	0,27	0,11
140	1,18	1,10	0,84	0,82	0,71	-0,02	-0,01	0,04	0,04	0,24	0,28	0,29
160	0,78	0,74	0,69	0,55	0,31	0,35	0,07	0,07	0,06	0,22	0,27	0,19
180	0,41	0,55	0,31	0,29	0,26	0,23	0,09	0,06	0,10	0,23	0,23	0,21

Table 12: Theoretical Ideal values for NSA for horizontal polarization

	Ideal NSA (dB)											
	Range length: 3m Various positions						Range length: 10m Various positions					
Freq: (MHz)	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**
30	12,79	11,53	15,16	9,39	8,51	11,54	26,43	25,48	27,51	21,51	20,65	22,52
35	10,48	9,24	12,79	7,64	6,85	9,71	23,84	22,90	24,91	19,09	18,25	20,06
40	8,51	7,30	10,79	6,25	5,54	8,25	21,61	20,68	22,67	17,06	16,26	18,00
45	6,81	5,64	9,07	5,12	4,48	7,04	19,66	18,74	20,71	15,33	14,57	16,23
50	5,34	4,20	7,58	4,16	3,57	6,01	17,93	17,02	18,97	13,86	13,15	14,72
60	2,91	1,85	5,14	2,58	2,05	4,32	14,99	14,11	16,00	11,54	10,95	12,31
70	1,01	0,01	3,21	1,28	0,78	2,93	12,58	11,74	13,56	9,91	9,94	10,55
80	-0,53	-1,46	1,66	0,16	-0,32	1,75	10,57	9,77	11,51	8,63	8,13	9,26
90	-1,81	-2,69	0,36	-0,84	-1,31	0,72	8,86	8,11	9,77	7,53	7,03	8,15
100	-2,91	-3,74	-0,75	-1,73	-2,20	-0,20	7,44	6,74	8,29	6,56	6,06	7,18
120	-4,70	-5,48	-2,57	-3,22	-3,99	-1,79	5,24	4,68	5,97	4,91	4,41	5,52
140	-6,16	-6,91	-4,05	-4,76	-5,38	-2,96	3,68	3,15	4,33	3,52	3,03	4,14
160	-7,39	-8,02	-5,30	-5,94	-6,51	-4,13	2,40	1,87	3,04	2,34	1,84	2,95
180	-8,43	-8,62	-6,38	-6,96	-7,48	-5,22	1,29	0,76	1,94	1,29	0,80	1,91
200	-9,12	-8,67	-7,33	-7,85	-8,42	-6,17	0,31	-0,21	0,96	0,37	-0,12	0,98
250	-10,33	-11,32	-8,84	-9,82	-10,40	-8,13	-1,72	-2,24	-1,07	-1,59	-2,08	-0,98
300	-12,38	-13,25	-10,21	-11,40	-11,97	-9,74	-3,35	-3,87	-2,71	-3,05	-3,48	-2,55
400	-15,22	-15,98	-13,11	-13,89	-14,49	-12,22	-5,90	-6,42	-5,25	-5,58	-6,06	-4,96
500	-17,30	-17,65	-15,20	-15,79	-16,43	-14,17	-7,86	-8,35	-7,21	-7,56	-8,05	-6,95
600	-18,66	-19,43	-16,87	-17,39	-18,02	-15,74	-9,22	-9,75	-8,69	-9,17	-9,64	-8,56
700	-20,10	-20,85	-17,99	-18,77	-19,03	-17,09	-10,63	-11,15	-9,98	-10,52	-11,01	-9,91
800	-21,35	-21,89	-19,20	-19,91	-20,51	-18,25	-11,83	-12,36	-11,19	-11,68	-12,14	-11,06
900	-22,24	-22,91	-20,32	-20,95	-21,50	-19,27	-12,89	-13,42	-12,23	-12,67	-13,14	-12,06
1 000	-23,20	-23,95	-21,30	-21,84	-22,35	-20,13	-13,82	-14,34	-13,18	-13,61	-14,05	-13,00

Completion of the results sheet

The next stage is to enter values in the column headed "Overall value". This is achieved by performing the following calculation:

"Overall value" = "V_{direct}" - "V_{site}" - "AF_T" - "AF_R" - "AF_{TOT}"

The resulting value is the measured NSA for the open area test site.

The final stages in determining the quality of the site are to complete the column headed "Ideal value" in the results sheet by taking the relevant values from tables 12 or 13 (for horizontal or vertical polarization respectively) and to calculate the entries for the "Difference" column from:

"Difference" = "Overall value" - "Ideal value"

The values in the "Difference" column represent the variation between the theoretical and the measured NSA of the open area test site.

Table 13: Ideal values for NSA for vertical polarization

	Ideal NSA (dB)											
	Range length: 3m Various positions						Range length: 10m Various positions					
Freq: (MHz)	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**
30	9,93	8,90	10,99	12,34	10,32	14,28	17,05	16,53	17,58	18,08	17,69	18,49
35	8,70	7,69	9,74	11,16	9,05	13,28	15,73	15,21	16,26	16,80	16,42	17,21
40	7,68	6,67	8,68	10,08	7,90	12,38	14,59	14,07	15,12	15,71	15,34	16,11
45	6,81	5,81	7,78	9,05	6,84	11,48	13,59	13,08	14,11	14,77	14,41	15,16
50	6,06	5,08	7,00	8,03	5,83	10,51	12,70	12,19	13,22	13,95	13,60	14,32
60	4,87	3,91	5,74	6,07	3,99	8,41	11,18	10,68	11,69	12,58	12,26	12,93
70	4,00	3,05	4,79	4,35	2,45	6,45	9,91	9,42	10,41	11,50	12,22	11,82
80	3,38	2,41	4,08	2,96	1,24	4,82	8,83	8,35	9,32	10,65	10,41	10,92
90	2,62	1,81	3,18	1,90	0,34	3,53	7,80	7,32	8,29	9,69	9,46	9,95
100	2,15	1,23	2,58	1,14	-0,34	2,54	6,92	6,45	7,41	8,96	8,77	9,21
120	1,56	-1,11	2,15	0,25	-1,67	1,15	5,53	5,09	5,99	8,12	7,31	8,26
140	-1,03	-3,35	1,41	-1,27	-3,46	0,17	4,42	4,01	4,85	5,83	5,29	6,43
160	-3,14	-5,20	-0,95	-3,01	-4,77	-0,91	3,53	3,16	3,92	4,31	3,79	4,83
180	-4,82	-6,66	-2,82	-4,10	-5,47	-2,44	2,81	2,50	3,17	3,04	2,55	3,55
200	-6,17	-7,82	-4,32	-4,75	-6,20	-3,48	2,25	2,00	2,56	1,97	1,48	2,46
250	-8,63	-9,89	-7,08	-6,95	-8,54	-5,09	0,83	0,23	1,57	-0,21	-0,67	0,26
300	-10,37	-11,36	-9,04	-8,23	-10,19	-7,00	-1,51	-2,10	-0,93	-1,93	-2,37	-1,46
400	-12,10	-13,81	-11,82	-10,90	-12,72	-9,49	-4,75	-5,32	-4,17	-4,55	-4,97	-4,09
500	-14,62	-15,91	-13,04	-12,96	-14,52	-11,42	-7,03	-7,59	-6,45	-6,52	-6,95	-6,09
600	-16,36	-17,37	-15,04	-14,58	-16,19	-12,99	-8,79	-9,35	-8,23	-7,93	-8,39	-7,63
700	-17,77	-18,83	-16,58	-15,92	-17,59	-14,32	-10,24	-10,80	-9,68	-9,36	-9,79	-8,90
800	-18,77	-19,87	-17,83	-17,05	-18,71	-15,47	-11,47	-12,02	-10,91	-10,56	-10,95	-12,11
900	-19,83	-20,97	-18,52	-18,06	-19,69	-16,48	-12,52	-13,10	-11,98	-11,62	-11,99	-11,15
1 000	-20,86	-21,92	-19,59	-18,97	-20,66	-17,38	-13,49	-13,91	-12,92	-12,51	-12,95	-12,11

6.5.3 Procedure 2: 1 GHz to 12,75 GHz

Antenna factors

Generally, the manufacturer of the LPDAs will supply figures for either the gain or antenna factor variation with frequency. Where the gain variation is given, this should be converted to antenna factor by the following formula:

$$Antenna\ factor = 20\log\left(\frac{9{,}734}{\lambda\sqrt{G}}\right)\,\mathrm{dB}$$

where:

- λ is the wavelength (m);
- G is the numeric gain.

Whether directly or indirectly (by using the formula), the antenna factor columns in the results sheet headed "Transmit Antenna factor AF_T" and "Receive Antenna factor AF_R" should now be filled in with the relevant values.

Table 14: Ideal values of NSA for horizontal polarization (1 GHz to 12,75 GHz)

	Ideal NSA (dB)											
	Range length: 3m Various positions						**Range length: 10m Various positions**					
Freq: (GHz)	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**
1,0	-23,2	-24,0	-21,4	-21,8	-22,3	-20,1	-13,8	-14,4	-13,2	-13,6	-14,1	-13,0
1,25	-24,9	-25,9	-23,1	-23,8	-24,4	-22,1	-15,8	-16,3	-15,2	-15,5	-16,0	-15,0
1,5	-26,8	-27,5	-24,7	-25,4	-25,9	-23,7	-17,4	-17,9	-16,8	-17,1	-17,6	-16,5
1,75	-28,2	-28,8	-26,0	-26,7	-27,3	-25,0	-18,7	-19,2	-18,1	-18,5	-18,9	-17,9
2,0	-29,2	-30,0	-27,4	-27,8	-28,5	-26,1	-19,8	-20,4	-19,2	-19,6	-20,1	-19,0
2,25	-30,4	-30,9	-28,1	-28,9	-29,5	-27,2	-20,9	-21,5	-20,3	-20,5	-21,1	-20,1
2,5	-31,2	-31,9	-29,2	-29,8	-30,4	-28,1	-21,8	-22,3	-21,2	-21,5	-22,0	-20,9
2,75	-31,6	-32,8	-30,1	-30,7	-31,2	-28,8	-22,6	-23,1	-22,0	-22,3	-22,9	-21,8
3,0	-32,7	-33,6	-30,8	-31,4	-32,0	-29,7	-23,4	-23,9	-22,7	-23,1	-23,7	-22,6
3,25	-33,4	-34,3	-31,5	-32,1	-32,6	-30,3	-24,1	-24,4	-23,4	-23,9	-24,3	-23,2
3,5	-34,1	-34,6	-32,1	-32,7	-33,3	-31,1	-24,7	-25,2	-24,1	-24,5	-24,9	-23,8
3,75	-34,5	-35,4	-32.8	-33,3	-33,8	-31,7	-25,3	-25,9	-24,7	-24,9	-25,6	-24,5
4,0	-35,4	-36,1	-33.4	-33,9	-34,4	-32,1	-25,9	-26,4	-25,3	-25,7	-26,1	-24,8
4,5	-36,3	-37,0	-34,0	-34,9	-35,5	-33,2	-26,9	-27,4	-26,2	-26,6	-27,2	-26,1
5,0	-37,1	-37,7	-35,2	-35,8	-36,4	-34,2	-27,7	-28,4	-27,2	-27,6	-28,0	-27,0
5,5	-37,9	-38,8	-36,1	-36,6	-37,3	-35,0	-28,7	-29,2	-28,0	-28,3	-28,9	-27,8
6,0	-38,6	-39,4	-36,8	-37,4	-38,0	-35,7	-29,4	-29,9	-28,8	-29,1	-29,6	-28,6
6,5	-39,4	-40,1	-37,5	-38,1	-38,6	-36,4	-30,0	-30,7	-29,5	-29,8	-30,3	-29,3
7,0	-40,0	-40,7	-38,2	-38,7	-39,4	-37,1	-30,6	-31,2	-30,1	-30,5	-31,0	-29,9
7,5	-40,7	-41,5	-38,6	-39,4	-40,0	-37,7	-31,3	-31,8	-30,5	-31,0	-31,6	-30,5
8,0	-40,9	-41,9	-39,2	-39,9	-40,5	-38,2	-31,9	-32,5	-31,2	-31,7	-32,2	-30,9
8,5	-41,9	-42,5	-39,8	-40,4	-41,0	-38,8	-32,4	-32,9	-31,8	-32,2	-32,7	-31,6
9,0	-42,3	-43,0	-40,3	-40,9	-41,5	-39,3	-32,9	-33,5	-32,3	-32,7	-33,2	-32,1
9,5	-42,7	-43,6	-40,5	-41,4	-42,0	-39,7	-33,4	-34,0	-32,7	-33,2	-33,7	-32,6
10,0	-43,2	-43,6	-41,3	-41,8	-42,4	-40,2	-33,8	-34,4	-33,2	-33,6	-34,1	-33,0
10,5	-43,5	-44,4	-41,7	-42,3	-42,8	-40,6	-34,0	-34,8	-33,6	-34,0	-34,4	-33,4
11,0	-43,9	-44,9	-42,1	-42,6	-43,2	-41,0	-34,7	-35,2	-34,0	-34,3	-34,9	-33,8
11,5	-44,4	-45,0	-42,5	-43,1	-43,6	-41,4	-35,0	-35,6	-34,2	-34,8	-35,3	-34,2
12,0	-44,8	-45,7	-42,8	-43,4	-43,9	-41,8	-35,4	-36,0	-34,8	-35,2	-35,7	34,4
12,75	-45,1	-46,1	-43,4	-44,0	-44,6	-42,3	-36,0	-36,4	-35,3	-35,7	-36,1	-35,1

Table 15: Ideal values of NSA for vertical polarization (1 GHz to 12,75 GHz)

	Ideal NSA (dB)											
	Range length: 3m Various positions						Range length: 10m Various positions					
Freq: (GHz)	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**	**1**	**2 3**	**4 5**	**6**	**7 8**	**9 10**
1,0	-21,4	-22,4	-20,1	-19,3	-20,8	-17,8	-13,6	-14,0	-13,0	-12,8	-13,3	-12,4
1,25	-23,2	-24,4	-22,2	-21,2	-22,8	-19,8	-15,4	-15,9	-14,8	-14,8	-15,1	-14,3
1,5	-24,6	25,9	-23,6	-22,8	-24,3	-21,4	-17,0	-17,6	-16,5	-16,3	-16,8	-15,9
1,75	-26,3	-27,3	-25,0	-24,1	-25,7	-22,7	-18,4	-19,0	-17,9	-17,7	-18,1	-17,2
2,0	-27,4	-28,4	-26,2	-25,3	-26,8	-23,8	-19,6	-20,0	-19,0	-18,8	-19,2	-18,4
2,25	-28,3	-29,4	-27,0	-26,3	-27,9	-24,9	-20,5	-21,0	-20,0	-19,9	-20,3	-19,4
2,5	-29,0	-30,4	-28,3	-27,2	-28,8	-25,7	-21,4	-22,1	-20,9	-20,8	-21,1	-20,3
2,75	-30,2	-31,1	-28,8	-28,0	-29,6	-26,6	-22,4	-22,9	-21,8	-21,4	-22,1	-21,2
3,0	-30,9	-32,0	-29,3	-28,8	-30,3	-27,4	-23,1	-23,5	-22,5	-22,4	22,7	-21,9
3,25	-31,5	-32,7	-30,3	-29,3	-31,1	-28,0	-23,8	-24,1	-23,3	-23,1	-23,5	-22,6
3,5	-32,3	-33,1	-31,0	-30,1	-31,7	-28,7	-24,4	-24,9	-23,9	-23,7	-24,0	-23,2
3,75	-32,5	-33,9	-31,8	-30,8	-32,3	-29,3	-24,9	-25,5	-24,4	-24,3	-24,7	-23,8
4,0	-33,4	-34,4	-32,2	-31,3	-32,9	-29,8	-25,5	-26,1	-25,0	-24,8	-25,3	-24,4
4,5	-34,5	-35,4	-32,6	-32,3	-33,9	-30,9	-26,5	-27,2	-26,0	-25,9	-26,3	-25,4
5,0	-35,3	-36,4	-34,3	-33,2	-34,8	-31,8	-27,3	-28,0	-26,9	-26,8	-27,1	-26,3
5,5	-36,2	-37,2	-34,7	-34,0	-35,7	-32,6	-28,3	-28,7	-27,7	-27,4	-28,1	-27,2
6,0	-36,8	-38,0	-35,4	-34,8	-36,3	-33,4	-28,9	-29,6	-28,5	-28,4	-28,9	-27,9
6,5	-37,5	-38,6	-36,3	-35,3	-37,1	-34,0	-29,8	-29,8	-29,3	-29,1	-29,5	-28,5
7,0	-38,3	-38,7	-37,0	-36,1	-37,7	-34,7	-30,2	-30,9	-29,9	-29,7	-29,8	-29,2
7,5	-38,4	-39,9	-37,8	-36,8	-38,3	-35,3	-31,0	-31,5	-30,4	-30,3	-30,8	-29,9
8,0	-39,5	-40,5	-38,2	-37,3	-38,9	-35,9	-31,6	-32,0	-31,0	-30,9	-31,3	-30,4
8,5	-39,9	-41,1	-38,6	-37,8	-39,4	-36,4	-32,1	-32,6	-31,6	-31,4	-31,8	-30,9
9,0	-40,3	-41,4	-38,7	-38,3	-39,9	-36,9	-32,6	-33,1	-31,9	-31,9	-32,4	-31,5
9,5	-40,5	-42,0	-39,8	-38,8	-40,3	-37,4	-33,0	-33,7	-32,5	-32,4	-32,8	-31,9
10,0	-41,3	-42,4	-40,2	-39,2	-40,9	-37,8	-33,3	-34,0	-33,0	-32,8	-33,1	-32,3
10,5	-41,8	-42,8	-40,5	-39,7	-41,3	-38,1	-33,6	-34,5	-33,4	-33,2	-33,2	-32,8
11,0	-42,2	-42,9	-40,9	-40,0	-41,7	-38,6	-34,3	-34,9	-33,6	-33,4	-34,1	-33,2
11,5	-42,4	-43,7	-41,4	-40,5	-42,0	-39,0	-34,8	-35,1	-33,8	-33,9	-34,5	-33,5
12,0	-42,4	-44,0	-41,5	-40,8	-42,4	-39,4	-35,2	-35,6	-34,6	-34,4	-34,9	-33,9
12,75	-43,4	-44,6	-42,3	-41,4	-42,8	-39,8	-35,6	-36,1	-35,0	-34,9	-35,4	-34,4

Completion of the results sheet

The next stage is to fill in the column headed "Overall value". The relevant values are determined by subtracting the combined values in the columns "V_{site}", "AF_T" and "AF_R" from the value in the "V_{direct} " column i.e.:

$$\text{"Overall value"} = \text{"}V_{direct}\text{"} - V_{site}\text{"} - \text{"}AF_T\text{"} - \text{"}AF_R\text{"}$$

The resulting value is the measured NSA for the open area test site.

