

**Speech processing, Transmission and Quality Aspects (STQ);  
Transmission characteristics of digital  
Private Branch eXchanges (PBXs) for interconnection  
to private networks, to the public switched network  
or to IP gateways**

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## Foreword

This ETSI Standard (ES) has been produced by ETSI Technical Committee Speech processing, Transmission and Quality aspects (STQ) and is now submitted for the ETSI standards Membership Approval Procedure.

The present document is intended to be used as a specification for the design of Private Branch eXchanges (PBXs) and for the harmonization of PBX transmission parameters throughout Europe. It has been developed based on four Interim ETSs (I-ETSs), one ETS and the first version of the present document, all of which are replaced by the present document:

- I-ETS 300 003 (1991): "Business Telecommunications (BT); Transmission characteristics of digital Private Automatic Branch Exchanges (PABXs)";
- I-ETS 300 004 (1991): "Business Telecommunications (BT); Transmission characteristics at 2-wire analogue interfaces of a digital Private Automatic Branch Exchange (PABX)";
- I-ETS 300 005 (1991): "Business Telecommunications (BT); Transmission characteristics at 4-wire analogue interfaces of a digital Private Automatic Branch Exchange (PABX)".
- I-ETS 300 006 (1991): "Business Telecommunications (BT); Transmission characteristics at digital interfaces of a digital Private Automatic Branch Exchange (PABX)".
- ETS 300 439 (1996): "Business Telecommunications (BTC); Transmission characteristics of digital Private Branch eXchanges (PBXs)".
- ES 201 168 (V1.1.1): "Corporate Networks (CN); Transmission characteristics of digital Private Branch eXchanges (PBXs)".

In the application of this PBX standard it should be considered that no network access requirements are contained herein. ETSI is maintaining a set of access requirement documents some of which have formerly been the technical basis for harmonized European regulation. In order to enable a suitable end-to-end speech transmission performance it will necessary to comply with the appropriate network access requirements as well.

---

# 1 Scope

The present document specifies the transmission requirements for digital Private Branch eXchanges (PBXs) (through-connecting telecommunications equipment) that:

- are not part of the public network;
- are intended for interconnection either to the public switched network, to a Private Network (e.g., a Corporate Network) or to an IP-Gateway;
- carry 3,1 kHz voice telephony between analogue interfaces, digital interfaces carrying 64 kbit/s A-law encoded signals and the acoustic interfaces of handset telephony terminals (wired or cordless) that are designed to be used together with the PBX for connections involving digital access to the public switched network;
- are capable of providing, for the purposes of testing, a test point that offers a 64 kbit/s signal with bit integrity to the digital transmission path (this test point need not be provided in production versions of a PBX);
- carry 3,1 kHz voice telephony, irrespective of whether they carry other services in addition.

In the light of recent developments on the marketplace it should clearly be understood that the present document may be applied not only to traditional types of PBXs but rather to every functional unit which performs like a PBX according to the aforementioned conditions.

NOTE: When dealing with voice bandwidth data transmission, special consideration may have to be given to certain parameters e.g. group delay distortion, error performance, bit integrity, bit sequence independence (the list is not exhaustive).

The present document does not apply to:

- handsfree and loud-speaking telephony terminals;
- the interface between the PBX and system specific telephones (excluding the acoustic interfaces as stated above) irrespective whether they are wired or cordless.

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# 2 References

The following documents contain provisions which, through reference in this text, constitute provisions of the present document.

- References are either specific (identified by date of publication, edition number, version number, etc.) or non-specific.
- For a specific reference, subsequent revisions do not apply.
- For a non-specific reference, subsequent revisions do apply.
- A non-specific reference to an ETS shall also be taken to refer to later versions published as an EN with the same number.

- [1] ETSI EG 201 050 (V1.2.2): "Speech Processing, Transmission and Quality Aspects (STQ); Overall Transmission Plan Aspects for Telephony in a Private Network".
- [2] ETSI I-ETS 300 245-3 (1995): "Integrated Services Digital Network (ISDN); Technical characteristics of telephony terminals; Part 3: Pulse Code Modulation (PCM) A-law, loudspeaking and handsfree telephony".
- [3] ETSI TBR 10 (1999): "Digital Enhanced Cordless Telecommunications (DECT); General Terminal Attachment Requirements; Telephony Applications".
- [4] ITU-T Recommendation G.101 (08/96): "The transmission plan".
- [5] ITU-T Recommendation G.103 (12/98): "Hypothetical reference connections".

- [6] ITU-T Recommendation G.107 (05/00): "The E-model, a computational model for use in transmission planning".
- [7] ITU-T Recommendation G.108 (09/99): "Application of the E-model - a planning guide".
- [8] ITU-T Recommendation G.113 (Draft Revised version 05/00): "Transmission Impairments".
- [9] ITU-T Recommendation G.122 (03/93): "Influence of national systems on stability and talker echo in international connections".
- [10] ITU-T Recommendation G.223 (11/88): "Assumptions for the calculation of noise on hypothetical reference circuits for telephony".
- [11] ITU-T Recommendation G.703 (11/98): "Physical/electrical characteristics of hierarchical digital interfaces".
- [12] ITU-T Recommendation G.711 (11/88): "Pulse code modulation (PCM) of voice frequencies".
- [13] ITU-T Recommendation G.712 (11/96): "Transmission performance characteristics of pulse code modulation channels".
- [14] ITU-T Recommendation G.726 (12/90): "40, 32, 24, 16 kbit/s adaptive differential pulse code modulation (ADPCM)".
- [15] ITU-T Recommendation G.727 (12/90): "5-, 4-, 3- and 2-bits/sample embedded adaptive differential pulse code modulation (ADPCM)".
- [16] ITU-T Recommendation G.728 (09/92): "Coding of speech at 16 kbit/s using low-delay code excited linear prediction".
- [17] ITU-T Recommendation I.430 (11/95): "Basic user - network interface - Layer 1 specification".
- [18] ITU-T Recommendation O.9 (03/99): "Measuring arrangements to access the degree of unbalance about earth".
- [19] ITU-T Recommendation O.41 (10/94): "Psophometer for use on telephone-type circuits".
- [20] ITU-T Recommendation O.131 (11/88): "Quantizing distortion measuring equipment using a pseudo-random noise test signal".
- [21] ITU-T Recommendation O.132 (11/88): "Quantizing distortion measuring equipment using a sinusoidal test signal".
- [22] ITU-T Recommendation O.133 (03/93): "Equipment for measuring the performance of PCM encoders and decoders".
- [23] ITU-T Recommendation P.50 (03/93): "Artificial Voices".
- [24] ITU-T Recommendation P.51 (08/96): "Artificial mouth".
- [25] ITU-T Recommendation P.57 (08/96): "Artificial ears".
- [26] ITU-T Recommendation P.58 (08/96): "Head and torso simulator for telephonometry".
- [27] ITU-T Recommendation P.59 (03/93): "Artificial Conversational Speech".
- [28] ITU-T Recommendation P.64 (09/99): "Determination of sensitivity/frequency characteristics of local telephone systems".
- [29] ITU-T Recommendation P.79 (09/99): "Calculation of loudness ratings for telephone sets".
- [30] ITU-T Recommendation P.501 (08/96): "Test signals for use in telephonometry".
- [31] ITU-T Recommendation Q.551 (11/96): "Transmission characteristics of digital exchanges".