The final stages in determining the quality of the open area test site are to complete the column headed "Ideal value" in the results sheet by taking the relevant values from tables 14 or 15 (for horizontal and vertical polarization respectively) and to calculate the entries for the "Difference" column from:

"Difference" = "Overall value" - "Ideal value"

The resulting values in the "Difference" column represent the variation between the theoretical and the measured performance of the open area test site.

6.5.4 Report format

It is suggested that the results of the verification are presented in two ways, firstly as indicated in the completed results sheets and secondly in the form of plots of the "Difference" column against frequency for each polarization as shown in figure 30.

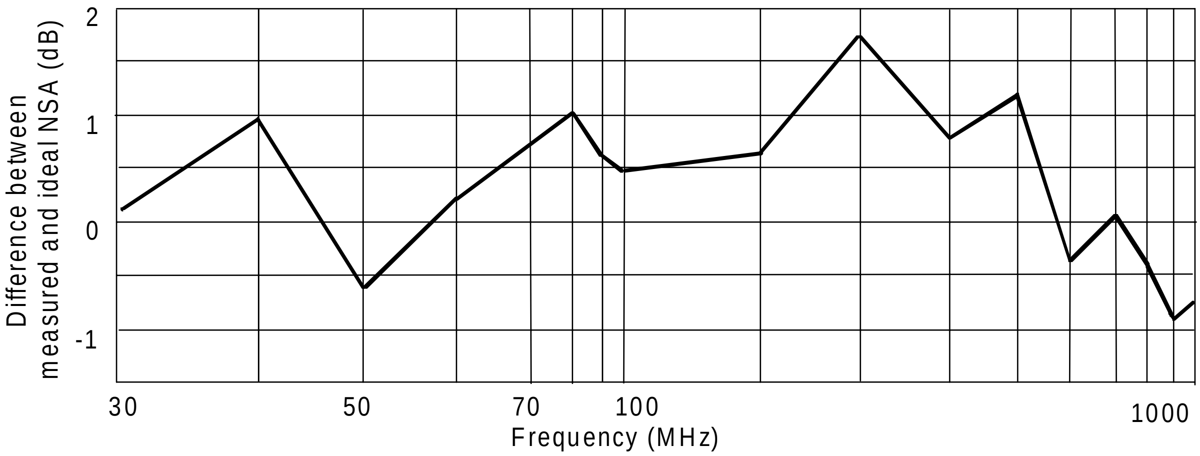

Figure 30: Plot of the difference between the measured and the ideal NSA against frequency

6.6 Calculation of measurement uncertainty (Procedure 1)

The column headed "Overall" in the results sheet is completed during the processing of the results for the verification procedure. The values entered in this column are the measured NSA figures for the open area test site.

The value, at any particular frequency, for the measured NSA is "Direct" (reference value) less "Site" (the value appearing on the receiver during the NSA measurement) less the sum of "Transmit Antenna factor AF_T ", "Receive Antenna factor AF_R " and "Mutual coupling correction AF_{TOT} " i.e.:

NSA = "Direct" - "Site" - "Transmit Antenna factor " - "Receive Antenna factor " - "Mutual coupling correction"

As an example, let the direct attenuation be +10 dBm and the received level during the site measurement be -33 dBm. Putting both the antenna factors at 3,9 dB and the mutual coupling correction at 2,1 dB gives a measured NSA value of:

$$NSA = [10 \text{ dBm} - (-33 \text{ dBm})] - (3{,}9 \text{ dB} + 3{,}9 \text{ dB} + 2{,}1 \text{ dB}) = 33{,}1 \text{ dB}$$

There are uncertainties in each of these components for the NSA and an example of a typical calculation of the expanded uncertainty is now given. A fully worked example can be found in clause 4 of ETR 273-1-2 [10].

6.6.1 Uncertainty contribution, direct attenuation measurement

The verification procedure involves two different measurement stages and the derivation of NSA. The first stage (the reference) is with all the items of test equipment connected directly together via an adapter between the attenuators as shown in figure 31 (components shown shaded are common to both stages of the procedure).

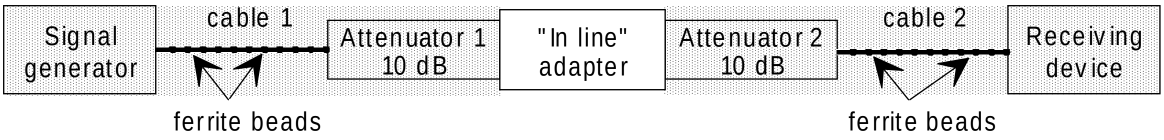

Figure 31: Stage 1: Direct attenuation measurement

Despite the commonality of most of the components to both stages of this procedure, the mismatch uncertainty contribution for both stages has to be calculated and included in the uncertainty calculations. This is the result of load conditions varying (i.e. antennas replacing the adapter in the second stage). Conversely, as a result of this commonality, the uncertainty contribution of some of the individual components will cancel.

The magnitude of the random uncertainty contribution to each stage of the procedure can be assessed from multiple repetition of the direct attenuation measurement. All of the uncertainty components which contribute to this stage of the test are listed in table 16. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

A fully worked example calculation can be found in ETR 273-1-2 [10].

Table 16: Contributions from the direct attenuation measurement

uj or i	Description of uncertainty contributions	dB
u_{j35}	*mismatch: direct attenuation measurement*	
u_{j38}	*signal generator: absolute output level*	
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: receiving antenna cable*	0,00
u_{j19}	*cable factor: transmitting antenna cable*	0,00
u_{j41}	*insertion loss: receiving antenna cable*	0,00
u_{j41}	*insertion loss: transmitting antenna cable*	0,00
u_{j40}	*insertion loss: receiving antenna attenuator*	0,00
u_{j40}	*insertion loss: transmitting antenna attenuator*	0,00
u_{j42}	*insertion loss: adapter*	
u_{j47}	*receiving device: absolute level*	0,00
u_{j48}	*receiving device: linearity*	0,00
u_{i01}	*random uncertainty*	

The standard uncertainties from table 16 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ direct\ attenuation\ measurement}$) for the direct attenuation measurement in dB.

6.6.2 Uncertainty contribution, NSA measurement

This stage involves removing the adapter and connecting each attenuator to an antenna as shown in figure 32, and recording the new level on the receiving device.

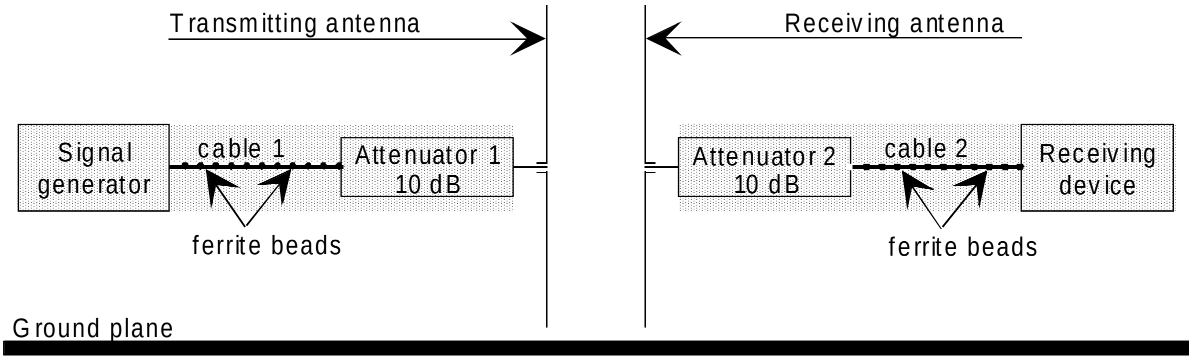

Figure 32: Stage 2: NSA measurement

The difference in received levels (after allowance for any correction factors which may be appropriate), for the same signal generator output level, reveals the NSA. All of the uncertainty components which contribute to this stage of the test are listed in table 17. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 17: Contributions from the NSA actual measurement

uj or i	Description of uncertainty contributions	dB
u_{j36}	*mismatch: transmitting part*	
u_{j37}	*mismatch: receiving part*	
u_{j38}	*signal generator: absolute output level*	0,00
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: receiving antenna cable*	
u_{j19}	*cable factor: transmitting antenna cable*	
u_{j41}	*insertion loss: receiving antenna cable*	0,00
u_{j41}	*insertion loss: transmitting antenna cable*	0,00
u_{j40}	*insertion loss: receiving antenna attenuator*	0,00
u_{j40}	*insertion loss: transmitting antenna attenuator*	0,00
u_{j47}	*receiving device: absolute level*	
u_{j48}	*receiving device: linearity*	
u_{j16}	*range length*	0,00
u_{j18}	*correction: measurement distance*	0,00
u_{j44}	*antenna: antenna factor of the receiving antenna*	
u_{j44}	*antenna: antenna factor of the transmitting antenna*	
u_{j46}	*antenna: tuning of the receiving antenna*	
u_{j46}	*antenna: tuning of the transmitting antenna*	
u_{j22}	*position of the phase centre: receiving antenna*	
u_{j22}	*position of the phase centre: transmitting antenna*	
u_{j17}	*correction: off boresight angle in the elevation plane*	0,00
u_{j15}	*mutual coupling: receiving antenna to its image in the ground plane*	
u_{j15}	*mutual coupling: transmitting antenna to its image in the ground plane*	0,00
u_{j10}	*mutual coupling: transmitting antenna to the receiving antenna*	0,00
u_{j12}	*mutual coupling: interpolation of mutual coupling and mismatch loss correction factors*	0,00
u_{j34}	*ambient effect*	0,00
u_{i01}	*random uncertainty*	

The standard uncertainties from table 19 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ NSA\ measurement}$) for the NSA measurement in dB.

6.6.3 Expanded uncertainty of the verification procedure

The combined standard uncertainty of the results of the verification procedure is the combination of the components outlined in subclauses 6.6.1 and 6.6.2. The components to be combined are $u_{c\ direct\ attenuation\ measurement}$ and $u_{c\ NSA\ measurement}$.

$$u_c = \sqrt{u_{c\,direct\,attenuation\,measurement}^2 + u_{c\,NSA\,measurement}^2} = \_\_,\_\_\,\text{dB}$$

The expanded uncertainty is ± 1,96 x u_c = ± __,__ dB at a 95 % confidence level.

6.7 Calculation of measurement uncertainty (Procedure 2)

The column headed "Overall" in the results sheet is completed during the processing of the results for the verification procedure. The values entered in this column are the measured NSA figures for the open area test site.

The value, at any particular frequency, for the measured NSA is "Direct" (reference value) less "Site" (the value appearing on the receiver during the NSA measurement) less the sum of "Transmit Antenna factor AF_T " and "Receive Antenna factor AF_R " i.e.:

NSA = "Direct" - "Site" - "Transmit Antenna factor" - "Receive Antenna factor"

As an example, let the direct attenuation value be 10 dBm and the received level during the site measurement be -33 dBm. Putting each antenna factor at 3,9 dB gives a measured NSA value of:

NSA = [0 dBm - (-43 dBm)] - (7,8 dB) = 35,2 dB

There are uncertainties in each of these three components for the NSA and an example of a typical calculation of the expanded uncertainty is now given. A fully worked example can be found in clause 4 of ETR 273-1-2 [10].

6.7.1 Uncertainty contribution, direct attenuation measurement

The verification procedure involves two different measurement stages and the derivation of NSA. The first stage (the reference) is with all the items of test equipment connected directly together via an adapter between the attenuators as shown in figure 33 (components shown shaded are common to both stages of the procedure).

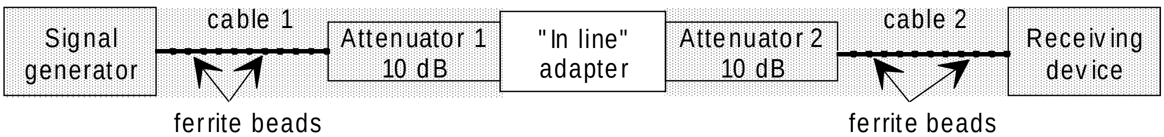

Figure 33: Stage 1: Direct attenuation measurement

Despite the commonality of most of the components to both stages of this procedure, the mismatch uncertainty contribution for both stages has to be calculated and included in the uncertainty calculations. This is the result of load conditions varying (i.e. antennas replacing the adapter in the second stage). Conversely, as a result of this commonality, the uncertainty contribution of some of the individual components will cancel.

The magnitude of the random uncertainty contribution to each stage of the procedure can be assessed from multiple repetition of the direct attenuation measurement. All of the uncertainty components which contribute to this stage of the test are listed in table 18. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

A fully worked example calculation can be found in clause 4 of ETR 273-1-2 [10].

Table 18: Contributions from the direct attenuation measurement

uj or i	Description of uncertainty contributions	dB
u_{j35}	*mismatch: direct attenuation measurement*	
u_{j38}	*signal generator: absolute output level*	
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: receiving LPDA cable*	0,00
u_{j19}	*cable factor: transmitting LPDA cable*	0,00
u_{j41}	*insertion loss: receiving LPDA cable*	0,00
u_{j41}	*insertion loss: transmitting LPDA cable*	0,00
u_{j40}	*insertion loss: receiving LPDA attenuator*	0,00
u_{j40}	*insertion loss: transmitting LPDA attenuator*	0,00
u_{j42}	*insertion loss: adapter*	
u_{j47}	*receiving device: absolute level*	0,00
u_{j48}	*receiving device: linearity*	0,00
u_{i01}	*random uncertainty*	

The standard uncertainties from table 18 should be combined by RSS in accordance with of clause 5 ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ direct\ attenuation\ measurement}$) for the direct attenuation measurement in dB.

6.7.2 Uncertainty contribution, NSA measurement

This stage involves removing the adapter and connecting each attenuator to an antenna as shown in figure 34, and recording the new level on the receiving device.

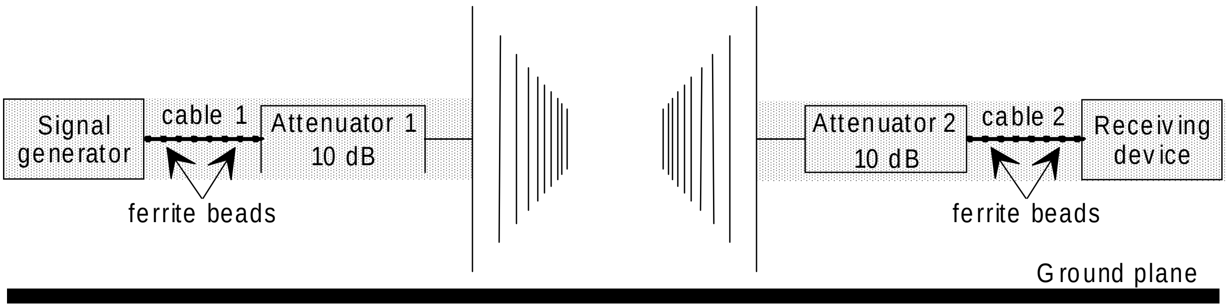

Figure 34: NSA measurement

The difference in received levels (after allowance for any correction factors which may be appropriate), for the same signal generator output level, reveals the NSA. All the uncertainty components which contribute to this stage of the test are listed in table 19. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 19: Contributions from the measurement

uj or i	Description of uncertainty contributions	dB
u_{j36}	*mismatch: transmitting part*	
u_{j37}	*mismatch: receiving part*	
u_{j38}	*signal generator: absolute output level*	0,00
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: receiving LPDA cable*	
u_{j19}	*cable factor: transmitting LPDA cable*	
u_{j41}	*insertion loss: receiving LPDA cable*	0,00
u_{j41}	*insertion loss: transmitting LPDA cable*	0,00
u_{j40}	*insertion loss: receiving LPDA attenuator*	0,00
u_{j40}	*insertion loss: transmitting LPDA attenuator*	0,00
u_{j47}	*receiving device: absolute level*	
u_{j48}	*receiving device: linearity*	
u_{j16}	*range length*	0,00
u_{j18}	*correction: measurement distance*	0,00
u_{j44}	*antenna: antenna factor of the receiving LPDA*	
u_{j44}	*antenna: antenna factor of the transmitting LPDA*	
u_{j22}	*position of the phase centre: receiving LPDA*	
u_{j22}	*position of the phase centre: transmitting LPDA*	
u_{j23}	*position of the phase centre: LPDA*	
u_{j17}	*correction: off boresight angle in the elevation plane*	
u_{j15}	*mutual coupling: receiving LPDA to its image in the ground plane*	
u_{j15}	*mutual coupling: transmitting LPDA to its image in the ground plane*	
u_{j34}	*ambient effect*	0,00
u_{i01}	*random uncertainty*	

The standard uncertainties from table 19 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ NSA\ measurement}$) for the NSA measurement of in dB.

6.7.3 Expanded uncertainty of the verification procedure

The combined standard uncertainty of the results of the verification procedure is the combination of the components outlined in subclauses 6.7.1 and 6.7.2. The components to be combined are $u_{c\ direct\ attenuation\ measurement}$ and $u_{c\ NSA\ measurement}$.

$$u_c = \sqrt{u_{c\,direct\,attenuation\,measurement}^2 + u_{c\,NSA\,measurement}^2} = \_\_,\_\_\,\mathrm{dB}$$

The expanded uncertainty is ± 1,96 x u_c = ± __,__ dB at a 95 % confidence level.

6.8 Summary

The expanded uncertainty values derived in subclauses 6.6.3 and 6.7.3 reveal the uncertainty with which the NSA can be measured. Any value of NSA which varies by more than these uncertainty values from the theoretical value is probably due to imperfection(s) in the site. These imperfections may be due to reflections from a range of possible sources on the open area test site at the time the verification process is carried out.

7 Test methods

7.1 Introduction

The following test methods apply to integral antenna devices only i.e. EUTs not fitted with either a permanent or a temporary external antenna connector. The Spurious emission test also applies to EUTs with a detachable antenna.

The range length of the open area test site should be adequate to allow for testing in the far-field of the EUT i.e. the range length should be equal to or exceed:

$$\frac{2(d_1 + d_2)^2}{\lambda}$$

where:

d_1 is the largest dimension of the EUT/dipole after substitution (m);
d_2 is the largest dimension of the test antenna (m);
λ is the test frequency wavelength (m).

It should be noted that in the substitution part of these tests, where both test and substitution/measuring antennas are half wavelength dipoles, this minimum range length for far-field testing would be:

$$2\lambda$$

It should be stated in the test report when either of these conditions is not met. The additional contribution to the measurement uncertainty which results can be incorporated into the analysis of the results.

7.1.1 Site preparation

The cables for both ends of the test site should be routed horizontally away from the testing area for a minimum of 2 m. They should then be allowed to drop vertically towards the ground plane, through which they should pass to the test equipment. These cables should be dressed with ferrite beads, spaced 0,15 m apart for their entire lengths above the ground plane. The routeing and dressing of the cables should be identical to the verification procedure set-up.

NOTE: Where a cable drum is incorporated with the antenna mast, the routeing requirement and ferrite beading of the cables may be impossible to comply with. In such cases increased measurement uncertainty results.

Calibration data for items of test equipment used should be available and valid. For both the test and substitution/measuring antennas, the data should include gain relative to an isotropic radiator (or antenna factor) against frequency. Also, the VSWR of the substitution/measuring antenna should be known.

The calibration data for all cables and attenuators used should include insertion loss and VSWR throughout the entire frequency range of the tests. All VSWR and insertion loss figures should be recorded in the log book results sheet for the specific test.

Where correction factors/tables are required, these should be immediately available.

For all items of test equipment, the maximum errors they exhibit should be known along with the distribution of the error e.g.:

- cable loss: ± 0,5 dB with a rectangular distribution;
- measuring receiver: 1,0 dB (standard deviation) signal level accuracy with a Gaussian error distribution.

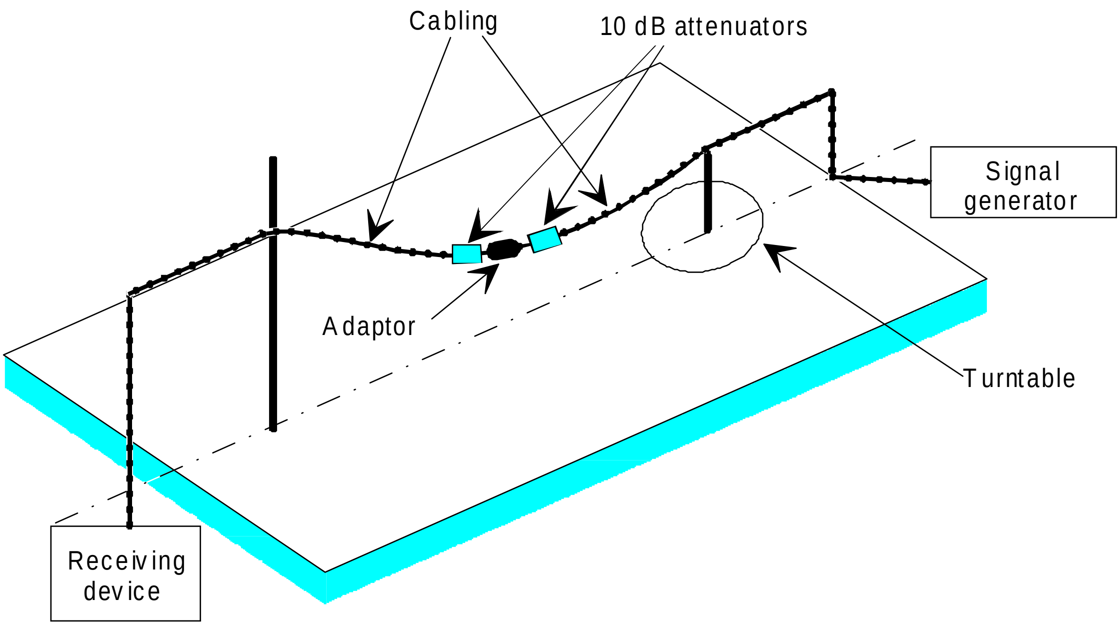

Figure 35: Open area test site set-up for daily system checking

At the start of each day, system checks should be made on the test equipment used on the open area test site. The following checking procedures, as a minimum requirement, should be carried out.

1) All items of test equipment requiring electrical supplies should be connected to their power sources, switched on and allowed adequate time to stabilize, as recommended by the manufacturers. Where no stabilization period is not given by a manufacturer, 30 minutes should be allowed. After this time period those items of test equipment which possess the facility should have their self test/self calibration procedures performed.

2) A signal generator should be connected to the existing cabling at the turntable end. The other end of this cable should be connected via a calibrated coaxial cable/10 dB attenuator/adapter/10 dB attenuator/calibrated coaxial cable combination to existing cabling at the other end of the test site. This existing cable should be connected to a receiving device (see figure 35). Where the use of a cable is impractical due to the arrangements on the test site, bicones or other suitable antennas could be connected at both ends as appropriate. The signal generator should be scanned across the appropriate frequency range and the response of the receiving device noted. It should be compared with previous tests carried out under similar conditions. Any anomalies should be investigated.

7.1.2 Preparation of the EUT

The manufacturer should supply information about the EUT covering the operating frequency, polarization, supply voltage(s) and the reference face. Additional information, specific to the type of EUT should include, where relevant, carrier power, channel spacing, whether different operating modes are available (e.g. high and low power modes) and if operation is continuous or is subject to a maximum test duty cycle (e.g. 1 minute on, 4 minutes off).

Where necessary, a mounting bracket of minimal size should be available for mounting the EUT on the turntable. This bracket should be made from low conductivity, low relative dielectric constant (i.e. less than 1,5) material(s) such as expanded polystyrene, balsawood, etc.

The presence of the cables supplying power can affect the measured performance of the EUT. For this reason, attempts should be made to make them "transparent" as far as the testing is concerned. This can be achieved by routeing them by the shortest possible paths down to, and through, the ground plane. Additionally, where possible, these leads should be twisted together and loaded with ferrite beads at 0,15 m spacing.

7.1.3 Standard antennas

In the frequency band 30 MHz to 1 000 MHz, except where stipulated, both test and substitution/measuring antennas should be tuned half-wavelength dipoles (constructed as detailed in ANSI C63.5 [1]) aligned for the same polarization.

NOTE: Due to size constraints a shortened dipole is used over part of this frequency band. For uniformity of procedures across open area test sites and both types of anechoic chamber, a shortened dipole is used from 30 MHz to 80 MHz. At all these frequencies the 80 MHz arm length (0,889 m) is used attached to the 20 MHz to 65 MHz balun for all test frequencies from 30 to 65 MHz inclusive and to the 65 MHz to 180 MHz balun for 65 MHz to 80 MHz. Tuned half wavelength dipoles, attached to their matching baluns are used for all frequencies in the band 80 MHz to 1 000 MHz inclusive. Table 20 details dipole arm lengths (as measured from the centre of the balun block) and balun type against frequency. Where the test frequency does not correspond to a set frequency in the table, the arm length to be used should be determined by linear interpolation between the closest set values.

Table 20: Dipole arm length and balun type against frequency

<table>
<tr><th>Frequency (MHz)</th><th>Dipole arm length (m)</th><th>Balun type</th><th>Frequency (MHz)</th><th>Dipole arm length (m)</th><th>Balun type</th></tr>
<tr><td>30</td><td>0,889</td><td rowspan="6">20 MHz to 65 MHz</td><td>160</td><td>0,440</td><td rowspan="2">65 MHz to 180 MHz</td></tr>
<tr><td>35</td><td>0,889</td><td>180</td><td>0,391</td></tr>
<tr><td>40</td><td>0,889</td><td>200</td><td>0,352</td><td rowspan="4">180 MHz to 400 MHz</td></tr>
<tr><td>45</td><td>0,889</td><td>250</td><td>0,283</td></tr>
<tr><td>50</td><td>0,889</td><td>300</td><td>0,235</td></tr>
<tr><td>60</td><td>0,889</td><td>400</td><td>0,175</td></tr>
<tr><td>70</td><td>0,889</td><td rowspan="6">65 MHz to 180 MHz</td><td>500</td><td>0,143</td><td rowspan="6">400 MHz to 1 000 MHz</td></tr>
<tr><td>80</td><td>0,889</td><td>600</td><td>0,117</td></tr>
<tr><td>90</td><td>0,791</td><td>700</td><td>0,102</td></tr>
<tr><td>100</td><td>0,714</td><td>800</td><td>0,089</td></tr>
<tr><td>120</td><td>0,593</td><td>900</td><td>0,079</td></tr>
<tr><td>140</td><td>0,508</td><td>1 000</td><td>0,076</td></tr>
</table>

7.1.4 Mutual coupling and mismatch loss correction factors

Correction factors are included where relevant, to allow for mutual coupling and mismatch loss for the 30 MHz to 180 MHz band, based on using the recommended ANSI C63.5 [1] dipoles. These have been calculated by computer modelling of their baluns, sectional arms and the testing arrangements (i.e. range length and optimized height above the ground plane) using MiniNEC. The factors are only valid for this particular type of dipole. However, if this type is unavailable, an alternative could be used. This alternative should be a tuned half wavelength dipole at the particular test frequency. Since correction factors have not been calculated in this ETR for any type other than the ANSI C63.5 [1] dipoles this will result in a greater expanded uncertainty for the measurement unless the test house/manufacturer has performed equivalent modelling on the dipoles used.

7.1.5 Power supplies to EUT

All tests should be performed using power supplies wherever possible, including tests on EUTs designed for battery-only use. In all cases, power leads should be connected to the EUTs supply terminals (and monitored with a digital voltmeter) but the battery should remain present, electrically isolated from the rest of the EUT, possibly by putting tape over its contacts. All leads involved should be taken down to the ground plane by the shortest possible routes, twisting pairs together and loading with ferrite beads at 0,15 m spacing.

7.1.6 Restrictions

The restriction that no part of any antenna should come within 0,25 m of the ground plane should be applied at all times throughout these test methods.

7.2 Transmitter tests

7.2.1 Frequency error (30 MHz to 1 000 MHz)

Definition

The frequency error of a transmitter is the difference between the measured carrier frequency in the absence of modulation and the nominal frequency of the transmitter as stated by the manufacturer.

7.2.1.1 Apparatus required

- digital voltmeter;
- ferrite beads;
- 10 dB attenuators;
- power supply;
- connecting cables;
- open area test site;
- test antenna (a half wavelength dipole, bicone or a LPDA);
- frequency counter.

The type and serial numbers of all items of test equipment should be recorded in the log book results sheet (table 21).

NOTE: The half wavelength dipole antennas, incorporating matching/transforming baluns, for the procedure are available in the following bands: 20 MHz to 65 MHz, 65 MHz to 180 MHz, 180 MHz to 400 MHz, 400 MHz to 1 000 MHz. Constructional details are contained in ANSI C63.5 [1]. In the recommended antenna scheme for this band, a shortened dipole is used at all frequencies from 30 MHz to 80 MHz.

7.2.1.2 Method of measurement

1) The measurement should always be performed in the absence of modulation.

2) The EUT should be mounted on a turntable whose mounting surface is at the height (above the ground plane) specified in the relevant standard. The EUT should be mounted in an orientation which matches that of its normal usage as stated by the manufacturer. This orientation and mounting configuration should be recorded in the log book results sheet (table 21).

   NOTE 1: The turntable should be constructed from non-conducting, low relative dielectric constant (preferably less than 1,5) material(s).

3) The test antenna (dipole, bicone or LPDA) should be mounted on the antenna mast and oriented for the stated polarization of the EUT. For cases in which the test antenna is a tuned half wavelength dipole, this should be tuned to the nominal frequency. The output of the test antenna should be connected to the frequency counter via a 10 dB attenuator and the calibrated, ferrited coaxial cable associated with that end of the test site (see figure 36). The phase centre of the test antenna should be at the same height above the floor as the mid point of the EUT.

NOTE 2: Where a dipole is used, frequencies below 80 MHz require a shortened version (as defined in subclause 7.1.3) to be used. For any frequency, the dipole arm length (given in table 20) is defined from the centre of the balun block to the tip of the arm. From a fully extended state, each telescopic element, in turn, should be "pushed in" from the tip until the required length is obtained. The outermost section needs to fully compress before any of the others, and so on. Table 20 also gives the choice of balun for set frequencies. Where the test frequency does not correspond to a set frequency in the table, the arm length to be used should be determined by linear interpolation between the closest set values.

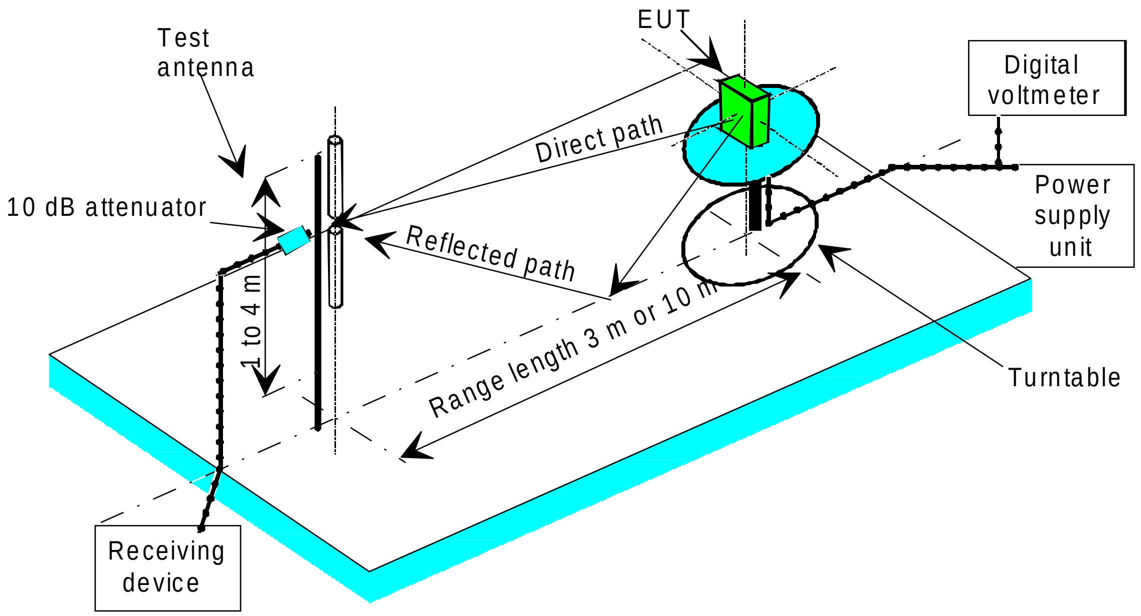

Figure 36: Open area test site set-up for the frequency error test

4) The EUT should be switched on without modulation, allowed adequate time to stabilize and the resolution of the frequency counter adjusted to read to the nearest Hz.

5) For cases in which no reading is given on the frequency counter, the height of the test antenna on the mast should be varied until a reading does appear.

6) The value of the frequency displayed on the counter should be recorded in the log book results sheet (table 21).

NOTE 3: In cases where the frequency does not appear stable, this might require observations over a 30 second or 1 minute time period, noting the highest and lowest readings and estimating the average value. In these cases it is the average value that should be recorded in the log book results sheet (table 21).

7.2.1.3 Procedure for completion of the results sheets

There are only two values that need to be derived before the overall results sheet (table 22) can be completed. Firstly the value for frequency error (from a straightforward calculation of recorded frequency minus the nominal frequency) and secondly, the value of the expanded uncertainty for the test. This should be carried out as given in subclause 7.2.2 and the resulting value entered in the overall results sheet (table 24).

7.2.1.4 Log book entries

Table 21: Log book results sheet

FREQUENCY ERROR			**Date:**		**PAGE 1 of 1**
Temperature:.........°C		**Humidity:...............%**		**Frequency:.............MHz**	
Manufacturer of EUT:.....................		**Type No:.............**		**Serial No:..................**	
Range length :.......................					
Test equipment item	**Type No.**	**Serial No.**	**VSWR**	**Insertion loss**	**Antenna factor/gain**
Test antenna				N/A	
Test antenna attenuator					N/A
Test antenna cable					N/A
Digital voltmeter			N/A	N/A	N/A
Power supply			N/A	N/A	N/A
Ferrite beads			N/A	N/A	N/A
Frequency counter				N/A	N/A
Mounting configuration of EUT					
Reading on frequency counter:			Hz		

7.2.1.5 Statement of results

The results should be presented in tabular form as shown in table 22.

Table 22: Overall results sheet

FREQUENCY ERROR	**Date:**	**PAGE 1 of 1**
Frequency error	Hz	
Expanded uncertainty (95 %)	dB	

7.2.2 Expanded uncertainty for Frequency error test

The method of calculating the expanded uncertainty for tests in which signal levels in dB are involved is equally adopted for the frequency error test in which all the uncertainties are in the units of Hz. That is, all the uncertainty contributions are converted into standard uncertainties and combined by the RSS method under the assumption that they are all stochastic. All the uncertainty components which contribute to the test are listed in table 23. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 23: Contributions from the measurement

uj or i	Description of uncertainty contributions	Hz
u_{i01}	*random uncertainty*	
u_{j09}	*mutual coupling: detuning effect of the test antenna on the EUT*	
u_{j56}	*frequency counter: absolute reading*	

The standard uncertainties from table 23 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. The combined standard uncertainty of the frequency measurement ($u_{c\ contributions\ from\ the\ measurement}$) is the combination of the components outlined above.

$$u_c = u_{c\ contributions\ from\ the\ measurement} = \_\_,\_\_\ \text{Hz}$$

The expanded uncertainty is ± 1,96 x u_c = ± __,__ Hz at a 95 % confidence level.

7.2.3 Effective radiated power (30 MHz to 1 000 MHz)

Definition

The effective radiated power is the power radiated in the direction of the maximum field strength under specified conditions of measurement, in the absence of modulation.

7.2.3.1 Apparatus required

- digital voltmeter;
- ferrite beads;
- 10 dB attenuators;
- power supply;
- connecting cables;
- open area test site;
- test Antenna (half wavelength dipole as detailed in ANSI C63.5 [1] recommended);
- substitution antenna (half wavelength dipole as detailed in ANSI C63.5 [1] recommended);
- receiving device (measuring receiver or spectrum analyser);
- signal generator.

The type and serial numbers of all items of test equipment should be recorded on page 1 of the log book results sheet (table 25).

NOTE: The half wavelength dipole antennas, incorporating matching/transforming baluns, for the procedure are available in the following bands: 20 MHz to 65 MHz, 65 MHz to 180 MHz, 180 MHz to 400 MHz, 400 MHz to 1 000 MHz. Constructional details are contained in ANSI C63.5 [1]. In the recommended antenna scheme for this band, a shortened dipole is used at all frequencies from 30 MHz to 80 MHz.

7.2.3.2 Method of measurement

1) The measurement should always be performed in the absence of modulation.

2) The EUT should be mounted directly onto the turntable, whose surface is at the height (above the ground plane) specified in the relevant Standard, in an orientation which matches that of its normal usage (as stated by the manufacturer). The normal to the reference face of the EUT should point directly down the test site towards the test antenna support. This is the 0° reference angle for the test. This orientation and mounting configuration should be recorded on page 1 of the log book results sheet (table 25). The items of test equipment should be set-up as shown in figure 37.