- [32] ITU-T Recommendation Q.552 (11/96): "Transmission characteristics at 2-wire analogue interfaces of digital exchanges".
- [33] ITU-T Recommendation Q.553 (11/96): "Transmission characteristics at 4-wire analogue interfaces of digital exchanges".
- [34] IEC 60651 (03/94): "Sound level meters".
- [35] IEC 61260 (07/95): "Electroacoustics - Octave-Band And Fractional-Octave-Band Filters".
- [36] ISO 3 (1973): "Preferred numbers - series of preferred numbers".
- [37] ISO 9614-1 (1993): "Acoustics - Determination of sound power levels of noise sources using sound intensity; Part 1: Measurement at discrete points".
- [38] ETSI TR 101 802 (V1.1.1): "Speech processing, Transmission and Quality aspects (STQ); The Concept of Relative Levels".

NOTE: The present document also contains a number of informative references which have been included to indicate the sources from which various material has been derived, hence they do not have an associated normative reference number. Details of these publications are given in annex C.

---

## 3 Definitions and abbreviations

### 3.1 Definitions

For the purposes of the present document, the following definitions apply:

#### 3.1.1 Private Branch eXchange (PBX)

A through connecting telecommunications equipment capable of establishing circuit switched connections between different interfaces under the control of the end user and intended for interconnection either to the PSTN, to a Private Network (e.g., a Corporate Network) or to an IP-Gateway.

#### 3.1.2 Test points, PBX input and output and half connections

In the following subclauses, the concepts of a "standard digital generator" and "a standard digital analyser" should be assumed and these are defined as follows.

**standard digital generator:** hypothetical device which is absolutely ideal, i.e. a perfect analogue-to-digital converter preceded by an ideal low pass filter (assumed to have no attenuation/frequency distortion and no group delay distortion), and which may be simulated by a digital processor.

**standard digital analyser:** hypothetical device which is absolutely ideal, i.e. a perfect digital-to-analogue converter followed by an ideal low pass filter (assumed to have no attenuation/frequency distortion and no group delay distortion), and which may be simulated by a digital processor.

The following specifications are based on ideal measuring equipment. Therefore, they do not include any margin for measurement errors.

##### 3.1.2.1 Test points

The test points shown in figure 3 are defined for specification purposes. They may not physically exist in a PBX but may be accessed at the Access Point (AP) via the digital switching network. In this case, a part or all of the switching network will be included in the path from the PBX interface to the points of access to the test points.

NOTE: For more information see annex A, clause A.2.

### 3.1.2.2 PBX input and output

The PBX input and output for a connection through a digital PBX are located at the interfaces identified in clause 1 and shown in figures 1, 2 and 3.

### 3.1.2.3 Half connections (analogue 2-wire or 4-wire, or digital)

- Input connection: an unidirectional path from an input of a digital PBX to an output test point.
- Output connection: an unidirectional path from an input test point to an output of a digital PBX.
- Half connection: a bi-directional path comprised of an input connection and an output connection, both having the same interface.

## 3.1.3 Relative levels

### 3.1.3.1 Test points

The input and output test points are defined as 0 dBr points for the equipment under test.

NOTE: See TR 101 802 [38] for a discussion of relative levels.

### 3.1.3.2 Analogue interfaces

The nominal relative level at the PBX input point is designated  $L_i$ .

The nominal relative level at the PBX output point is designated  $L_o$ .

## 3.1.4 Transmission loss

### 3.1.4.1 Nominal transmission loss, analogue half connections

A connection through the PBX (see figure 3) is established by connecting in both directions an input located at one interface to an output located at another interface.

The nominal transmission loss between the input at an analogue interface and the output test point is defined as:

$$NL_i = L_i \quad [\text{dB}]$$

The nominal transmission loss between the input test point and the output of an analogue interface is defined as:

$$NL_o = -L_o \quad [\text{dB}]$$

NOTE: It is assumed that  $L_i$  and  $L_o$  are achieved by operating on the analogue signal, only.

### 3.1.4.2 Switching Loss (SL)

Where there are two digital points within the PBX between which bit integrity is not preserved, there may be a Switching Loss (SL) between them.

NOTE 1: Devices which cause bit integrity to be lost include digital pads, code converters (e.g., low bit-rate coders) and echo control devices.

NOTE 2: SL may be associated with a digital interface, with additional loss adjustment of an analogue interface, or with additional loss adjustment within the switching network. As an example, switching loss may be constantly assigned to an interface, e.g. to achieve a  $L_i$  of +3 dBr by using an ideal codec followed by a 3 dB digital loss. The requirements assume, however, that all kinds of SL can be switched off for testing purposes (see also clause 4).

NOTE 3: By the use of the concept of SL the relative levels can remain unchanged.

### 3.1.4.3 Nominal transmission loss, full connections

The nominal transmission loss for a connection through a PBX is equal to the difference of the relative levels at the input and the output, plus switching loss in the connection. Therefore the nominal transmission loss between analogue interfaces is defined as:

$$NL = L_i - L_o + SL \quad [\text{dB}]$$

The nominal transmission loss between the input of an analogue interface and the output of a digital interface is defined as:

$$NL = L_i + SL \quad [\text{dB}]$$

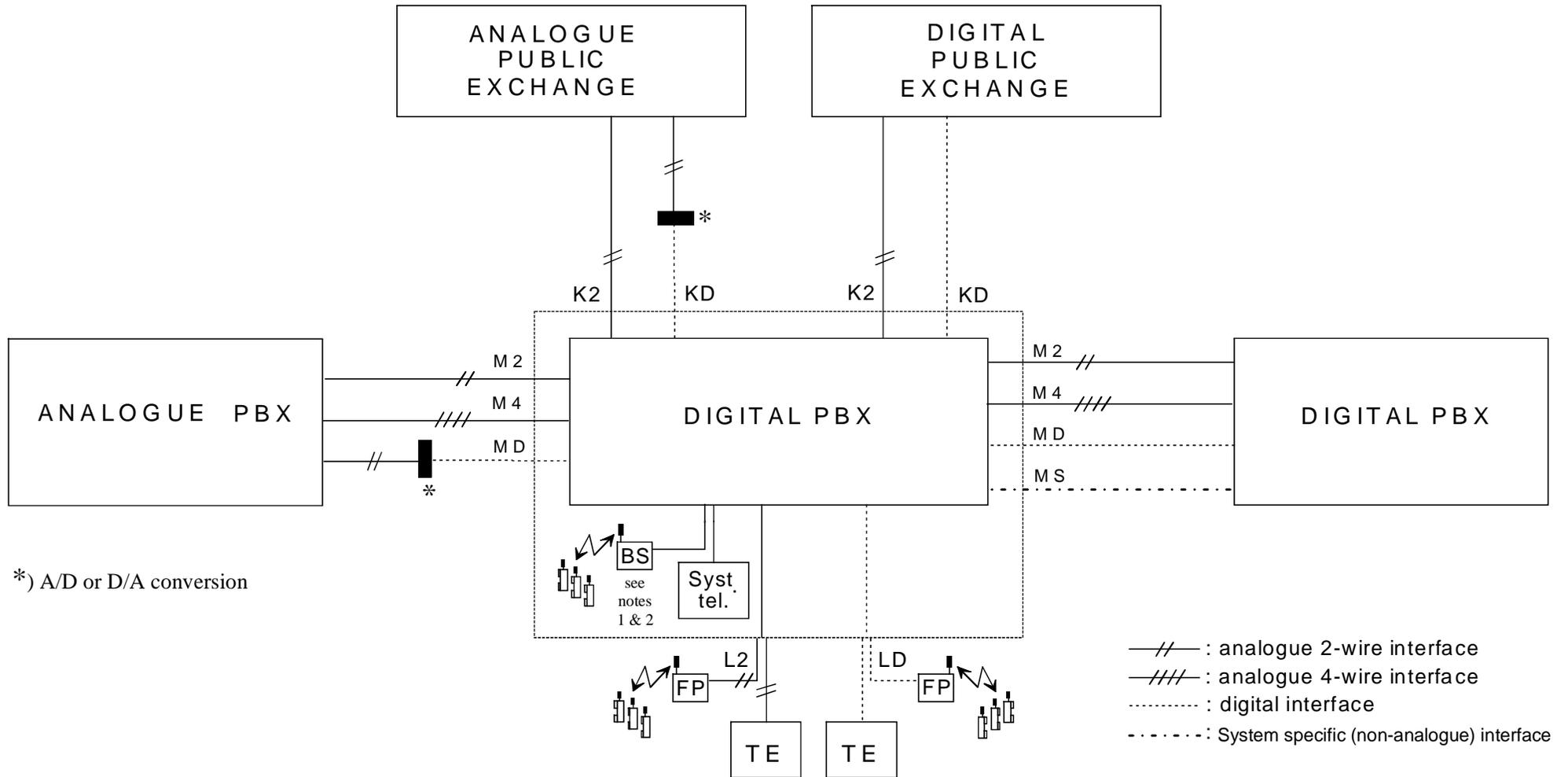
The nominal transmission loss between the input of a digital interface and the output of an analogue interface is defined as:

$$NL = -L_o + SL \quad [\text{dB}]$$

The nominal transmission loss between digital interfaces is defined as:

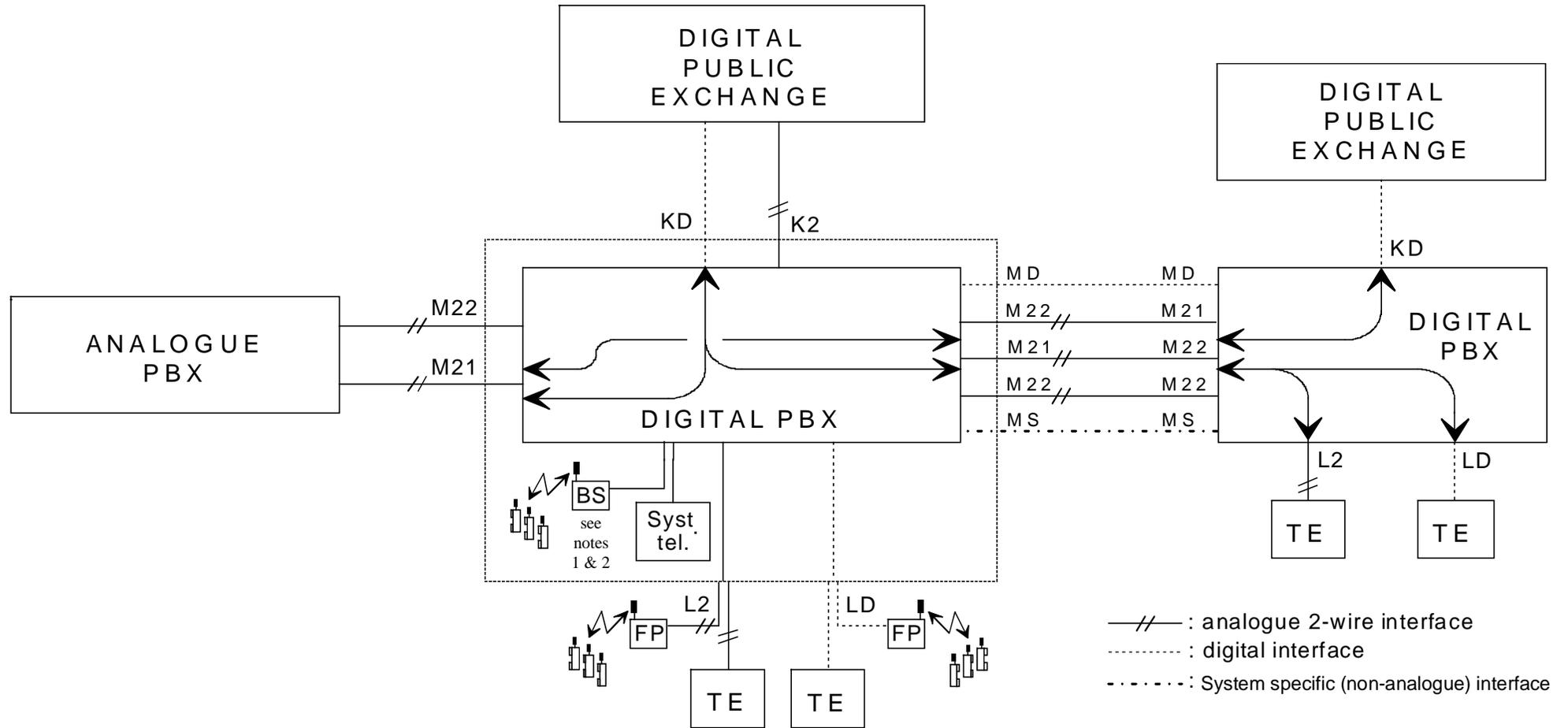
$$NL = SL \quad [\text{dB}]$$

NOTE: SL represents the value of any Switching Loss implemented in the PBX.



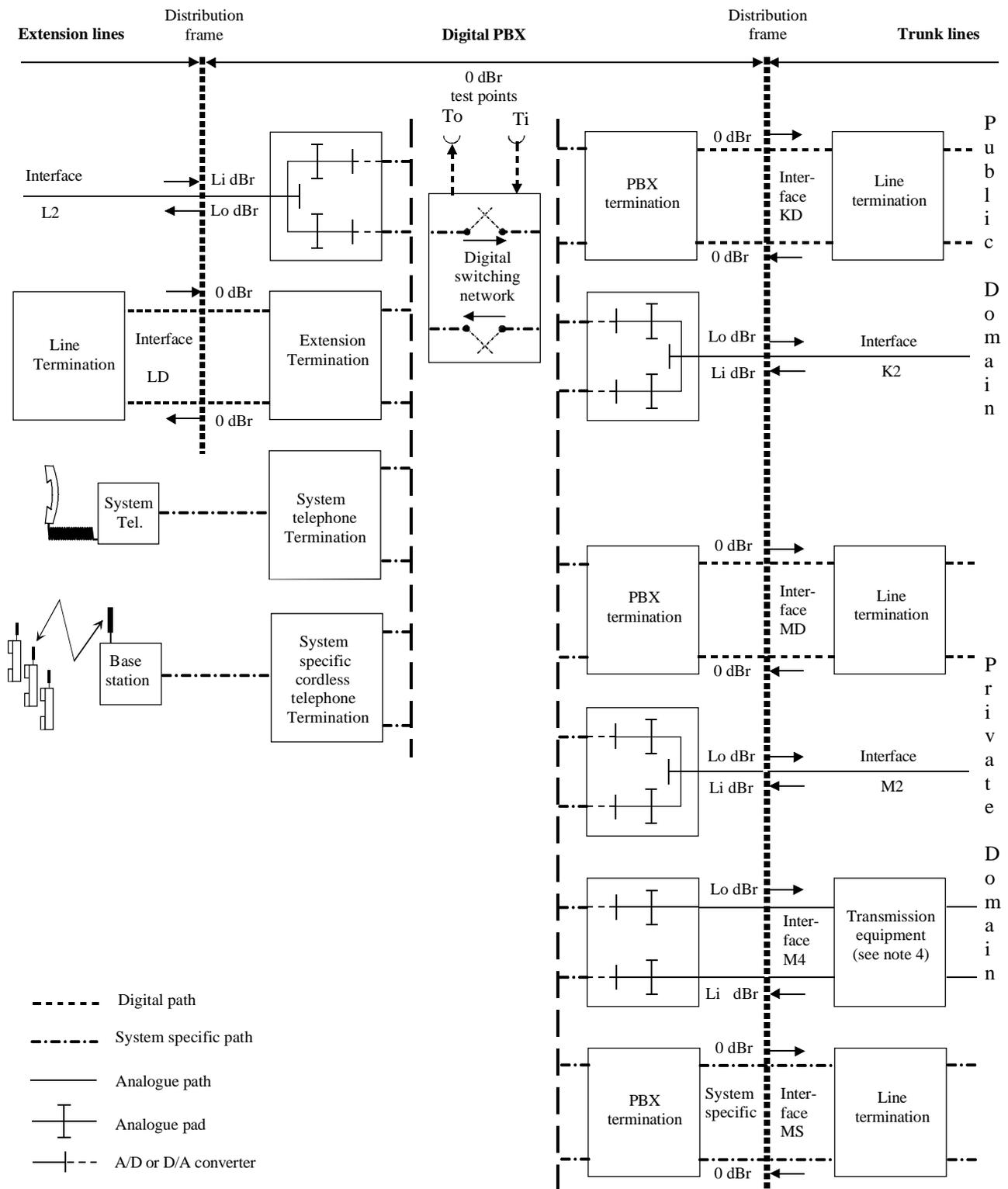
NOTE 1: The present document does not apply to the interface between the PBX and system specific telephones irrespective whether they are wirebound or cordless.  
 NOTE 2: The Base Station (BS) may also be integrated into the digital PBX.