NOTE 1: The turntable should be constructed from non-conducting, low relative dielectric constant (preferably less than 1,5) material(s).

3) In cases where the position of the phase centre of the EUTs antenna is known, the EUT should be positioned on the turntable such that this phase centre is as coincident with the axis of rotation as possible. Alternatively, if the position of the phase centre is unknown, but the antenna is a single rod which is visible and vertical in normal usage, the axis of the antenna should be used. If neither alternative is possible, the volume centre of the EUT should be used instead.

4) The height above the ground plane of the phase centre (if known) of the EUT should be recorded on page 1 of the log book results sheet (table 25). If the position of the phase centre is unknown, but the antenna is visible, then the height above the ground plane of the point at which the antenna meets the case of the EUT should be recorded. If neither alternative is possible, the volume centre of the EUT should be used instead.

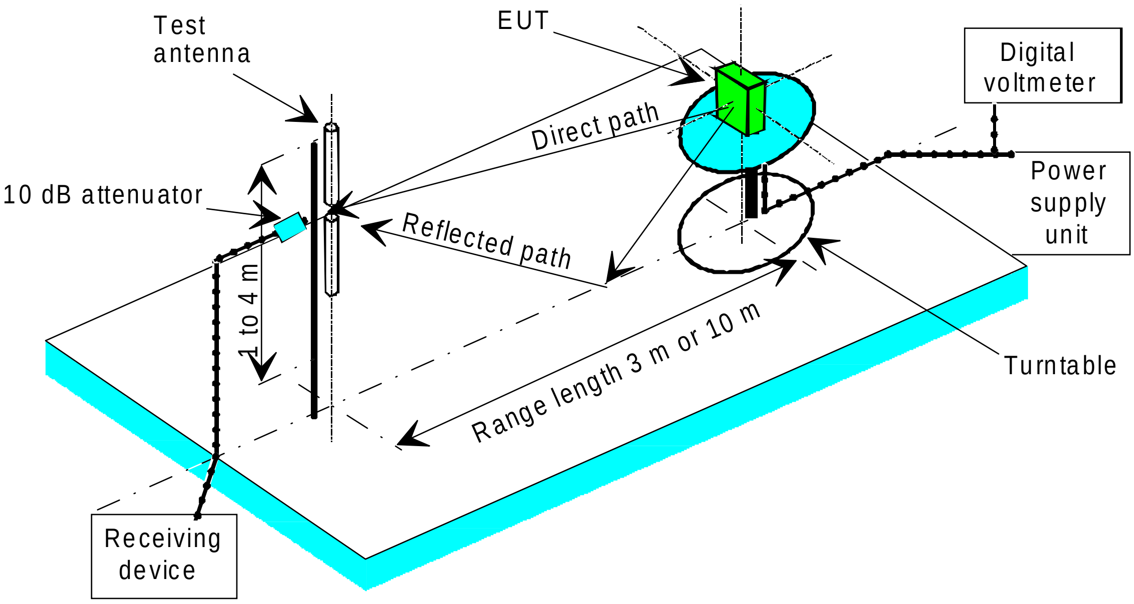

Figure 37: Open area test site set-up for effective radiated power measurement on the EUT

5) The test antenna (in the recommended scheme a tuned ANSI C63.5 [1] half wavelength dipole for frequencies of 80 MHz and above, a shortened dipole for frequencies from 30 to 80 MHz) should be mounted on the antenna mast, tuned to the appropriate frequency and oriented for vertical polarization. Its output should be connected to the receiving device via a 10 dB attenuator and the calibrated, ferrited coaxial cable associated with that end of the test site.

NOTE 2: For all frequencies below 80 MHz, a shortened dipole (as defined in subclause 7.1.3) should be used. The dipole arm length is defined from the centre of the balun block to the tip of the arm. From a fully extended state, each telescopic element, in turn, should be "pushed in" from the tip until the required length is obtained. The outermost section needs to fully compress before any of the others, and so on. Table 20 gives the dipole arm lengths and choice of balun for set frequencies. Where the test frequency does not correspond to a set frequency in the table, the arm length to be used should be determined by linear interpolation between the closest set values.

6) The EUT should be switched on without modulation, and the receiving device tuned to the nominal frequency.

7) The test antenna should be raised and lowered through the specified range of heights (1 m to 4 m, ensuring that no part of the antenna is less than 0,25 m from the ground plane at any time) until the maximum signal level is detected on the receiving device. The height of the test antenna on the mast should be recorded on page 2 of the log book results sheet (table 25).

NOTE 3: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level should be at the top of the height range.

8) The EUT should be rotated through 360° in the horizontal plane until the maximum signal is detected on the receiving device. The angle with reference to the nominal orientation of the EUT and the maximum signal level (dBm) detected by the receiving device should be recorded on page 2 of the log book results sheet (table 25).

9) The EUT should be replaced on the turntable by the substitution antenna (identical to the test antenna), which has been adjusted to correspond to the frequency of the EUT. See figure 38.

10) The height of the phase centre of the substitution antenna should be located at the height recorded in Step 3, whilst the phase centre should lie on the axis of rotation of the turntable.

11) The substitution antenna should be oriented for vertical polarization and connected via a 10 dB attenuator to a calibrated signal generator using the calibrated, ferrited coaxial cable associated with the turntable end of the test site.

12) The signal generator should be tuned to the appropriate frequency and its output level adjusted until the level measured on the receiving device, is at least 20 dB above the level with the output from the signal generator switched off.

13) The test antenna should be raised and lowered through the specified range of heights until the maximum signal level is achieved on the receiving device. The height of the test antenna on the mast should be recorded on page 2 of the log book results sheet (table 25).

NOTE 4: The true maximum may lie beyond the top of the mast, in which case the maximum received level should be at the top of the height range.

14) The substitution antenna should be rotated until the maximum level is detected on the receiving device.

NOTE 5: This is to correct for possible misalignment of a directional beam i.e. dipoles used in horizontally polarized tests. This step can be omitted when dipoles are used in vertically polarized tests.

15) The output level of the signal generator should be adjusted until the level, measured on the receiving device, is identical to that recorded in Step 8. This output signal level (dBm) from the signal generator should be recorded on page 2 of the log book results sheet (table 25).

NOTE 6: In the event of insufficient range of signal generator output level, the receiving device input attenuation should be decreased to compensate. The signal generator output level (dBm) and the change in attenuation (dB) should both be recorded on page 2 of the log book results sheet (table 25) in this case.

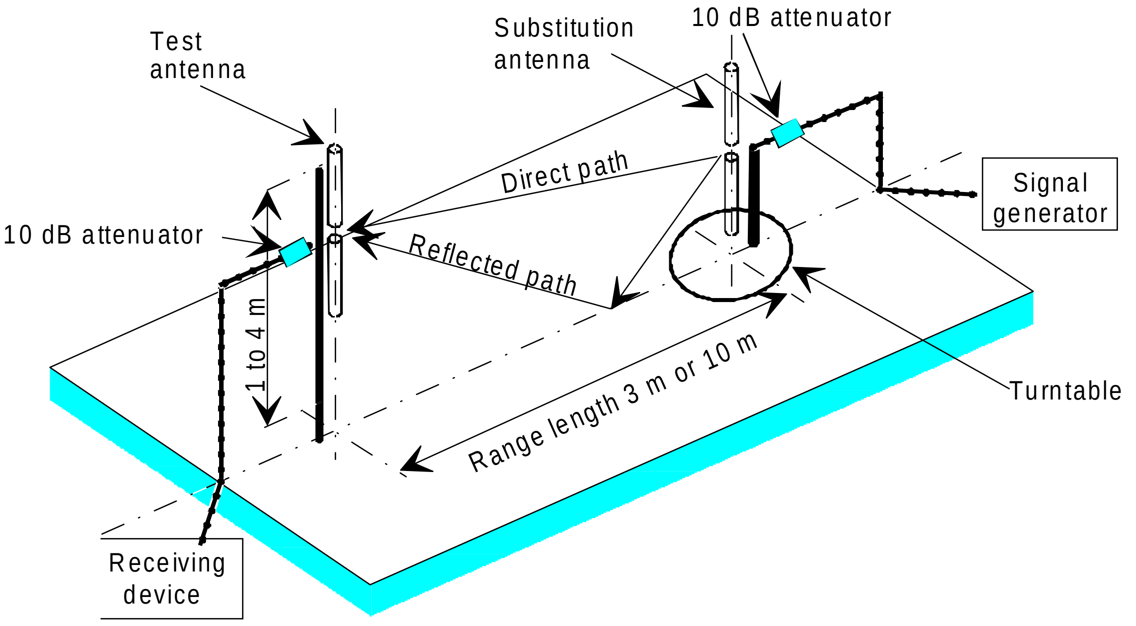

Figure 38: Open area test site set-up for the Effective radiated power substitution measurement

16) The EUT should be remounted on the turntable as stipulated in Steps 2, 3 and 4, the test antenna oriented for horizontal polarization and Steps 5 to 15 repeated with the substitution antenna also oriented for horizontal polarization.

7.2.3.3 Procedure for completion of the results sheets

There are two values that need to be derived before the overall results sheet (table 26) can be completed. These are the overall measurement correction and the expanded uncertainty values.

Guidance for deriving the values of the correction factors is given in table 24.

When the correction factors have been derived, they should be entered on page 2 of the log book results sheet (table 25) as a result of which the overall correction can be calculated as follows:

overall correction = *substitution antenna cable loss*
+ *substitution antenna attenuator loss*
+ *substitution antenna balun loss*
+ *mutual coupling and mismatch loss (where applicable)*
+ *correction for measurement distance*
+ *correction for off-boresight elevation angles*
- *gain of substitution antenna*

NOTE: For frequencies greater than 180 MHz the mutual coupling mismatch loss factor should be taken as 0,00 dB.

The resulting value for the overall correction factor should then be entered on page 2 of the log book result sheet (table 26). The effective radiated power can then be calculated:

effective radiated power = *signal generator output level*
- *reduction in the input attenuation of receiving device (if any)*
+ *overall correction*

The only calculation that remains to be performed before the overall results sheet (table 26) can be completed is the determination of the expanded measurement uncertainty. This should be carried out as given in subclause 7.2.4 and the resulting value entered in the overall results sheet (table 26).

Table 24: Guidance for deriving correction factors

Figures for correction factors:	
Substitution antenna cable loss	Obtained directly from the calibration data
Substitution antenna attenuator loss	Obtained from calibration data
Substitution antenna balun loss	If not known from calibration data, the value should be taken as 0,30 dB
Mutual coupling and mismatch loss factors between the test antenna and substitution antenna	For ANSI dipoles (30 to 180 MHz) values can be obtained from ETR 273-1-2 [10] table A.20. For frequencies greater than 180 MHz, this value is 0,00 dB. For non-ANSI dipoles this value is 0,00 dB.
Measurement distance	For different heights of the test antenna. The correction is the difference between the values for the 2 heights (if different) in the 2 stages of the test. A value for each height should be taken from ETR 273-1-2 [10] figure A.7. Value 1 (height for the measurement on the EUT).......................dB Value 2 (height for the substitution measurement).....................dB Correction value is: (value 2 - value 1) dB
Off boresight angle in elevation plane (for vertically polarized case only)	For different heights of the test antenna. The correction is the difference between the values for the 2 heights (if different) in the 2 stages of the test. A value for each height should be taken from ETR 273-1-2 [10] figure A.8. Value 1 (height for the measurement on the EUT).......................dB Value 2 (height for the substitution measurement).....................dB Correction value is: (value 2 - value 1) dB note: For horizontally polarized tests this is 0,00 dB
Gain of substitution antenna	For ANSI dipoles (30 to 1 000 MHz) the value is 2,10 dBi. For other types, the value can be obtained from calibration data
NOTE: For horizontally polarized tests this is 0,00 dB	

7.2.3.4 Log book entries

Table 25: Log book results sheet

EFFECTIVE RADIATED POWER		Date:			PAGE 1 of 2
Temperature:.........°C	**Humidity:...............%**		**Frequency:.............MHz**		
Manufacturer of EUT:.....................	**Type No:.............**		**Serial No:..................**		
Bandwidth of Receiving Device...................Hz					
Range length :.......................					
Test equipment item	**Type No.**	**Serial No.**	**VSWR**	**Insertion loss**	**Antenna factor/gain**
Test antenna				N/A	
Test antenna attenuator					N/A
Test antenna cable					N/A
Substitution antenna				N/A	
Substitution antenna attenuator					N/A
Substitution antenna cable					N/A
Digital voltmeter			N/A	N/A	N/A
Power supply			N/A	N/A	N/A
Receiving device				N/A	N/A
Signal generator				N/A	N/A
Ferrite beads			N/A	N/A	N/A
Mounting configuration of EUT					

(continued)

Table 25 (concluded): Log book results sheet

EFFECTIVE RADIATED POWER		Date:	PAGE 2 of 2
Vertical polarization		**Horizontal polarization**	
Height of the phase centre, antenna attachment point or volume centre of the EUT		Height of the phase centre, antenna attachment point or volume centre of the EUT	
Height of test antenna (EUT measurement)		Height of test antenna (EUT measurement)	
Maximum signal level on receiving device	dBm	Maximum signal level on receiving device	dBm
Angle at which the maximum signal is received		Angle at which the maximum signal is received	
Height of test antenna (substitution measurement)		Height of test antenna (substitution measurement)	
Output level from signal generator into substitution antenna	dBm	Output level from signal generator into substitution antenna	dBm
Change in receiver attenuator	dB	Change in receiver attenuator	dB
Correction factors			
Substitution antenna cable loss		Substitution antenna cable loss	
Substitution antenna attenuator loss		Substitution antenna attenuator loss	
Substitution antenna balun loss		Substitution antenna balun loss	
Mutual coupling and mismatch loss (30 - 180 MHz)		Mutual coupling and mismatch loss (30 - 180 MHz)	
Measurement distance		Measurement distance	
Off boresight in elevation plane		Off boresight in elevation plane	
Gain of the substitution antenna		Gain of the substitution antenna	
Overall measurement correction	dB	Overall measurement correction	dB

7.2.3.5 Statement of results

The results should be presented in tabular form as shown in table 26.

Table 26: Overall results sheet

EFFECTIVE RADIATED POWER		Date:	PAGE 1 of 1
Vertical polarization		**Horizontal polarization**	
Effective radiated power	dBm	Effective radiated power	dBm
Expanded uncertainty (95 %)	dB	Expanded uncertainty (95 %)	dB

7.2.4 Measurement uncertainty for Effective radiated power

A fully worked example illustrating the methodology to be used can be found in clause 4 of ETR 273-1-2 [10].

7.2.4.1 Uncertainty contributions: Stage 1: EUT measurement

For the measurement of effective radiated power two stages of test are involved. The first stage (the EUT measurement) is to measure on the receiving device, a level from the EUT as shown in figure 39 (shaded components are common to both stages of the test).

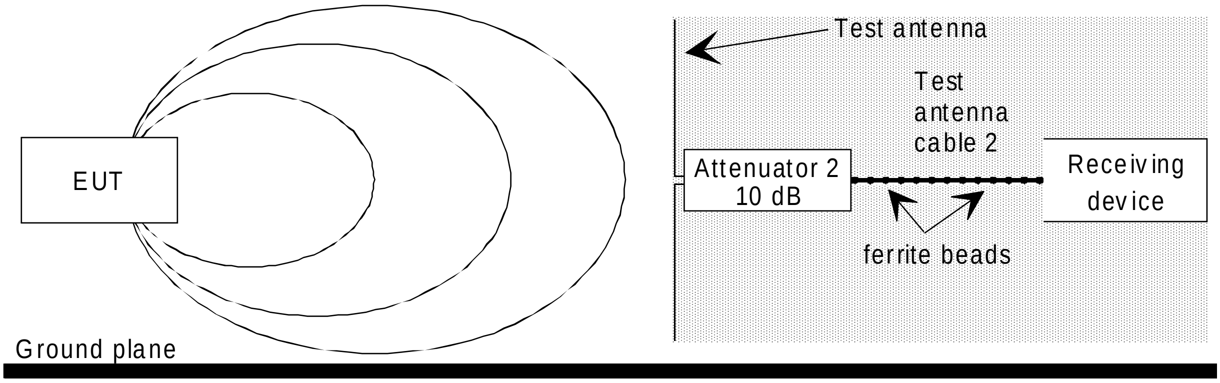

Figure 39: Stage 1:EUT measurement

Due to the commonality of all of the components from the test antenna to the receiver in both stages of the test, the mismatch uncertainty contributes identically in each stage and hence cancels. Similarly, the systematic uncertainty contributions (e.g. test antenna cable loss, etc.)of the individual components also cancel.

The magnitude of the random uncertainty contribution to each stage of the procedure can be assessed from multiple repetition of the EUT measurement. All the uncertainty components which contribute to this stage of the test are listed in table 27. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 27: Contributions from the EUT measurement

uj or i	Description of uncertainty contributions	dB
u_{j37}	*mismatch: receiving part*	
u_{j19}	*cable factor: test antenna cable*	0,00
u_{j41}	*insertion loss: test antenna cable*	0,00
u_{j40}	*insertion loss: test antenna attenuator*	0,00
u_{j47}	*receiving device: absolute level*	0,00
u_{j53}	*EUT: influence of setting the power supply on the ERP of the carrier*	
u_{j20}	*position of the phase centre: within the EUT volume*	
u_{j21}	*positioning of the phase centre: within the EUT over the axis of rotation of the turntable*	
u_{j50}	*EUT: influence of the ambient temperature on the ERP of the carrier*	
u_{j16}	*range length*	
u_{j45}	*antenna: gain of the test antenna*	0,00
u_{j46}	*antenna: tuning of the test antenna*	0,00
u_{j17}	*correction: off boresight angle in the elevation plane*	0,00
u_{j55}	*EUT: mutual coupling to the power leads*	
u_{j08}	*mutual coupling: amplitude effect of the test antenna on the EUT*	
u_{j13}	*mutual coupling: EUT to its image in the ground plane*	
u_{j14}	*mutual coupling: test antenna to its image in the ground plane*	
u_{i01}	*random uncertainty*	

The standard uncertainties from table 27 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ contribution\ from\ the\ EUT\ measurement}$) for the EUT measurement in dB.

7.2.4.2 Uncertainty contributions: Stage 2: Substitution measurement

The second stage (the substitution) involves replacing the EUT with a substitution antenna and signal source as shown in figure 40 and adjusting the output level of the signal generator until the same level as in stage one is achieved on the receiving device.

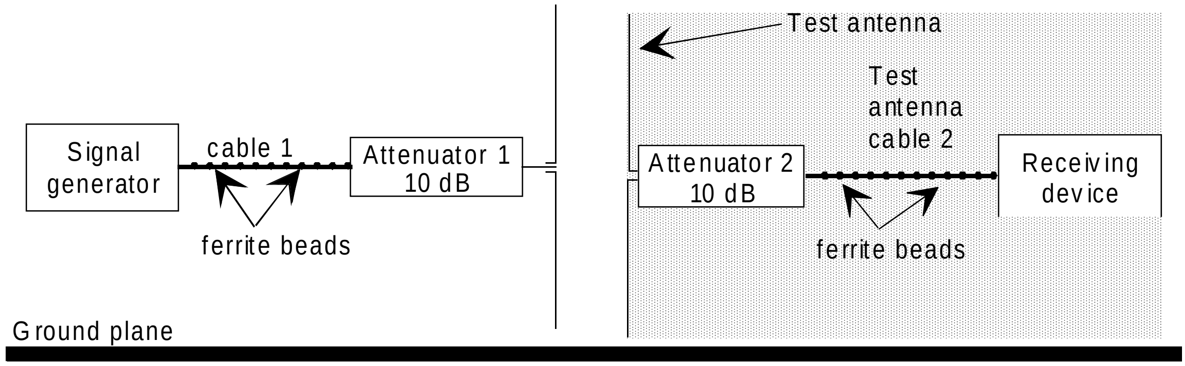

Figure 40: Stage 2: Substitution measurement

All the uncertainty components which contribute to this stage of the test are listed in table 28. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 28: Contributions from the substitution

uj or i	Description of uncertainty contributions	dB
u_{j36}	*mismatch: transmitting part*	
u_{j37}	*mismatch: receiving part*	
u_{j38}	*signal generator: absolute output level*	
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: substitution antenna cable*	
u_{j19}	*cable factor: test antenna cable*	
u_{j41}	*insertion loss: substitution antenna cable*	
u_{j41}	*insertion loss: test antenna cable*	0,00
u_{j40}	*insertion loss: substitution antenna attenuator*	
u_{j40}	*insertion loss: test antenna attenuator*	0,00
u_{j47}	*receiving device: absolute level*	0,00
u_{j16}	*range length*	0,00
u_{j18}	*correction: measurement distance*	
u_{j45}	*antenna: gain of the substitution antenna*	
u_{j45}	*antenna: gain of the test antenna*	0,00
u_{j46}	*antenna: tuning of the substitution antenna*	
u_{j46}	*antenna: tuning of the test antenna*	0,00
u_{j22}	*position of the phase centre: substitution antenna*	
u_{j17}	*correction: off boresight angle in the elevation plane*	
u_{j14}	*mutual coupling: substitution antenna to its image in the ground plane*	
u_{j14}	*mutual coupling: test antenna to its image in the ground plane*	
u_{j11}	*mutual coupling: substitution antenna to the test antenna*	
u_{j12}	*mutual coupling: interpolation of mutual coupling and mismatch loss correction factors*	
u_{i01}	*random uncertainty*	

The standard uncertainties from table 28 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ contributions\ from\ the\ substitution}$) for the substitution measurement in dB.

7.2.4.3 Expanded uncertainty of the ERP measurement

The combined standard uncertainty of the effective radiated power measurement is the RSS combination of the components outlined in 7.2.4.1 and 7.2.4.2. The components to be combined are $u_{c\ contribution\ from\ the\ EUT\ measurement}$ and $u_{c\ contribution\ from\ the\ substitution}$.

$$u_c = \sqrt{u^2_{c\ contribution\ from\ the\ EUT\ measurement} + u^2_{c\ contribution\ from\ the\ substitution}} = \_\_,\_\_\ \mathrm{dB}$$

The expanded uncertainty is ± 1,96 x u_c = ± __,__ dB at a 95 % confidence level.

7.2.5 Spurious Emissions (30 MHz - 4 GHz or 12,75 GHz)

Spurious emissions are unwanted sources of radiation from an EUT. They are at frequencies other than those of the carrier and sidebands associated with normal modulation and by definition, their radiating mechanisms and locations within the equipment, as well as their directivities, polarizations and directions are unknown.

An EUT which is large in terms of wavelength, may possess highly directional (i.e. narrow beam) spurious, particularly at high frequencies, which could radiate at angles that are difficult to detect. Mainly for this reason, a "characterization" procedure, i.e. the identification of all frequencies at which an EUT radiates, should be performed in a shielded enclosure (i.e. an enclosure with metal walls but no absorbing material) prior to testing on the open area test site. An additional benefit of the characterization procedure is that it ensures that no ambient is mistaken for a spurious emission on a noisy test site. Characterization should cover the full 30 MHz to 4 or 12,75 GHz band (as stated in the relevant standard).

Spurious emission testing is performed on all radio equipment possessing an integral antenna. For EUTs fitted with an external antenna connector, spurious emission testing is carried out with a broadband 50 Ω load (sometimes known as an artificial antenna) connected instead of the antenna. The test is then referred to as cabinet radiation testing.

NOTE: For integral antenna devices, the measurement of a spurious emission (for transmitters) is unavoidably performed in the presence of the carrier at full power level. Care should always be exercised under this condition to prevent overloading the input of the receiving device. For these receiving devices, for both characterization and spurious emission testing, a high "Q" notch filter (centred on the carrier frequency) should be used for frequencies up to approximately 1,5 times the carrier frequency and a high pass filter for frequencies above this (the cut-off being approximately 1,5 times the carrier frequency). This should be connected between the test antenna and the input to the receiving device as appropriate.

Definition

Spurious emissions are emissions at frequencies other than those of the carrier and sidebands associated with normal modulation.

The level of a spurious emission should be measured as either:

the effective radiated power of the cabinet and integral antenna together, in the case of EUTs not fitted with an external antenna connector;

or

the effective radiated power of the cabinet and structure of the equipment combined (this is termed cabinet radiation) in the case of EUTs fitted with an external antenna connector.

7.2.5.1 Apparatus required

- digital voltmeter;
- ferrite beads;
- 10 dB Attenuators;
- power supply;
- connecting cables;
- open area test site;
- shielded chamber (non-anechoic);
- broadband test antenna (biconic, typically 30 MHz to 200 MHz, LPDAs, typically 200 MHz to 1 GHz and 1 GHz to 12,75 GHz or waveguide horns, typically 1 GHz to 12,75 GHz);
- substitution antenna (half wavelength dipole as detailed in ANSI C63.5 [1] recommended 30 to 1 000 MHz and waveguide horns 1 to 12,75 GHz);

- receiving device (measuring receiver or spectrum analyser);
- signal generator;
- high "Q" notch filter and high pass filter - only for tests on EUTs not fitted with a permanent antenna connector;
- 50 Ω load - only for tests on EUTs fitted with a permanent antenna connector. This load should perform well throughout the entire frequency band (typically VSWR 1,25:1 up to 1 000 MHz, better than 2,0:1 over 1 GHz to 4 GHz or 12,75 GHz). It should be able to absorb the maximum carrier power at the nominal frequency of the EUT.

The types and serial numbers of all items of test equipment should be recorded on page 1 of the log book results sheet (table 30).

NOTE: The half wavelength dipole antennas, incorporating matching/transforming baluns, for the procedure are available in the following bands: 20 MHz to 65 MHz, 65 MHz to 180 MHz, 180 MHz to 400 MHz, 400 MHz to 1 000 MHz. Constructional details are contained in ANSI C63.5 [1]. In the recommended antenna scheme for this band, a shortened dipole is used at all frequencies from 30 MHz to 80 MHz.

7.2.5.2 Method of measurement

Characterization

The process of characterization should take place within a shielded, totally reflecting enclosure where no absorbing material is present.

C1) The EUT should be mounted on a non-conducting turntable of low relative dielectric constant (preferably less than 1,5) material(s) in a shielded enclosure. (i.e. no absorber).

C2) The test equipment should be arranged as shown in figure 41. The protecting filter should only be used for EUT which are not fitted with an external antenna connector. For those which do have such a connector, the broadband 50 Ω load should be connected to the EUT and the filter becomes unnecessary.

C3) The EUT should be mounted in the position closest to normal use as declared by the manufacturer. This mounting configuration should be recorded on page 1 of the log book results sheet (table 30).

C4) The broadband test antenna should be aligned for vertical polarization and spaced a convenient distance away from the EUT.

NOTE 1: For the purposes of this characterization procedure, the range length does not have to meet the conditions for far-field testing given earlier.

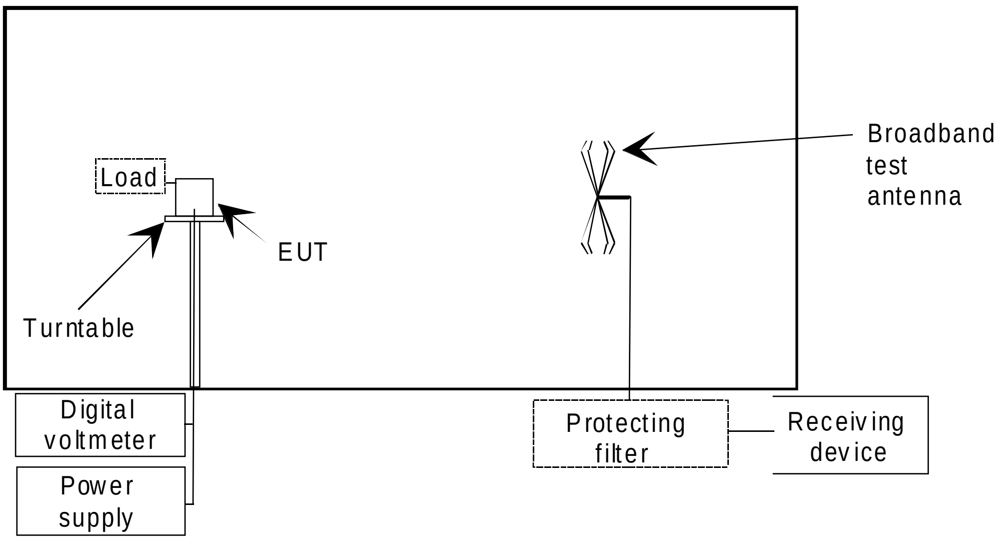

Figure 41: Elevation view of shielded chamber set up for the characterization tests

C5) The EUT should be switched on, without modulation, and the receiving device scanned through the appropriate frequency band, avoiding the carrier frequency and its adjacent channels. All frequencies producing a response on the receiving device should be recorded on page 2 of the log book results sheet (table 30).

NOTE 2: The test antenna should be changed as necessary to ensure that the complete frequency range is covered.

C6) The broadband test antenna should be aligned for horizontal polarization and Step C5 repeated.

NOTE 3: The only information provided by the characterization procedure is which frequencies should be measured on the open area test site.

Measurement

NOTE 4: The following procedure steps involve, for every frequency identified in the characterization procedure, scanning for the peak of the spurious emission in both horizontal and vertical planes around the EUT. The amplitude peak in both planes is measured in both horizontal and vertical polarizations. Large EUTs, however, may possess highly directional spurious emissions particularly at high frequencies and, despite the two plane scanning, there remains for these cases, a small possibility that no spurious can be detected.

1) The measurement should always be performed in the absence of modulation.

2) The EUT should be mounted directly onto the turntable whose mounting surface is at the height (above the ground plane) specified in the relevant Standard. The items of test equipment should be set-up as shown in figure 42.

NOTE 5: The turntable should be constructed from non-conducting, low relative dielectric constant (preferably less than 1,5) material(s).

3) The EUT should be mounted in an orientation which matches that of its normal usage as declared by the manufacturer. The normal to the reference face of the EUT should point directly down the test site towards the antenna mast. This is the 0° reference angle for this test. This orientation and mounting configuration should be recorded on page 1 of the log book results sheet (table 30).

4) The volume centre of the EUT should be positioned on the turntable such that it lies on the axis of rotation of the turntable.

5) The height above the ground plane of the volume centre of the EUT should be recorded on page 2 of the log book results sheet (table 30).

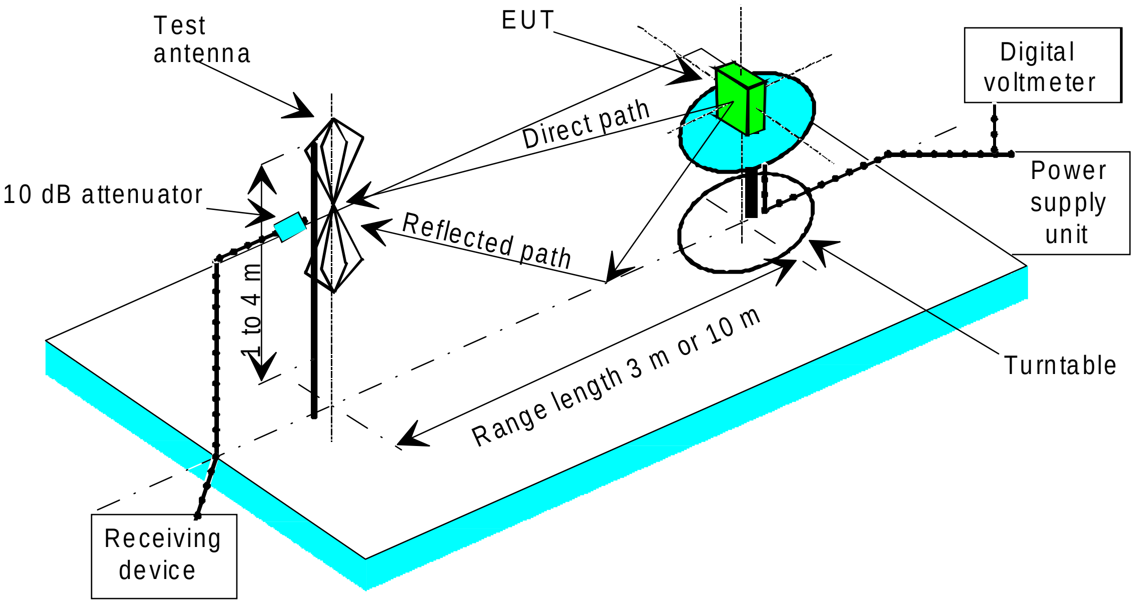

Figure 42: Open area test site set-up for spurious emission testing on the EUT

6) For EUTs fitted with a permanent antenna connector, the broadband 50 Ω load should be connected in place of the antenna.

7) The test antenna (a biconic, LPDA or waveguide horn) should be mounted on the antenna mast and oriented for vertical polarization. Its output should be connected to the receiving device via a 10 dB attenuator and the calibrated, ferrited coaxial cable associated with that end of the test site, and a protective filter (only if the EUT does not possess an external antenna connector).

8) The EUT should be switched on, without modulation, and the receiving device tuned to the first frequency recorded on page 2 of the log book results sheet (table 30).

9) The test antenna should be raised and lowered through the specified range of heights (1 - 4 m, ensuring that no part of the antenna is less than 0,25 m from the ground plane at any time) until the maximum signal level is detected on the receiving device.

NOTE 6: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level should be at the top of the height range.

10) The EUT should be rotated through 360° in the azimuth plane until the maximum signal level is observed on the receiving device. The corresponding received level (dBm_1), height of the test antenna on the mast ($height_1$) and angle of the turntable ($angle_1$) should be recorded on page 2 of the log book results sheet (table 30). Retaining the same height of the test antenna on the mast and angle of turntable, the power to the EUT should be turned off and the value of the level of the noise floor (amb_1) for the receiving device recorded on page 2 of the log book results sheet (table 30).

11) The polarization of the test antenna should be changed to horizontal, the antenna height on the mast readjusted for maximum signal and the resulting received signal level (dBm_2) and the new height of the antenna on the mast ($height_2$) recorded on page 2 of the log book results sheet (table 30). Again, by turning off the power to the EUT, a value for the level of the noise floor (amb_2) for the receiving device should be recorded on page 2 of the log book results (table 30).

12) Retaining the test antenna polarization (horizontal), the EUT should be rotated about its volume centre to lie on its side as shown in figure 43. The height of the test antenna on the mast should be adjusted for maximum received signal level. Using the turntable, the EUT should then be rotated through 360° in the azimuth plane to locate the angle of at which the maximum received signal level is again found. This maximum received level (dBm_3), the height of the test antenna on the mast ($height_3$) and the angle of the turntable ($angle_2$) should be recorded on page 2 of the log book results sheet (table 30). Retaining the same height of the test antenna on the mast and angle of turntable, the power to the EUT should be turned off and the value of the level of the noise floor (amb_3) for the receiving device recorded on page 2 of the log book results sheet (table 30).

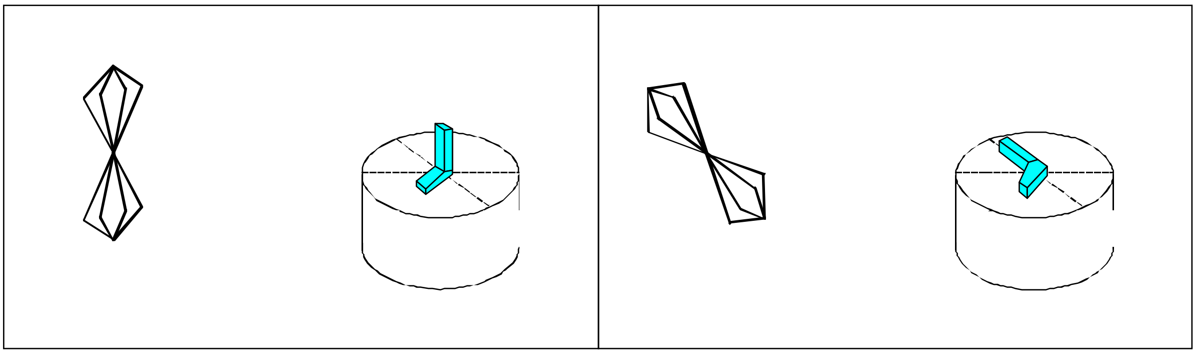

Figure 43: Turning the EUT

13) The polarization of the test antenna should be changed to vertical, the antenna height on the mast readjusted for maximum signal and the resulting received signal level (dBm_4) and the new height of the antenna on the mast ($height_4$) recorded on page 2 of the log book results sheet (table 30). Again, by turning off the power to the EUT, a value for the level of the noise floor (amb_4) for the receiving device should be recorded on page 2 of the log book results (table 30).

14) The EUT should be replaced on the turntable by the substitution antenna (a tuned half wavelength dipole which has been adjusted to correspond to the appropriate frequency or waveguide horn). See figure 44.