Figure 1: Interfaces of digital PBX's in network interconnections



NOTE 1: The present document does not apply to the interface between the PBX and the system specific telephones irrespective whether they are wirebound or cordless.  
 NOTE 2: The Base Station (BS) may also be integrated into the digital PBX.

Figure 2: Detailed illustration for access to Public Switched Telephone Network (PSTN) involving M interfaces



- NOTE 1: Digital loss pads, if required, may be located in the switching network or the PBX terminals (see subclause 3.1.3.2).
- NOTE 2: For different interfaces, the value of Li and Lo are, in general, not equal.
- NOTE 3: This figure shows typical examples utilizing the defined interfaces.
- NOTE 4: This term refers to different types of transmission equipment (e.g., FDM, TDM, etc.).

Figure 3: Interfaces, transmission levels and test points at a digital PBX

### 3.1.5 Loss distortion with frequency

The loss distortion with frequency is the logarithmic ratio of output voltage at the reference frequency (nominally 1 020 Hz),  $U(1\ 020\ \text{Hz})$ , divided by its value at frequency  $f$ ,  $U(f)$ :

$$D_L = 20 \log \frac{U(1020\text{Hz})}{U(f)} \text{ [dB]}$$

See ITU-T Recommendation Q.551 [31].

### 3.1.6 Parameters relevant for echo and stability

Terminal Balance Return Loss (TBRL) is introduced in order to characterize the PBX performance with respect to echo. The TBRL of an equipment port is measured in the talking state as in an established connection through a digital PBX. For measurement of TBRL, see annex A.

The parameter "stability loss" as defined in ITU-T Recommendation G.122 [9], applies to the worst terminating conditions encountered at a 2-wire interface in normal operation.

#### 3.1.6.1 Terminal Balance Return Loss (TBRL)

The term TBRL is used to characterize an impedance balancing property of the 2-wire analogue equipment port.

The expression for TBRL is:

$$TBRL = 20 \log \left| \frac{Z_a + Z_b \cdot \frac{Z_t + Z_b}{Z_t - Z_b}}{2 \cdot Z_a} \right| \text{ [dB]}$$

where:

- $Z_a$ : PBX input impedance of a 2-wire equipment port;
- $Z_b$ : impedance of the balance network presented at a 2-wire equipment port;
- $Z_t$ : impedance of the balance test network.

NOTE: It could be advantageous to choose  $Z_a = Z_b$  in order to optimize TBRL. In this case the expression reduces to:

$$TBRL = 20 \log \left| \frac{Z_t + Z_b}{Z_t - Z_b} \right| \text{ [dB]}$$

#### 3.1.6.2 Stability loss

The stability loss is defined as the loss between the PBX test points  $T_i$  and  $T_o$  of a half connection (see also annex A).

#### 3.1.6.3 Echo Loss (EL) and weighted Terminal Coupling Loss (TCLw)

Couplings via hybrids or acoustic paths of telephone sets, are normally subject to extensive shape in their frequency response. For the effect of echo, when considering the echo behaviour of a hybrid, the transhybrid loss is weighted with a specific weighting scale over the frequency range 300 Hz to 3 400 Hz. This weighted transhybrid loss is then called Echo Loss (EL). For the (acoustical) echo path of digital telephone sets presently the same weighting is used and expressed as weighted Terminal Coupling Loss (TCLw).

According to ITU-T Recommendation G.122 [9], subclause 4.2, EL and TCLw are derived from the integral of the power transfer characteristic  $A(f)$  weighted by a negative slope of 3 dB/octave from 300 Hz to 3 400 Hz as follows:

$$EL = 3,85 - 10 * \log \left\{ \int_{300}^{3400} \frac{A(f)}{f} df \right\} \quad (dB)$$

where:

$$A(f) = 10^{-Lab(f)/10}$$

with Lab as the loss of the echo path at frequency f. If the results are available in graphical form or as tabulated data, the EL may also be calculated using the trapezoidal rule. More information is given in annex B of ITU-T Recommendation G.122 [9].

### 3.1.7 Digital parameters

#### 3.1.7.1 Bit integrity

Bit integrity is the property of a digital half connection in which the binary values and the sequence of the bits in an octet and of the octets at the input of the half connection are reproduced exactly at the output.

NOTE: Digital processing devices are to be disabled to provide bit integrity when needed.

### 3.1.8 Characteristics of interfaces

The interfaces taken into account are those of figure 3. For voice frequency interfaces (L2, M2, K2 and M4) the electrical parameters refer to the appropriate Interface Measurement Points (IMP). For further details, see subclause A.1.5. For limitations on the cable length between Distribution Frame (DF) and the actual digital PBX interface, see ITU-T Recommendation G.703 [11].

#### 3.1.8.1 2-wire analogue interface

##### 3.1.8.1.1 Interface L2

The interface L2 provides for the connection of 2-wire analogue extension lines and will carry signals such as speech, voice-band analogue data and multi-frequency push-button signals, etc. In addition, the interface L2 provides for ordinary functions such as direct current (DC) feeding, DC signalling, ringing, etc.

NOTE 1: Since the interface L2 terminates the extension line, the impedance and unbalance about earth should be controlled.

NOTE 2: The interface L2 is a 2-wire analogue extension interface used to connect terminals which are also intended to be connected directly to the PSTN.

##### 3.1.8.1.2 Interface M2

The interface M2 provides for connection to 2-wire analogue inter-PBX circuits e.g. via leased lines. The interface M2 is subdivided into the interfaces "M21" and "M22".

The interface M21 provides the termination of connections to/from the PSTN wired to all types of K interfaces (also via digital (Interface KD, see subclause 3.1.8.3.3) subscriber line access) with the PBX concerned acting as a transit switch (see figure 2).

The interface M22 provides the termination of connections other than those covered by M21. A typical example is the interconnection of an L2 interface with an M22 interface in a PBX for routings through existing 2-wire analogue circuits to other PBXs (see figure 2).

### 3.1.8.1.3 Interface K2

The interface K2 provides for the connection of 2-wire analogue subscriber lines between PBX and Public Exchange.

NOTE: Since the interface K2 terminates the line to the public exchange, the impedance and unbalance about earth should be controlled, in general, those parameters are subject to standards which provide for the individual network access.

## 3.1.8.2 4-wire analogue interfaces

### 3.1.8.2.1 Interface M4

The interface M4 provides for connection to 4-wire analogue inter-PBX circuits.

With the PBX acting as a transit switch (see figures 1 and 3), this interface can be part of an incoming or outgoing connection to the public network.