NOTE 7: For all frequencies below 80 MHz, a shortened dipole (as defined in subclause 7.1.3) should be used. The dipole arm length is defined from the centre of the balun block to the tip of the arm. From a fully extended state, each telescopic element, in turn, should be "pushed in" from the tip until the required length is obtained. The outermost section needs to fully compress before any of the others, and so on. Table 20 gives the dipole arm lengths and choice of balun for set frequencies. Where the test frequency does not correspond to a set frequency in the table, the arm length to be used should be determined by linear interpolation between the closest set values.

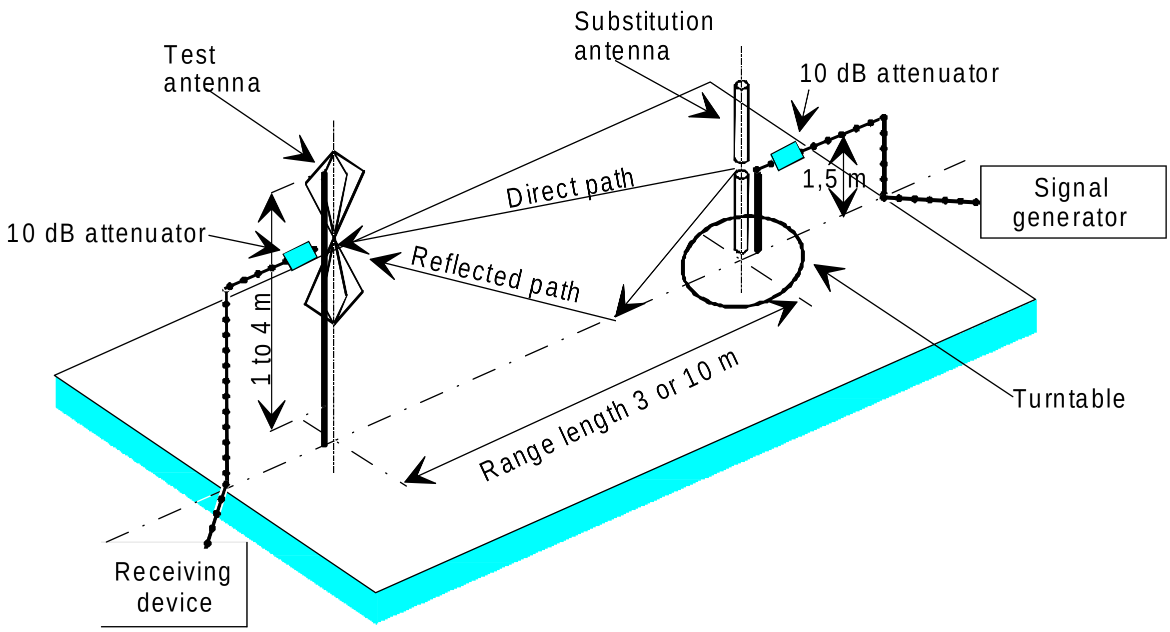

Figure 44: Substitution antenna replacing the EUT for spurious emissions testing on an open area test site

15) The phase centre of the substitution antenna should be located at the same height above the floor as noted in Step 5 and should lie directly on the axis of rotation of the turntable.

NOTE 8: The phase centre of a dipole is in the centre of its two rods. That for a waveguide horn is in the centre of its open mouth.

16) The substitution antenna should be oriented for vertical polarization and connected to a calibrated signal generator via a 10 dB attenuator and the calibrated, ferrited, coaxial cable associated with that end of the test site.

17) The signal generator should be tuned to the appropriate frequency and its output level adjusted until the level measured on the receiving device, is at least 20 dB above the level with the output from the signal generator switched off.

18) The test antenna should be raised and lowered through the specified range of heights until the maximum signal level is recorded on the receiving device. The height of the test antenna on the mast ($height_5$) should be recorded on page 2 of the log book results sheet (table 30).

NOTE 9: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level should be at the top of the height range.

19) The substitution antenna should be rotated until the maximum level is detected on the receiving device.

NOTE 10: This is to correct for possible misalignment of a directional beam (i.e. as produced by waveguide horns in all tests and by dipoles when used in horizontally polarised tests only). This step can be omitted for dipoles used in vertically polarized tests.

20) The output level of the signal generator should be adjusted until the level, measured on the receiving device, is the same as the larger of dBm_1 and dBm_4. This output signal level (dBm_5) should be recorded on page 2 of the log book results sheet (table 30).

NOTE 11: In the event of insufficient range of signal generator output level, the input attenuation to the receiving device should be decreased to compensate. The signal generator output level (dBm_5) and the change in attenuation (dB_1, where a decrease is taken as + dB, an increase is taken as - dB) should be recorded on page 2 of the log book results sheet (table 30).

21) The test antenna and the substitution antenna should both be oriented for horizontal polarization and Steps 17 to 20 repeated. This time, $height_6$ is recorded in Step 18 and dBm_6 and dB_2 recorded in Step 20 after adjustment of the signal generator output level until the receiving device level is the larger of dBm_2 and dBm_3.

22) Steps 1 to 21 should be repeated for all the other frequencies recorded in the log book results sheet (table 30) changing the antennas as necessary.

7.2.5.3 Procedure for completion of the results sheets

There are several values that remain to be entered in the overall results sheet (table 31). These are the overall spurious emission levels (corrected for the systematic offsets involved in the measurement) and the expanded measurement uncertainty.

Initially, the overall correction factors for each of the two polarizations should be calculated. Then, all received signal levels (i.e. dBm_1 to dBm_4) should be corrected to convert them into effective radiated power figures, the corrections not only accounting for the systematic offsets (cable losses, attenuator loss, etc.) but also for the different measurement distances and off boresight elevation angles involved. All corrections should be made relating the measurement to the corresponding substitution measurement for that polarization.

Table 29 lists all the correction factors involved in this procedure along with giving guidance on how their values can be obtained. It should be noted that some values differ depending on the polarization considered.

Table 29: Guidance for deriving correction factors

Figures for correction factors	
Substitution antenna cable loss	Obtained directly from the calibration data
Substitution antenna attenuator loss	Obtained from calibration data
Substitution antenna balun loss	For dipoles only, if not known from calibration this value should be taken as 0,3 dB. For waveguide horns the value is 0,00 dB
Mutual coupling mismatch loss correction factors between the test antenna and the substitution antenna	For ANSI dipoles (30 MHz to 180 MHz) can be obtained from ETR 273-1-2 [10] table A.20. For frequencies greater than 180 MHz, this value is 0,00 dB. For non-ANSI dipoles this value is 0,00 dB
Measurement distance	(only for different heights of the test antenna). The correction is the difference between the values for the 2 heights in the 2 stages of the test. A value for each height should be taken from ETR 273-1-2 [10] figure A.7. Value 1 (height for the measurement on the EUT).......................dB Value 2 (height for the substitution measurement).....................dB Correction value is: (value 2 - value 1) dB
Off boresight angle in elevation plane (for vertically polarized case only)	(only for different heights of the test antenna). The correction is the difference between the values for the 2 heights in the 2 stages of the test. A value for each height should be taken from ETR 273-1-2 [10] figure A.8. Value 1 (height for the measurement on the EUT).......................dB Value 2 (height for the substitution measurement).....................dB Correction value is: (value 2 - value 1) dB
Gain of substitution antenna	2,10 dBi for ANSI dipoles (30 to 1 000 MHz) for other types the value can be obtained from calibration data
NOTE: For horizontally polarized tests this is 0,00 dB	

Once derived, all the various corrections should be incorporated into the following formula for overall correction for both polarizations:

overall correction = *substitution antenna cable loss*
+ *substitution antenna attenuator loss*
+ *substitution antenna balun loss*
+ *mutual coupling and mismatch loss (where applicable)*
+ *correction for measurement range*
+ *correction for off-boresight elevation angles*
- *gain of substitution antenna*
- *decrease in input attenuation to receiving device (if any)*

NOTE: For frequencies greater than 180 MHz the mutual coupling and mismatch loss factor should be taken as 0,00 dB.

Both values of overall correction factor should be entered on page 2 of the log book results sheet (table 30).

All four received signal levels (dBm_1 to dBm_4) should then be corrected by the relevant overall correction factor (i.e. dBm_1 and dBm_4 with the vertically polarized correction factor, dBm_2 and dBm_3 with the horizontally polarized one) to reveal effective radiated power levels (erp_1, erp_2, erp_3 and erp_4 respectively) in dBm. These four new values should be entered on page 2 of the log book results sheet (table 30).

The final calculation is to combine the two polarization components of each of the two spurious in the following manner.

- If the calculated effective radiated power value erp_1 is more than 20 dB greater than erp_2, then "Spurious level 1", is simply the value of erp_1. Similarly, if erp_2 exceeds erp_1 by more than 20 dB, "Spurious level 1" is simply erp_2. Alternatively, the spurious level should be calculated as:

$$Spurious\,level\,1 = 20\log\left(10^{\left(\frac{erp_1}{20}\right)} + 10^{\left(\frac{erp_2}{20}\right)}\right)\ \text{dBm}$$

- The resulting value should be entered on page 2 of the log book results sheet as "Spurious level 1".

- If the calculated ERP value erp_3 is more than 20 dB greater than erp_4, then "Spurious level 2", is simply the value of erp_3. Similarly, if erp_4 exceeds erp_3 by more than 20 dB, "Spurious level 2" is simply erp_4. Alternatively, the spurious level should be calculated as:

$$Spurious\,level\,2 = 20\log\left(10^{\left(\frac{erp_3}{20}\right)} + 10^{\left(\frac{erp_4}{20}\right)}\right)\ \text{dBm}$$

- The resulting value should be entered on page 2 of the log book results sheet as "Spurious level 2".

- Whichever value is the larger of "Spurious level 1" and "Spurious level 2" should be entered as "Overall spurious level" on page 2 of the log book results sheet (table 30). The resulting value is the ERP of the Spurious emission and should entered as such in the overall results table (table 31).

The final value to be entered in the overall results sheet (table 31) is that for the expanded uncertainty. This should be calculated according to subclause 7.2.6.

7.2.5.4 Log book entries

Table 30: Log book results sheet

SPURIOUS EMISSIONS			**Date:**		**PAGE 1 of 2**
Temperature:.........°C **Manufacturer of EUT:.....................** **Bandwidth of Receiving Device..................Hz**		**Humidity:...............%** **Type No:.............**		**Frequency:.............MHz** **Serial No:..................**	
Range length :.......................					
Test equipment item	**Type No.**	**Serial No.**	**VSWR**	**Insertion loss**	**Antenna factor/gain**
Broadband test antenna (typically 30 to 200 MHz)				N/A	
Broadband test antenna (typically 200 MHz to 1 GHz)				N/A	
Broadband test antenna (typically 1 to 12,75 GHz)				N/A	
Test antenna attenuator					N/A
Test antenna cable					N/A
Substitution antenna (typically ANSI C63.5 [1] 30 to 1 000 MHz)				N/A	
Substitution antenna (typically waveguide horns 1 to 12,75 GHz)				N/A	
Substitution antenna attenuator					N/A
Substitution antenna cable					N/A
Digital voltmeter			N/A	N/A	N/A
Power supply			N/A	N/A	N/A
Receiving device				N/A	N/A
Signal generator				N/A	N/A
Ferrite beads			N/A	N/A	N/A
High "Q" notch filter					N/A
High pass filter					N/A
Mounting configuration of EUT (Characterization)					
Mounting configuration of EUT (Measurement)					

(continued)

Table 30 (concluded): Log book results sheet

SPURIOUS EMISSIONS				**Date:**			**PAGE 2 of 2**
Height above the ground plane of the volume centre of the EUT ....m							
Frequency (MHz)							
dBm_1							
$Height_1$							
$Angle_1$							
amb_1							
dBm_2							
$Height_2$							
amb_2							
dBm_3							
$Height_3$							
$Angle_2$							
amb_3							
dBm_4							
$Height_4$							
amb_4							
Signal generator output level (dBm_5)							
Change in attenuator level (dB_1)							
Signal generator output level (dBm_6)							
Change in attenuator level (dB_2)							
Overall correction factor - Vertical polarization							
Overall correction factor - Horizontal polarization							
erp_1							
erp_2							
erp_3							
erp_4							
Spurious level 1							
Spurious level 2							
Overall Spurious level dBm							

Correction factors														
	polarization													
Frequency (MHz)														
	V	H	V	H	V	H	V	H	V	H	V	H	V	H
Substitution antenna cable loss														
Substitution antenna attenuator loss														
Substitution antenna balun loss														
Mutual coupling and mismatch loss (30 - 180 MHz)														
Measurement distance														
Off-elevation boresight level														
Gain of the substitution antenna														
Overall measurement correction	dB		dB		dB		dB		dB		dB		dB	

7.2.5.5 Statement of results

The results should be presented in tabular form as shown in table 31.

Table 31:Overall results sheet

SPURIOUS EMISSIONS				Date:			PAGE 1 of 1
Frequency (MHz)							
Spurious emission ERP (dBm)							
Expanded uncertainty (95 %)	dB	dB	dB	dB	dB	dB	dB

7.2.6 Measurement uncertainty for Spurious emissions

A fully worked example illustrating the methodology to be used can be found in clause 4 of ETR 273-1-2 [10].

7.2.6.1 Uncertainty contributions: Stage 1: EUT measurement

For the measurement of spurious effective radiated power two stages of test are involved. The first stage (the EUT measurement) is to measure on the receiving device, a level from the EUT as shown in figure 45 (shaded components are common to both stages of the test).

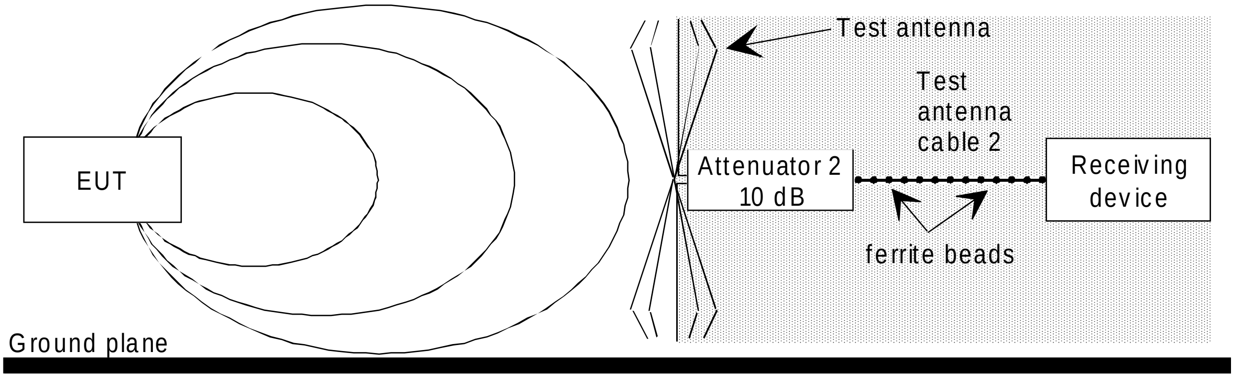

Figure 45: Stage 1: EUT measurement

Due to the commonality of all of the components from the test antenna to the receiver in both stages of the test, the mismatch uncertainty contributes identically in each stage and hence cancels. Similarly, the systematic uncertainty contributions (e.g. test antenna cable loss, etc.) of the individual components also cancel.

The magnitude of the random uncertainty contribution to each stage of the procedure can be assessed from multiple repetition of the EUT measurement.

All the uncertainty components which contribute to this stage of the test are listed in table 32. ETR 273-1-1 [**9**] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 32: Contributions from the measurement on the EUT

uj or i	Description of uncertainty contributions	dB
u_{j37}	*mismatch: receiving part*	
u_{j19}	*cable factor: test antenna cable*	0,00
u_{j41}	*insertion loss: test antenna cable*	0,00
u_{j40}	*insertion loss: test antenna attenuator*	0,00
u_{j47}	*receiving device: absolute level*	0,00
u_{j54}	*EUT: influence of setting the power supply on the spurious emission level*	
u_{j20}	*position of the phase centre: within the EUT volume*	
u_{j21}	*positioning of the phase centre: within the EUT over the axis of rotation of the turntable*	
u_{j51}	*EUT: influence of the ambient temperature on the spurious emission level*	
u_{j16}	*range length*	
u_{j18}	*correction: measurement distance*	
u_{j45}	*antenna: gain of the test antenna*	0,00
u_{j46}	*antenna: tuning of the test antenna*	0,00
u_{j55}	*EUT: mutual coupling to the power leads*	
u_{j08}	*mutual coupling: amplitude effect of the test antenna on the EUT*	
u_{j13}	*mutual coupling: EUT to its images in the ground plane*	
u_{j14}	*mutual coupling: test antenna to its images in the ground plane*	
u_{i01}	*random uncertainty*	

The standard uncertainties from table 32 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ contribution\ from\ the\ EUT\ measurement}$) for the EUT measurement in dB.

7.2.6.2 Uncertainty contributions: Stage 2: Substitution measurement

The second stage (the substitution) involves replacing the EUT with a substitution antenna and signal source as shown in figure 46 and adjusting the output level of the signal generator until the same level as in stage one is achieved on the receiving device.

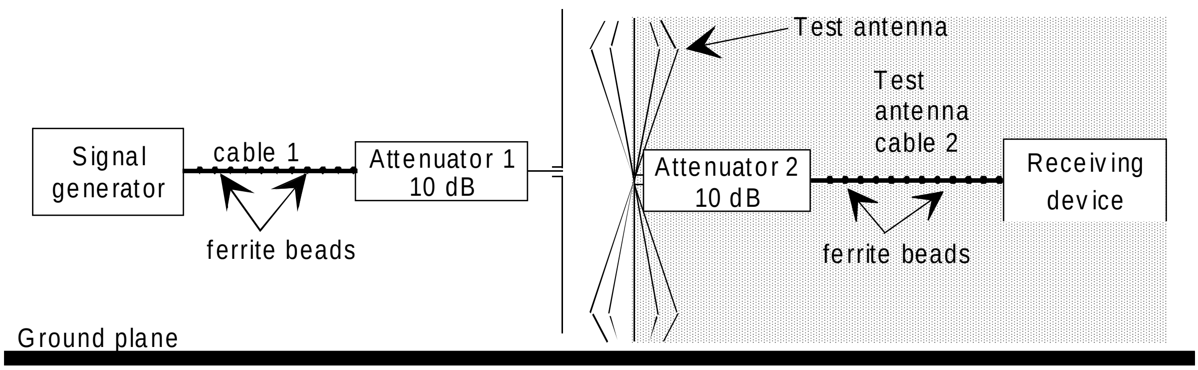

Figure 46: Stage 2: Typical emission substitution test

All the uncertainty components which contribute to this stage of the test are listed in table 33. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contribution.

Table 33: Contributions from the substitution

uj or i	Description of uncertainty contributions	dB
u_{j36}	*mismatch: transmitting part*	
u_{j37}	*mismatch: receiving part*	
u_{j38}	*signal generator: absolute output level*	
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: substitution antenna cable*	
u_{j19}	*cable factor: test antenna cable*	
u_{j41}	*insertion loss: substitution antenna cable*	
u_{j41}	*insertion loss: test antenna cable*	0,00
u_{j40}	*insertion loss: substitution antenna attenuator*	
u_{j40}	*insertion loss: test antenna attenuator*	0,00
u_{j47}	*receiving device: absolute level*	0,00
u_{j16}	*range length*	0,00
u_{j18}	*correction: measurement distance*	
u_{j45}	*antenna: gain of the substitution antenna*	
u_{j45}	*antenna: gain of the test antenna*	0,00
u_{j46}	*antenna: tuning of the substitution antenna*	
u_{j46}	*antenna: tuning of the test antenna*	0,00
u_{j22}	*position of the phase centre: substitution antenna*	
u_{j17}	*correction: off boresight angle in the elevation plane*	
u_{j14}	*mutual coupling: substitution antenna to its image in the ground plane*	
u_{j14}	*mutual coupling: test antenna to its image in the ground plane*	
u_{j11}	*mutual coupling: substitution antenna to the test antenna*	
u_{j12}	*mutual coupling: interpolation of mutual coupling and mismatch loss correction factors*	
u_{i01}	*random uncertainty*	

The standard uncertainties from table 33 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ \text{contribution from the substitution}}$) for the EUT measurement in dB.

7.2.6.3 Expanded uncertainty of the Spurious emission

The combined standard uncertainty of the ERP measurement of the spurious emission is the combination of the components outlined in subclauses 7.2.6.1 and 7.2.6.2. The components to be combined are $u_{c\ \text{contribution from the EUT measurement}}$ and $u_{c\ \text{contribution from the substitution}}$.

$$u_c = \sqrt{u^2_{c\ \text{contribution fron the EUT mesurement}} + u^2_{c\ \text{contribtution from the substitution}}} = \_\_,\_\_\ \text{dB}$$

The expanded uncertainty is ± 1,96 x u_c = ± __,__ dB at a 95 % confidence level.

7.2.7 Adjacent channel power

This test is normally carried out using a test fixture and as a result has not been considered for the anechoic chamber.

7.3 Receiver tests

The tests carried out on receivers can be divided into two categories, namely sensitivity and immunity. However, only sensitivity tests are considered here.

7.3.1 Sensitivity tests (30 MHz to 1 000 MHz)

The test method for measuring the maximum or average usable sensitivity of a receiver is in two parts. In the first part, a Transform Factor for the test site (i.e. the relationship in decibels between the output power level (in dBm) from the signal generator to the resulting electric field strength (in dBµV/m) at the point of test) is determined. In the second part, the sensitivity of the EUT is measured by finding the lowest output level from the signal generator which produces the required response at each of eight angles in the horizontal plane.

The receiver output depends on the type of information the receiver has been designed to demodulate. There are principally three different types of information: analogue speech, bit stream and messages.

Definition

For analogue speech:

- the ***maximum usable sensitivity*** expressed as field strength is the minimum of eight field strength (in dBµV/m) measurements (at 45° increments in the horizontal plane) at the nominal frequency of the receiver and with specified test modulation, which produces a SINAD ratio of 20 dB measured at the receiver input through a telephone psophometric weighting network. The starting horizontal angle is the reference orientation as stated by the manufacturer.

- the ***average usable sensitivity*** expressed as field strength is the average of 8 field strength (in dBµ V/m) measurements (at 45° increments in the horizontal plane) at the nominal frequency of the receiver and with specified test modulation, which produces a SINAD ratio of 20 dB measured at the receiver input through a telephone psophometric weighting network. The starting horizontal angle is the reference orientation as stated by the manufacturer.

For bit stream:

- the ***maximum usable sensitivity*** expressed as field strength is the minimum of 8 field strength (in dBµV/m) measurements (at 45° increments in the horizontal plane) at the nominal frequency of the receiver and with specified test modulation, which produces, after demodulation, a data signal with a bit error ratio of 10^{-2} measured at the receiver input. The starting horizontal angle is the reference orientation as stated by the manufacturer.

- the ***average usable sensitivity*** expressed as field strength is the average of 8 field strength (in dBµ V/m) measurements (at 45° increments in the horizontal plane) at the nominal frequency of the receiver and with specified test modulation, which produces, after demodulation, a data signal with a bit error ratio of 10^{-2} measured at the receiver input. The starting horizontal angle is the reference orientation as stated by the manufacturer.

For messages:

- the ***maximum usable sensitivity*** expressed as field strength is the minimum of 8 field strength (in dBµV/m) measurements (at 45° increments in the horizontal plane) at the nominal frequency of the receiver, and with specified test modulation, which produces, after demodulation, a message acceptance ratio of 80 % measured at the receiver input. The starting horizontal angle is the reference orientation as stated by the manufacturer.

- the ***average usable sensitivity*** expressed as field strength is the average of 8 field strength (in dBμ V/m) measurements (at 45° increments in the horizontal plane) at the nominal frequency of the receiver and with specified test modulation, which produces, after demodulation, a message acceptance ratio of 80 % measured at the receiver input. The starting horizontal angle is the reference orientation as stated by the manufacturer.

7.3.1.1 Apparatus required

- digital voltmeter;
- ferrite beads;
- 10 dB attenuators;
- power supply;
- connecting cables;
- open area test site;
- test antenna (half wavelength dipole as detailed in ANSI C63.5 [1] recommended);
- measuring antenna (half wavelength dipole as detailed in ANSI C63.5 [1] recommended);
- RF Signal generator;
- receiving device (measuring receiver or spectrum analyser).

Additional requirements for analogue speech:

- AF source;
- SINAD Meter (incorporating telephone psophometric weighting network);
- acoustic coupler (alternatively: audio load).

Additional requirements for bit stream:

- bit stream generator;
- bit error measuring test set.

Additional requirements for messages:

- acoustic coupler;
- message generator;
- response measuring test set.

The types and serial numbers of all items of test equipment should be recorded on page 1 of the log book results sheet (table 35).

NOTE: The half wavelength dipole antennas, incorporating matching/transforming baluns, for the procedure are available in the following bands: 20 MHz to 65 MHz, 65 MHz to 180 MHz, 180 MHz to 400 MHz, 400 MHz to 1 000 MHz. Constructional details are contained in ANSI C63.5 [1]. In the recommended antenna scheme for this band, a shortened dipole is used at all frequencies from 30 MHz up to 80 MHz.

7.3.1.2 Method of measurement

Determination of the Transform Factor for the test site

1) For this part of the test, it is necessary to position the measuring antenna such that its phase centre is at the same height above the ground plane as the phase centre of the EUT in the second part of the test. The height of the phase centre of the EUT should be either measured remotely or determined by sitting the EUT on the turntable. The height above the turntable (whose mounting surface should be at the height above the ground plane as specified in the relevant Standard) should be recorded on page 2 of the log book results sheet (table 35).

   NOTE 1: If the position of the phase centre within the EUT is unknown, but the antenna is visible, then the height above the ground plane of the point at which the antenna meets the case of the EUT should be used. If the phase centre is unknown and there is no visible antenna, the volume centre of the EUT should be used instead.

2) The measuring antenna (in the recommended scheme: a tuned ANSI C63.5 [1] half wavelength dipole for frequencies of 80 MHz and above, a shortened dipole for frequencies from 30 MHz to 80 MHz) should be adjusted to correspond to the nominal frequency of the EUT and positioned with its phase centre on the axis of rotation of the turntable and at the height above it as recorded in Step 1. It should be oriented for vertical polarization.

NOTE 2: For all frequencies below 80 MHz, a shortened dipole (as defined in subclause 7.1.3) should be used. The dipole arm length is defined from the centre of the balun block to the tip of the arm. From a fully extended state, each telescopic element, in turn, should be "pushed in" from the tip until the required length is obtained. The outermost section needs to fully compress before any of the others, and so on. Table 20 gives the dipole arm lengths and choice of balun for set frequencies. Where the test frequency does not correspond to a set frequency in the table, the arm length to be used should be determined by linear interpolation between the closest set values.

NOTE 3: The turntable should be constructed from non-conducting, low relative dielectric constant (preferably less than 1,5) material(s).

3) The measuring antenna should be connected via a 10 dB attenuator and the calibrated, ferrited coaxial cable associated with that end of the test site, to the receiving device.

4) The test antenna (identical to the measuring antenna) should be mounted on the antenna mast, tuned to the nominal frequency of the EUT and oriented for vertical polarization.

5) The test antenna should be connected via a 10 dB attenuator and the calibrated, ferrited coaxial cable associated with that end of the test site, to the signal generator whose output is unmodulated. See figure 47. The signal generator should be tuned to the nominal frequency of the EUT.

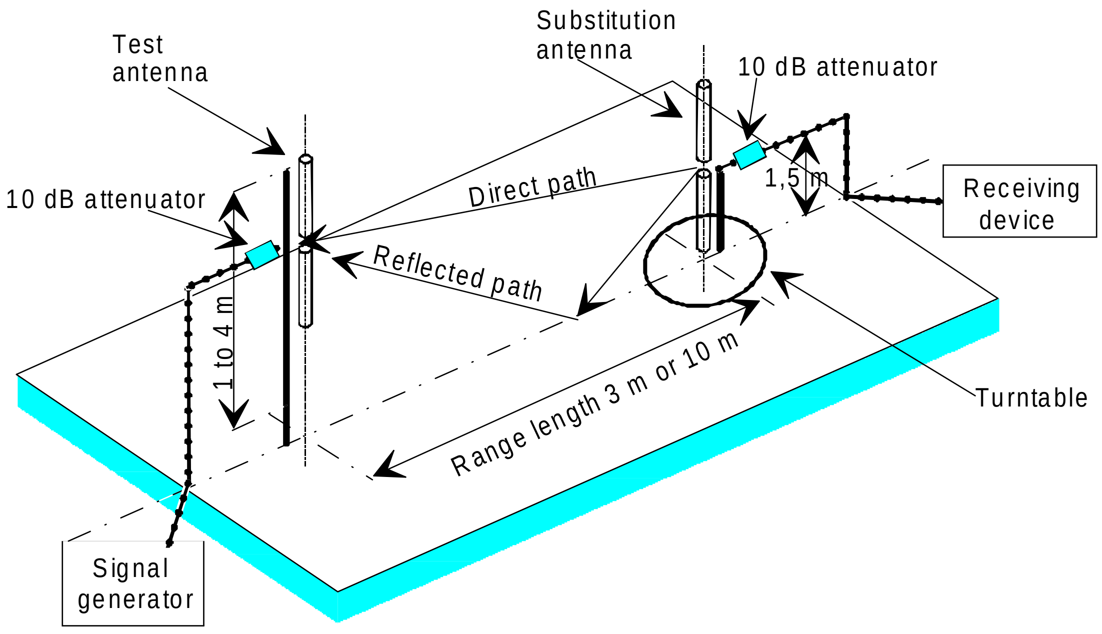

Figure 47: Equipment layout for the derivation of the transform factor during sensitivity tests on an open area test site

6) The output level of the signal generator should be adjusted until a received signal level at least 20 dB above the noise floor is observed on the receiving device.

7) The test antenna should be raised and lowered through the specified range of heights whilst monitoring the received signal level on the receiving device. The test antenna should be positioned at the height corresponding to the maximum received signal. This height should be recorded on page 2 of the log book results sheet (table 35).

NOTE 4: The true maximum may lie beyond the top of the mast, in which case the maximum receivable level should be at the top of the height range.

8) The measuring antenna should be rotated in the horizontal plane until the maximum level is detected on the receiving device.

NOTE 5: This is to correct for possible misalignment of a directional beam i.e. dipoles used in horizontally polarized tests. This step can be omitted when dipoles are used in vertically polarized tests.

9) The maximum received signal level (dBμV) appearing on the receiving device along with the output level from the signal generator (dBm) should be recorded on page 2 of the log book results sheet (table 35). The Transform Factor for the test site (i.e. the factor relating the output power level from the signal generator (dBm) to the resulting field strength (dBμV/m) at the point of measurement) should be calculated according to the following formula:

Transform Factor = *maximum received signal level (dBμV)*
+ *measuring antenna cable loss*
+ *measuring antenna attenuator loss*
+ *measuring antenna balun loss*
+ *mutual coupling and mismatch loss correction factor (if applicable)*
+ *antenna factor of the measuring antenna*
- *signal generator output level (dBm)*

NOTE 6: Guidance for deriving/calculating/finding the values for all of the unknown factors in the above are given in table 34. These values should be entered on page 2 of the log book results sheet (table 35).

The resulting value for the Transform Factor should be entered on page 2 of the log book results sheet (table 35).

Table 34: Guidance for deriving Transform Factor

Values in the formula for Transform Factor	
Measuring antenna cable loss	Obtained directly from the calibration data
Measuring antenna attenuator loss	Obtained directly from the calibration data
Measuring antenna balun loss	If not known from calibration data, the value should be taken as 0,30 dB
Mutual coupling and mismatch loss correction factors between the test antenna and the measuring antenna	For ANSI dipoles (30 to 180 MHz), values can be obtained from ETR 273-1-2 [10] table A20. For frequencies greater than 180 MHz, this value is 0,00 dB. For non-ANSI dipoles this value is 0,00 dB
Antenna factor of the measuring antenna	For ANSI dipoles: Antenna factor = 20 $\log_{10}(f)$ - 31,4 dB/m (where f is the frequency in MHz) For other types the value can be obtained from calibration data

Sensitivity measurement on the EUT

10) The measuring antenna should be replaced on the turntable by the EUT. The EUT should be positioned on the turntable such that its phase centre is in the same place as formerly occupied by the phase centre of the measuring antenna.

NOTE 7: If the position of the phase centre within the EUT is unknown but the antenna is a single rod which is visible and vertical in normal usage, the axis of the antenna should be aligned with the axis of rotation of the turntable. If the phase centre is not known and there is no visible antenna the volume centre of the EUT should be aligned with the axis of rotation of the turntable.

11) The EUT should be mounted in an orientation which matches that of its normal usage as declared by the manufacturer. The normal to its reference face should point directly towards the antenna mast. This is the 0° reference angle for this test. This orientation and mounting configuration should be recorded on page 1 of the log book results sheet (table 35).

For analogue speech

12a) The EUT should be connected to the modulation detector (a SINAD meter incorporating a telephone psophometric weighting network) through an AF load or by an acoustic coupler which is made from low dielectric constant (i.e. less than 1,5) material(s) for EUTs not fitted with a direct connection (see figure 48).

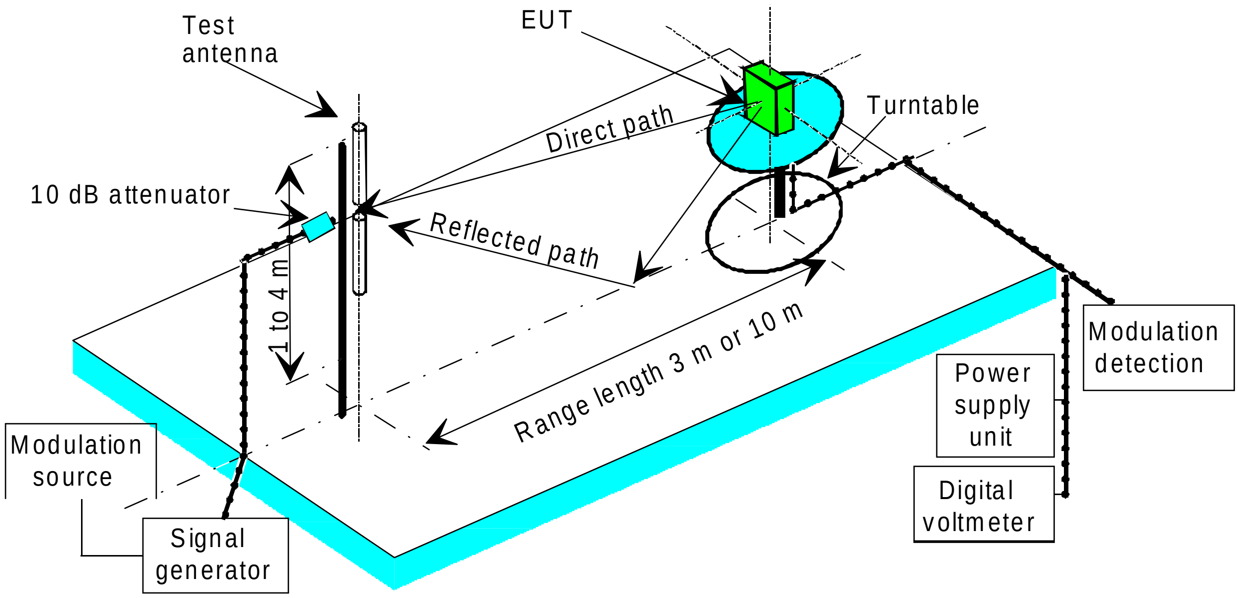

Figure 48: Open area test site set-up for sensitivity tests on the EUT

12b) The signal generator output should be modulated with test modulation AM-1 (produced by the AF source) and its output level should be adjusted until a psophometrically weighted SINAD ratio of 20 dB is obtained from the EUT. The corresponding signal generator output power level should be recorded on page 2 of the log book results sheet (table 35).

12c) The EUT should be successively rotated through 45° in the horizontal plane to new testing angles of 45°, 90°, 135°, 180°, 225°, 270°, 315° (thereby covering the entire 360° in eight measurements). At each angle Step 12b should be repeated.

12d) The eight values of signal generator output power level resulting from Steps 12b and 12c should be converted into field strength values by firstly adding the Transform Factor to produce the field strength in dBµV/m and then secondly converting dBµV/m to µV/m i.e.:

1) field strength (dBµV/m) = signal generator level (dBm) + transform factor (dB);
2) field strength (µV/m) = $10^{(\text{field strength(dB}\mu\text{V/m)/20})}$.

The resulting values in µV/m should be entered on page 2 of the log book results sheet (table 35).

12e) The test procedure should now continue with step 13.

For bit stream:

12a) The EUT should be connected to the modulation detector (a bit error measuring test set, which should also receive a direct input from the bit stream generator) by a direct connection (see figure 48).

12b) The signal generator output should be modulated with test modulation DM-2 (produced by the bit stream generator) and its output level should be adjusted until a bit error ratio of 10^{-2} is obtained from the EUT. The corresponding signal generator output power level should be recorded on page 2 of the log book results sheet (table 35).

12c) The EUT should be successively rotated through 45° in the horizontal plane to new testing angles of 45°, 90°, 135°, 180°, 225°, 270°, 315° (thereby covering the entire 360° in 8 measurements). At each angle Step 12b should be repeated.