NOTE: The performance of different transmission media used in conjunction with 4-wire analogue circuits between PBXs is not addressed in this document; the following example may provide guidance on this topic: An analogue subscriber interface K2 in PBX A is connected another analogue subscriber interface K2 in PBX B. The interconnection between the two PBXs is provided via a M4 interface in PBX A, an analogue 4-wire line and another M4 interface in PBX B. In order to calculate the actual value for the Overall Loudness Rating (OLR), beside the relative levels and the switching loss, the actual loss of the 4-wire line between the two PBXs should be considered.

## 3.1.8.3 Digital interfaces

### 3.1.8.3.1 Interface LD

The interface LD is a digital extension interface used to connect terminals which are also intended to be connected directly to digital interfaces of the public switched network.

### 3.1.8.3.2 Interface MD

The interface MD provides for connection to a digital inter-PBX circuit.

### 3.1.8.3.3 Interface KD

The interface KD provides for the connection of a digital access to the public switched network.

## 3.1.8.4 System specific (non-analogue) interfaces

### 3.1.8.4.1 Interface MS

The interface MS provides for connection to a system specific (non-analogue) inter-PBX circuit.

## 3.1.9 Voice band parameters of a connection between two interfaces of the same PBX

### 3.1.9.1 General

This subclause provides guidance on obtaining the overall characteristics for connections between two interfaces of the same PBX.

The transmission parameters relating to the input connection from a PBX interface to a PBX output test point will be referred to as input parameters. Transmission parameters relating to the output connection from a PBX input test point to a PBX interface will be referred to as output parameters. For additional information about the measurement configurations, see annex A.

### 3.1.9.2 Overall transmission parameters

#### 3.1.9.2.1 Transmission loss

The transmission loss in each direction through the PBX is equal to the algebraic sum of the input transmission loss, the output transmission loss, and the Switching Loss (SL) in each direction between the two interfaces.

#### 3.1.9.2.2 Other overall parameters

The overall characteristic for the following parameters can be obtained as given in subclause 3.1.9.2.1:

- loss distortion with frequency;
- variation of gain with input level.

### 3.1.9.3 Delay

#### 3.1.9.3.1 Mean one way transmission time

The mean one way transmission time is the algebraic sum of the one-way transmission times in both directions of transmission between the two interfaces (of the PBX) divided by two.

NOTE: The one-way transmission time through a PBX may vary mainly dependent on the PBX architecture, the types of connections involved and the traffic load.

#### 3.1.9.3.2 Group delay

The time of propagation between two points of a certain element (for example the crest) of the envelope of a wave. For a given frequency it is equal to the first derivative of the phase shift measured in radians, between these points, with reference to the angular frequency measured in radians per second.

#### 3.1.9.3.3 Group delay distortion

The difference between group delay at a given frequency and minimum group delay, in the frequency band of interest.

## 3.1.10 Loudness Ratings (LR)

Within the context of ITU-T, a loudness rating is an objective measure of the loudness loss, i.e., a weighted, electro-acoustic loss between certain interfaces in the telephone network.

### 3.1.10.1 Receive Loudness Rating (RLR)

The loudness loss between an electric interface and the Ear Reference Point (ERP).

### 3.1.10.2 Send Loudness Rating (SLR)

The loudness loss between the Mouth Reference Point (MRP) and an electric interface.

### 3.1.10.3 Talker sidetone, SideTone Masking Rating (STMR)

The loudness loss between the MRP and the ERP via the sidetone path under free sound field conditions.

### 3.1.10.4 Listener SideTone Rating (LSTR)

The loudness loss between the MRP and the ERP via the electrical sidetone path under diffuse sound field conditions.

### 3.1.10.5 Talker Echo Loudness Rating (TELR)

The transmitted speech signal of the talking subscriber is delayed along the different sections of the transmission path, coupled at the far end and received again with further delay, affecting the talker with an echo of his own voice. Since this type of echo in the given configuration is only observed by the talker, it is called Talker Echo. The magnitude of the talker echo is characterized by the Talker Echo Loudness Rating (TELR).

$$\text{TELR} = \text{EL} + \text{SLR} + \text{RLR}$$

Here SLR and RLR are the send and receive loudness ratings of the talker's telephone set, referred to that 4-wire interface where the Echo Loss (EL) (see subclause 3.1.6) applies.

### 3.1.10.6 Noise rejection capability

When room noise is present a higher received signal level (lower  $\text{RLR}_H$ ) is required to give the best possible receiving speech quality and intelligibility. The increase in the receiving level is a function of increasing room noise level.

When room noise is present people raise their voice level (talk louder) and the sending speech level will be higher than the optimum level. By decreasing the sending sensitivity (higher  $\text{SLR}_H$ ) the sending level to the line will be around optimum and at the same time the absolute level of the transmitted noise will decrease.

For every dB increase in room noise level there is a corresponding increase in the voice level of the talker of about 0,5 dB (see ITU-T Recommendation G.107 [6]). This effect - also referred to as part of the Lombard Effect - permits the receiving sensitivity to be increased and the sending sensitivity to be reduced by a similar 0,5 dB.

### 3.1.11 System specific telephony terminal (wired or cordless)

A system specific telephony terminal (wired or of a cordless system) is a telephony terminal used for a specific PBX family for use in a digital environment. The system specific telephony terminal (wired) or the Base Station (BS) of the cordless system may be connected via a digital or an analogue line to the system specific telephone termination (see figure 4). The BS may also be integrated within the PBX. The system specific telephony terminal (including the air interface of a cordless telephony terminal) is considered an integral part of the PBX in the sense that the characteristics of the path between the PBX itself and the telephony terminal is not subject to standardization. The system specific telephony terminal (wired or cordless) is not intended for direct connection to a public network.

### 3.1.12 Ear Reference Point (ERP)

A point located at the entrance to the ear canal of the listener's ear as described in figure A.1 of ITU-T Recommendation P.64 [28].

### 3.1.13 Mouth Reference Point (MRP)

A point 25 mm in front of and on the axis of the lip position of a typical human mouth (or artificial mouth) (see figure A.1 of ITU-T Recommendation P.64 [28]).

### 3.1.14 Acoustic Reference Level (ARL)

The acoustic level which gives -10 dBm0 at the digital output test point.

### 3.1.15 dBPa

Sound pressure level relative to 1 Pa (no weighting).

### 3.1.16 dBPa(A)

Sound level relative to 1 Pa measured using the A-weighting defined in IEC 60651 [34].

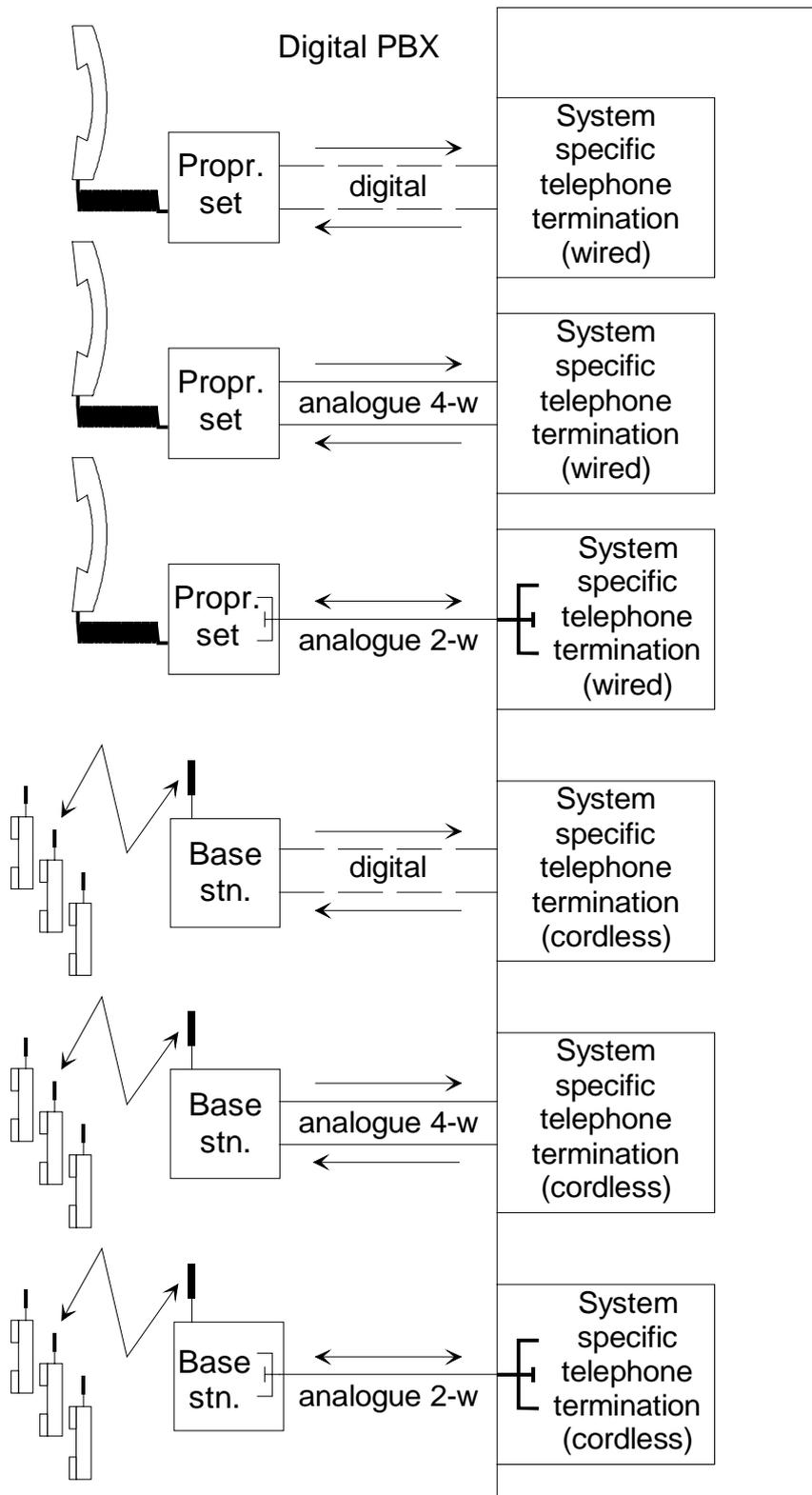


Figure 4: System specific telephone configurations (wired or cordless)

## 3.2 Abbreviations

For the purposes of the present document, the following abbreviations apply:

AC	Alternating Current
AP	Access Point
APC	Access Point Connection
ARL	Acoustic Reference Level
BS	Base Station
DC	Direct Current
DF	Distribution Frame
DRS	Digital Reference Sequence
DTS	Digital Test Sequence
EL	Echo Loss
emf	electro motoric force
ERP	Ear Reference Point
FDM	Frequency Division Multiplex
FEXT	Far End Crosstalk
FFT	Fast Fourier Transformation
IMP	Interface Measurement Point
IP	Internet Protocol
IUT	Interface Under Test
LCL	Longitudinal Conversion Loss
LCTL	Longitudinal Conversion Transfer Loss
LD	Loss Distortion
LR	Loudness Rating
LRGP	Loudness Rating Guard ring Position
LSTR	Listener SideTone Rating
LSTRcorr	corrected LSTR value
LSTRmeas	measured LSTR value
MNRU	Modulated Noise Reference Unit
MRP	Mouth Reference Point
NEXT	Near End Crosstalk
NL	Nominal (Transmission) Loss
NS	Not Specified
PBN	Private Branch Network
PBX	Private Branch eXchange
PCM	Pulse Code Modulation
PP	Portable Part
PSTN	Public Switched Telephone Network
qdu	quantizing distortion unit
RLH	Return Loss Hybrid
RLR	Receive Loudness Rating
RLRmeas	measured RLR value
RLRnom	declared nominal RLR value
rms	root mean square
RPP	Reference Portable Part
SL	Switching Loss
SLR	Send Loudness Rating
SLRmeas	measured SLR value
SLRnom	declared nominal SLR value
STMR	SideTone Masking Rating
STMRcorr	corrected STMR value
STMRmeas	measured STMR value
TBRL	Terminal Balance Return Loss
TCLw	weighted Terminal Coupling Loss
TDU	Transmission Decoupling Unit
TEI	Test Equipment Interface
TELR	Talker Echo Loudness Rating
TRP	Transmission Reference Point

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## 4 Compliance principles

All digital signal processing devices, which affect bit integrity of the 64 kbit/s speech-path within a digital PBX, e.g., digital loss or gain, low bit-rate coders, digital echo control devices etc., shall be rendered inoperative, when measuring the transmission parameters of the present document. However, if the NL or the SLR and RLR of a systems specific telephone set are implemented by a digital loss or gain, the parameters "Nominal value" and "Tolerance" of the relative levels for input and output connections and of the SLR and RLR, respectively shall be measured with digital loss or gain switched operative.

NOTE: In some digital PBXs such a digital loss or gain might be realized in a way, that it is not possible to switch this digital signal processing inoperative during measurement. However, several transmission parameters like quantizing distortion, variation of gain with input level etc., will be influenced additionally by digital signal processing. This means, the existing limits in the present document - derived only for the process of encoding/decoding - may not be met.

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## 5 Characteristics of analogue interfaces

The test conditions for analogue interfaces are described in annex A.

### 5.1 PBX input impedance of interfaces K2, L2, M2 and M4

The nominal value of the PBX impedance for 2-wire interfaces shall be:

$$Z_a = 270 \Omega + (750 \Omega \parallel 150 \text{ nF})$$

NOTE: The choice of this nominal value of the complex PBX impedance is providing a termination of:

- unloaded analogue subscriber line of a public exchange with reference to the interface K2;
- unloaded analogue lines between PBXs with reference to the interfaces M21 and M22 to ensure that the public network and every PBX will have adequate values of stability margin and echo.

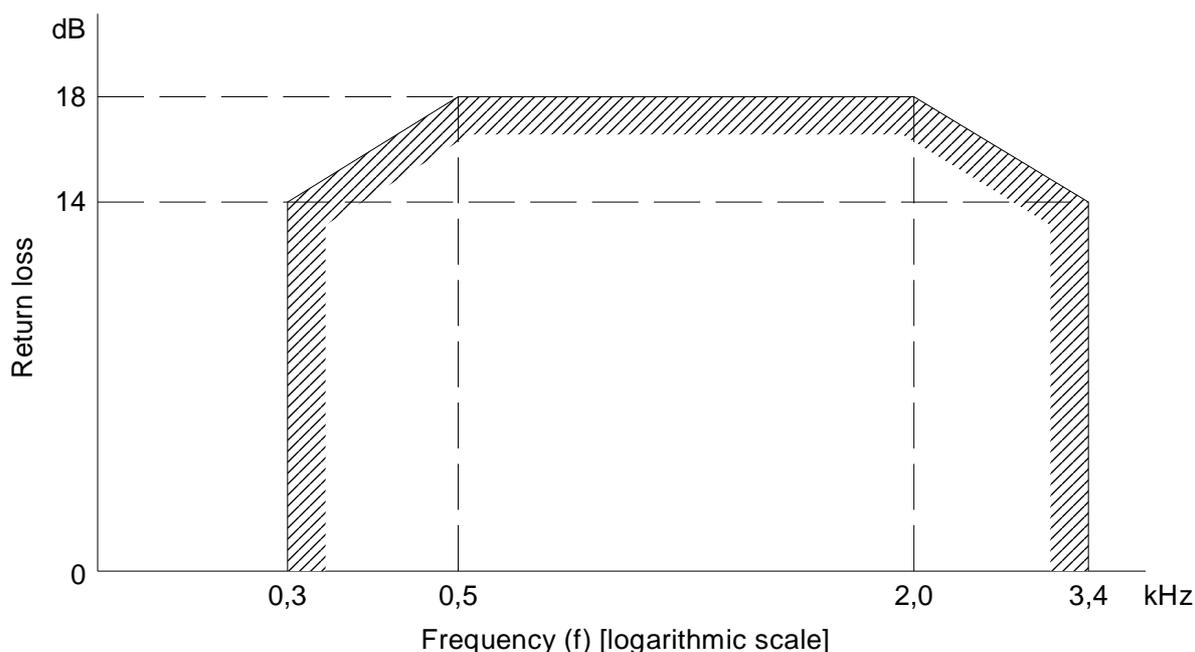
The choice of this nominal value for the complex PBX impedance also ensures an adequate sidetone performance for telephony terminals connected via analogue lines to the L2 interface, particularly those operated on short lines. This impedance will also be suitable for extension lines fitted with voice band modems.