12d) The 8 values of signal generator output power level resulting from Steps 12b and 12c should be converted into field strength values by firstly adding the transform factor to produce the field strength in dBμV/m and then secondly converting dBμV/m to μV/m i.e.:

1) field strength (dBμV/m) = signal generator level (dBm) + Transform Factor (dB);
2) field strength (μV/m) = $10^{(\text{field strength(dB}\mu\text{V/m)/20})}$.

The resulting values in μV/m should be also entered on page 2 of the log book results sheet (table 35).

12e) The test procedure should now continue with Step 13.

For messages:

12a) The EUT should be connected to the modulation detector (a response measuring test set) via an acoustic coupler (pipe) which is made from low dielectric constant (i.e. less than 1,5) material(s). See figure 48.

12b) The signal generator output should be modulated with test modulation DM-3 (produced by the message generator) and its output level should be adjusted until a message acceptance ratio of less than 10 % is obtained from the EUT.

12c) The test message should be transmitted repeatedly from the test antenna, whilst observing for each message whether a successful response is obtained. The output level of the signal generator should be increased by 2 dB for each occasion that a successful response is NOT obtained.

12d) Step 12c should be repeated until three consecutive successful responses are observed at the same output level from the signal generator. The output level from the signal generator should be recorded on page 2 of the log book results sheet (table 35).

12e) The output signal level from the signal generator should be reduced by 1 dB. The new signal level should be recorded on page 2 of the log book results sheet (table 35) and the response of the EUT observed.

12f) If a successful response is NOT obtained, the output signal level should be increased by 1 dB and the new level recorded in the results sheet. If a successful response IS obtained, the input level should not be changed until three consecutive successful responses have been observed. In this case, the output signal level from the signal generator should be reduced by 1 dB and the new level recorded in the results sheet. No signal levels should be recorded unless preceded by a change of level.

12g) Step 12f should be repeated until a total of 10 recorded values for the signal generator output level have been entered on page 2 of the log book results sheet (table 35).

12h) The EUT should be successively rotated through 45° in the horizontal plane to new testing angles of 45°, 90°, 135°, 180°, 225°, 270°, 315° (thereby covering the entire 360° in eight measurements). At each angle Steps 12b to 12g should be repeated.

12i) For each angle, the 10 recorded values of the signal generator output level (dBm) should be converted to field strength (μV/m) by firstly adding the transform factor to produce the field strength in dBμV/m and then secondly converting dBμV/m to μV/m i.e.:

1) field strength (dBµV/m) = signal generator level (dBm) + Transform Factor (dB);
2) field strength (µV/m) = $10^{(\text{field strength(dB}\mu\text{V/m)/20})}$.

The resulting values in µV/m should be entered on page 2 of the log book results sheet (table 35).

12j) For each angle, the 10 new recorded values of field strength in µV/m should be averaged according to the following formula:

$$\text{Average field strength } (\mu\text{V/m}) = \sqrt{\left(\frac{10}{\sum_{i=1}^{i=10} \frac{1}{field\ strength\ (\mu V/m)_i^{\,2}}}\right)}$$

The resulting eight average values should also be entered on page 2 of the log book results sheet (table 35).

12k) The procedure should continue with Step 13.

13) For the maximum sensitivity test only, the lowest of the 8 values of field strength (µV/m) calculated during the multiple-stage Step 12 represents the minimum field strength to which the EUT responds. This minimum value of field strength in µV/m should be entered on page 2 of the log book results sheet (table 35) as the maximum sensitivity.

14) For the average sensitivity test only, the average of the 8 values of field strength (µV/m) calculated during the multiple-stage Step 12 represents the average field strength to which the EUT responds. This average value of field strength in µV/m should now be calculated by the following:

$$\text{Average field strength } (\mu\text{V/m}) = \sqrt{\left(\frac{8}{\sum_{i=1}^{i=8} \frac{1}{field\ strength\ (\mu V/m)_i^{\,2}}}\right)}$$

This average value of field strength (µV/m) should be entered on page 2 of the log book results sheet (table 35) as the average sensitivity.

15) Steps 3 to 14 should be repeated with both the test and measuring antennas oriented for horizontal polarization.

7.3.1.3 Procedure for completion of the results sheets

All the necessary processing of the measured results is carried out during the course of the test procedure. The only calculation that remains to be performed before the overall results sheet (table 36) can be completed is the determination of expanded uncertainty of the measurement. This should be performed as given in subclause 7.3.2 and the resulting value entered in the overall results sheet (table 36).

7.3.1.4 Log book entries

Table 35: Log book results sheet

RECEIVER SENSITIVITY			**Date:**		**PAGE 1 of 2**
Temperature:.........°C		**Humidity:...............%**		**Frequency:.............MHz**	
Manufacturer of EUT:.....................		**Type No:.............**		**Serial No:..................**	
Range length :.......................					
Test equipment item	**Type No.**	**Serial No.**	**VSWR**	**Insertion loss**	**Antenna factor**
Test antenna				N/A	
Test antenna attenuator					N/A
Test antenna cable					N/A
Measuring antenna				N/A	
Measuring antenna attenuator					N/A
Measuring antenna cable					N/A
Ferrite beads			N/A	N/A	N/A
Receiving device				N/A	N/A
Signal generator				N/A	N/A
Digital voltmeter			N/A	N/A	N/A
Power supply			N/A	N/A	N/A
AF source (if applicable)			N/A	N/A	N/A
SINAD meter (if applicable)			N/A	N/A	N/A
Audio load (if applicable)			N/A	N/A	N/A
Bit stream generator (if applicable)			N/A	N/A	N/A
Bit error measuring test set (if applicable)			N/A	N/A	N/A
Acoustic coupler (if applicable)			N/A	N/A	N/A
Message generator (if applicable)			N/A	N/A	N/A
Response measuring test set (if applicable)			N/A	N/A	N/A
Mounting configuration of EUT					

(continued)

Table 35 (continued): Log book results sheet

RECEIVER SENSITIVITY (analogue speech)									Date:						PAGE 2 of 2		
Vertical polarization									**Horizontal polarization**								
Height above the turntable						m			Height above the turntable						m		
Height of the test antenna						m			Height of the test antenna						m		
Received signal level						dBµV			Received signal level						dBµV		
Output level from signal generator						dBm			Output level from signal generator						dBm		
Transform Factor						dB			Transform Factor						dB		
Signal generator level (dBm) against angle for 20 dB SINAD									**Signal generator level (dBm) against angle for 20 dB SINAD**								
	0°	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**		**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**
level									**level**								
Conversion to µV/m									**Conversion to µV/m**								
	0°	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**		**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**
level									**level**								
MAXIMUM Sensitivity						µV/m			MAXIMUM Sensitivity						µV/m		
AVERAGE Sensitivity						µV/m			AVERAGE Sensitivity						µV/m		
Values in the formula for Transform Factor																	
Measuring antenna cable loss									Measuring antenna cable loss								
Measuring antenna attenuator loss									Measuring antenna attenuator loss								
Measuring antenna balun loss									Measuring antenna balun loss								
Mutual coupling and mismatch loss (30 - 180 MHz)									Mutual coupling and mismatch loss (30 - 180 MHz)								
Antenna factor of the measuring antenna									Antenna factor of the measuring antenna								

RECEIVER SENSITIVITY (bit stream)									Date:						PAGE 2 of 2		
Vertical polarization									**Horizontal polarization**								
Height above the turntable						m			Height above the turntable						m		
Height of the test antenna						m			Height of the test antenna						m		
Received signal level						dBµV			Received signal level						dBµV		
Output level from signal generator						dBm			Output level from signal generator						dBm		
Transform Factor						dB			Transform Factor						dB		
Signal generator level (dBm) against angle for 10^{-2} BER									**Signal generator level (dBm) against angle for 10^{-2} BER**								
	0°	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**		**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**
level									**level**								
Conversion to µV/m									**Conversion to µV/m**								
	0°	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**		**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**
level									**level**								
MAXIMUM Sensitivity						µV/m			MAXIMUM Sensitivity						µV/m		
AVERAGE Sensitivity						µV/m			AVERAGE Sensitivity						µV/m		
Values in the formula for Transform Factor																	
Measuring antenna cable loss									Measuring antenna cable loss								
Measuring antenna attenuator loss									Measuring antenna attenuator loss								
Measuring antenna balun loss									Measuring antenna balun loss								
Mutual coupling and mismatch loss (30 - 180 MHz)									Mutual coupling and mismatch loss (30 - 180 MHz)								
Antenna factor of the measuring antenna									Antenna factor of the measuring antenna								

(continued)

Table 35 (concluded): Log book results sheet

RECEIVER SENSITIVITY (messages)											**Date:**				**PAGE 2 of 2**		
Vertical polarization									**Horizontal polarization**								
Height above the turntable						m			Height above the turntable						m		
Height of the test antenna						m			Height of the test antenna						m		
Received signal level						dBµV			Received signal level						dBµV		
Output level from signal generator						dBm			Output level from signal generator						dBm		
Transform Factor						dB			Transform Factor						dB		
Signal generator level (dBm) against angle									**Signal generator level (dBm) against angle**								
level	**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**	**level**	**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**
1									**1**								
2									**2**								
3									**3**								
4									**4**								
5									**5**								
6									**6**								
7									**7**								
8									**8**								
9									**9**								
10									**10**								
Conversion to µV/m									**Conversion to µV/m**								
level	**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**	**level**	**0°**	**45°**	**90°**	**135°**	**180°**	**225°**	**270°**	**325°**
1									**1**								
2									**2**								
3									**3**								
4									**4**								
5									**5**								
6									**6**								
7									**7**								
8									**8**								
9									**9**								
10									**10**								
Ave.									**Ave.**								
MAXIMUM Sensitivity						µV/m			MAXIMUM Sensitivity						µV/m		
AVERAGE Sensitivity						µV/m			AVERAGE Sensitivity						µV/m		
Values in the formula for Transform Factor																	
Measuring antenna cable loss									Measuring antenna cable loss								
Measuring antenna attenuator loss									Measuring antenna attenuator loss								
Measuring antenna balun loss									Measuring antenna balun loss								
Mutual coupling and mismatch loss (30 - 180 MHz)									Mutual coupling and mismatch loss (30 - 180 MHz)								
Antenna factor of the measuring antenna									Antenna factor of the measuring antenna								

7.3.1.5 Statement of results

The results should be presented in tabular form as shown in table 36.

Table 36: Overall results sheet

RECEIVER SENSITIVITY		Date:	PAGE 1 of 1
Vertical polarization		**Horizontal polarization**	
MAXIMUM Usable Sensitivity	µV/m	MAXIMUM Usable Sensitivity	µV/m
AVERAGE Usable Sensitivity	µV/m	AVERAGE Usable Sensitivity	µV/m
Expanded uncertainty (95 %)	dB	Expanded uncertainty (95 %)	dB

7.3.2 Measurement uncertainty for maximum or average usable sensitivity

A fully worked example illustrating the methodology to be used can be found in clause 4 of ETR 273-1-2 [10].

7.3.2.1 Uncertainty contributions: Stage one: Transform Factor

The first stage (determining the Transform Factor) involves placing a measuring antenna as shown in figure 49 and determining the relationship between the signal generator output power level and the resulting field strength (the shaded areas in figure 42 represent components common to both stages of the test).

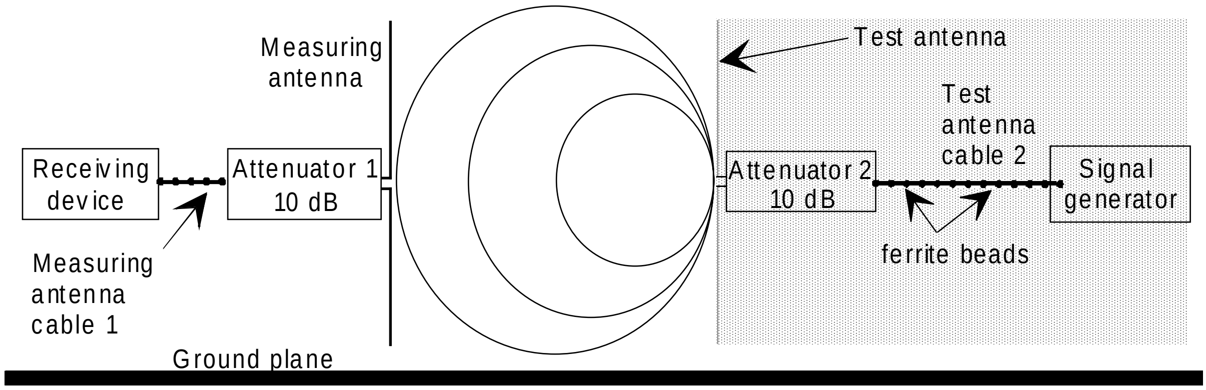

Figure 49: Stage 1: Transform Factor

All the uncertainty components which contribute to this stage of the test are listed in table 37. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contribution.

Table 37: Contributions for the transform factor

uj or i	Description of uncertainty contributions	dB
u_{j36}	*mismatch: transmitting part*	
u_{j37}	*mismatch: receiving part*	
u_{j38}	*signal generator: absolute output level*	0,00
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: measuring antenna cable*	
u_{j19}	*cable factor: test antenna cable*	
u_{j41}	*insertion loss: measuring antenna cable*	
u_{j41}	*insertion loss: test antenna cable*	0,00
u_{j40}	*insertion loss: measuring antenna attenuator*	
u_{j40}	*insertion loss: test antenna attenuator*	0,00
u_{j47}	*receiving device: absolute level*	
u_{j16}	*range length*	
u_{j44}	*antenna: antenna factor of the measuring antenna*	
u_{j45}	*antenna: gain of the test antenna*	
u_{j46}	*antenna: tuning of the measuring antenna*	
u_{j46}	*antenna: tuning of the test antenna*	0,00
u_{j22}	*position of the phase centre: measuring antenna*	
u_{j14}	*mutual coupling: measuring antenna to its images in the ground plane*	
u_{j14}	*mutual coupling: test antenna to its images in the ground plane*	
u_{j11}	*mutual coupling: measuring antenna to the test antenna*	
u_{j12}	*mutual coupling: interpolation of mutual coupling and mismatch loss correction factors*	
u_{i01}	*random uncertainty*	

The standard uncertainties from table 37 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ contributions\ from\ the\ Transform\ Factor}$) for the transform factor in dB.

7.3.2.2 Uncertainty contributions: Stage 2: EUT measurement

The second stage (the EUT measurement) is to determine the minimum signal generator output level which produces the required response from the EUT as shown in figure 50 (the shaded areas represent components common to both stages of the test).

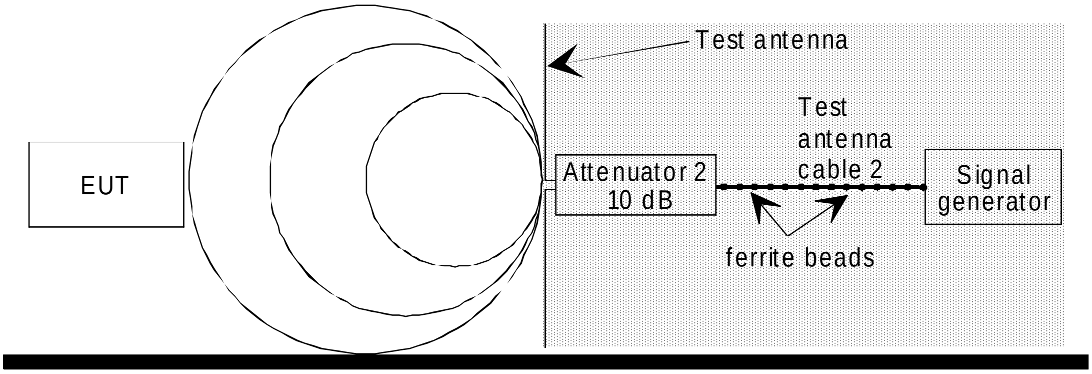

Figure 50: Stage 2: EUT measurement

All the uncertainty components which contribute to this stage of the test are listed in table 38. ETR 273-1-1 [9] annex A should be consulted for the sources and/or magnitudes of the uncertainty contributions.

Table 38: Contributions from the EUT measurement

uj or I	Description of uncertainty contributions	dB
u_{j36}	*mismatch: transmitting part*	
u_{j38}	*signal generator: absolute output level*	0,00
u_{j39}	*signal generator: output level stability*	
u_{j19}	*cable factor: test antenna cable*	
u_{j41}	*insertion loss: test antenna cable*	0,00
u_{j40}	*insertion loss: test antenna attenuator*	0,00
u_{j20}	*position of the phase centre: within the EUT volume*	
u_{j21}	*positioning of the phase centre: within the EUT over of the axis of rotation of the turntable*	
u_{j52}	*EUT: modulation detection*	
u_{j16}	*range length*	
u_{j45}	*antenna: gain of the test antenna*	0,00
u_{j46}	*antenna: tuning of the test antenna*	0,00
u_{j55}	*EUT: mutual coupling to the power leads*	
u_{j08}	*mutual coupling: amplitude effect of the test antenna on the EUT*	
u_{j13}	*mutual coupling: EUT to its image in the ground plane*	
u_{j14}	*mutual coupling: test antenna to its image in the ground plane*	
u_{i01}	*random uncertainty*	

The standard uncertainties from table 38 should be combined by RSS in accordance with clause 5 of ETR 273-1-1 [9]. This gives the combined standard uncertainty ($u_{c\ contribution\ from\ the\ EUT\ measurement}$) for the EUT measurement in dB.

7.3.2.3 Expanded uncertainty of the receiver sensitivity measurement

The combined uncertainty of the sensitivity measurement is the combination of the components outlined in subclauses 7.3.2.1 and 7.3.2.2. The components to be combined are $u_{c\ contribution\ from\ the\ Transform\ Factor}$ and $u_{c\ contribution\ from\ the\ EUT\ measurement}$.

$$u_c = \sqrt{u_{c\ contribution\ from\ the\ Transform\ factor}^2 + u_{c\ contribution\ from\ the\ EUT\ measurement}^2} = \_\_,\_\_ \text{ dB}$$

The expanded uncertainty is ± 1,96 x u_c = ± __,__ dB at a 95 % confidence level.

7.3.3 Co-channel rejection

This test is normally carried out using a test fixture and as a result has not been considered for the anechoic chamber.

7.3.4 Adjacent channel selectivity

This test is normally carried out using a test fixture and as a result has not been considered for the anechoic chamber.

7.3.5 Intermodulation immunity

This test is normally carried out using a test fixture and as a result has not been considered for the anechoic chamber.

7.3.6 Spurious response rejection

This test is normally carried out using a test fixture and as a result has not been considered for the anechoic chamber.

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