The nominal value of the PBX impedance for M4 interfaces shall be:

$$Z_a = 600 \Omega$$

The return loss of the impedance presented by K2, L2, M2 and M4 interfaces against the nominal value for the PBX impedance shall comply with the limits given in figure 5.

Compliance shall be checked by the method described in subclause A.4.3.1.



**Figure 5: Minimum value of return loss against the nominal PBX impedance**

## 5.2 Transmission loss

### 5.2.1 Nominal transmission loss

The nominal input and output relative levels shall have a value stated by the supplier.

**NOTE:** It is understood as "good engineering practice" that the input and output relative levels - as stated by the supplier - are being derived from an overall transmission planning effort. Guidance on transmission planning can be found in EG 201 050 [1] and in ITU-T Recommendation G.108 [7]. Guidance on preferred ranges of relative levels can be found in ITU-Recommendations Q.552 [32] and Q.553 [33].

The difference between the measured value of the transmission loss, between the interface and the test point, and the nominal value of transmission loss ( $NL_i$  and  $NL_o$ ) calculated from the stated value of relative level, shall lie within the following ranges:

- input loss: -0,35 dB to +0,35 dB;
- output loss: -0,35 dB to +0,35 dB.

**NOTE:** These differences may arise, for example, from design tolerances and adjustment increments.

Compliance shall be checked by the methods described in subclauses A.4.2.1.1 and/or A.4.2.2.1.

### 5.2.2 Variation of gain with input level

With a sine-wave test signal at the reference frequency 1 020 Hz and at a level between -55 dBm0 and +3 dBm0, applied to the 2-wire or 4-wire analogue interface of any input connection, or with a digitally simulated sine-wave signal of the same characteristic applied to the PBX input test point  $T_i$  of any output connection, the gain variation of that connection, relative to the gain at an input level of -10 dBm0, shall lie within the limits given in figure 6.

Compliance shall be checked by the methods described in subclauses A.4.2.1.2 and/or A.4.2.2.2.

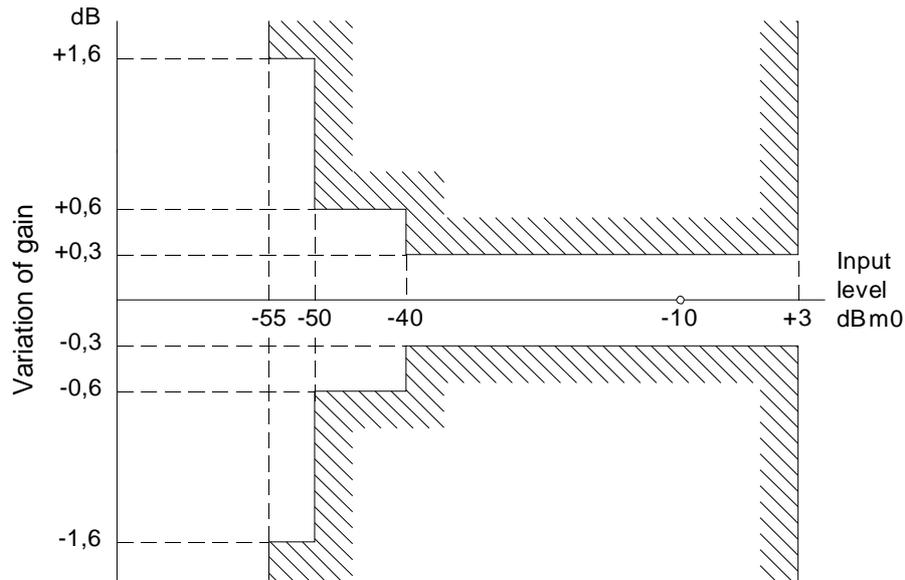


Figure 6: Variation of gain with input level

### 5.2.3 Loss distortion with frequency

The loss distortion with frequency of any input or output connection according to subclause 3.1.5 shall lie within the limits shown in the mask of figures 7 and 8, respectively. The preferred input level is -10 dBm0.

Compliance shall be checked by the methods described in subclauses A.4.2.1.3 and/or A.4.2.2.3.

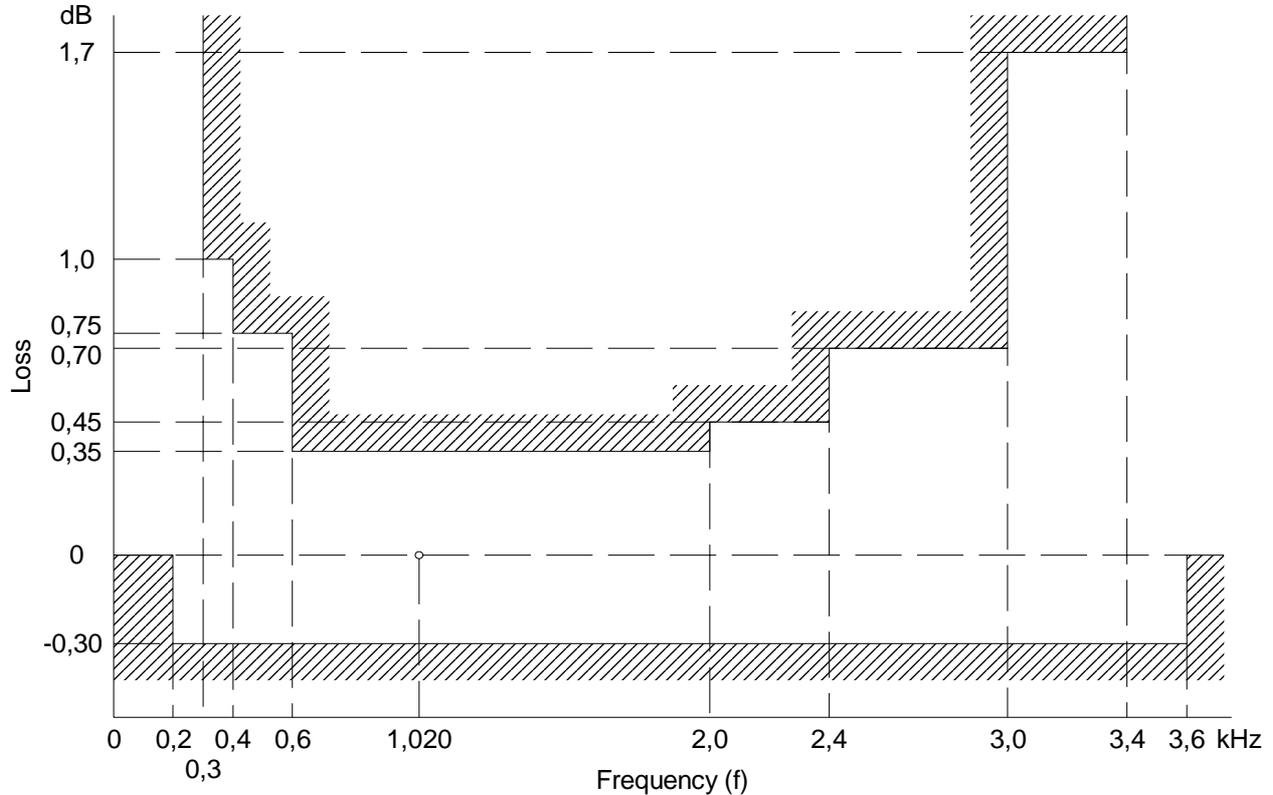
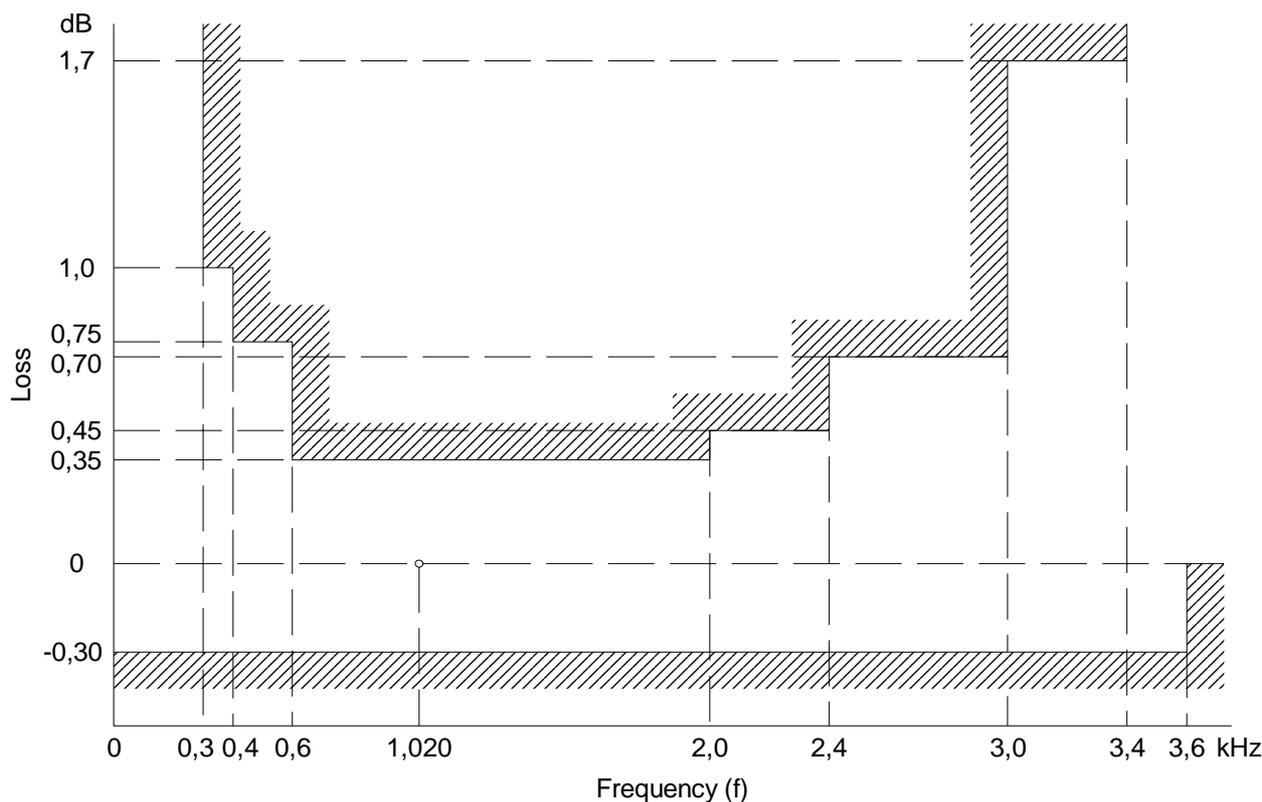


Figure 7: Loss distortion with frequency - input connection



**Figure 8: Loss distortion with frequency - output connection**

### 5.3 Group delay distortion

There are no requirements for group delay distortion.

### 5.4 Noise

**NOTE:** When evaluating the PBX noise characteristics, two components of noise should be considered. One of these arises from the Pulse Code Modulation (PCM) coding/decoding process, the other from analogue sources, e.g. signalling circuits, power supply, line power feeding on both sides of a connection between two interfaces through the same PBX.

Limits for the noise arising due to PCM encoding and decoding processes are given in ITU-T Recommendation G.712 [13] for all types of analogue interfaces. ITU-T Recommendation G.103 [5] considers the noise arising from analogue sources. Guidance on the combination of those two components is provided by and values for all types of interfaces are given in the Q.55x-series of ITU-T Recommendations, which is applicable to local exchanges as well as to PBXs.

#### 5.4.1 Weighted noise of interfaces without a feeding bridge

**NOTE:** For the calculation of these values, two components of noise should be considered: noise arising from the coding process and noise from the PBX power supply and other analogue sources transmitted through signalling circuits. ITU-T Recommendation Q.551 [31], annex A, provides further guidance on these issues.

The maximum values for overall weighted noise at the outputs of a half connection shall be:

Input connection:

- -65,2 dBm<sub>0p</sub>: For equipment with signalling on the speech wires;
- -67,0 dBm<sub>0p</sub>: For equipment with signalling on separate wires.

Output connection:

- -67,0 dBm0p: for equipment with signalling on the speech wires;
- -70,0 dBm0p: for equipment with signalling on separate wires.

Compliance shall be checked by the method described in subclause A.4.5.1.1 or A.4.5.1.2, respectively.

## 5.4.2 Weighted noise of interfaces with a feeding bridge

NOTE: For the calculation of noise, worst case conditions are assumed. The band limiting effect of the encoder on the noise has not been taken into account.

### 5.4.2.1 Output connection

NOTE: Two components of noise should be considered. One of these, (noise arising from the decoding process) is dependent upon the output relative level. The other (power supply noise from the feeding bridge) is independent of the output relative level. This latter component can be caused by the main DC power supply and auxiliary DC-DC converters. ITU-T Recommendation Q.551 [31], annex A, provides further guidance on these issues.

The total psophometric power allowed at an interface with a relative output level of  $L_o$  dB shall be:

$$P_{TNo} \leq P_{AN} + 10^{0,1(90+L_{INo}+L_o)} [pWp]$$

The total noise level shall be:

$$L_{TNo} \leq (10 \log \left| \frac{P_{TNo}}{1pW} \right| - 90) [dBmp]$$

where:

- $P_{TNo}$ : total weighted noise power for the output connection of the digital PBX;
- $P_{AN}$ : weighted noise power in pWp caused by analogue functions according to ITU-T Recommendation Q.551 [31], subclause 3.4, i.e. 200 pWp;
- $L_{INo}$ : receiving equipment noise (weighted) in dBm0p for PCM translating equipment according to ITU-T Recommendation Q.551 [31], subclause 3.4, i.e. -70 dBm0p;
- $L_o$ : output relative level in dBr of a half connection of a digital PBX
- $L_{TNo}$ : total weighted noise level for the output connection of the digital PBX.

EXAMPLE: Examples of the limits for different values of  $L_o$  are listed in table 1.

**Table 1: Examples of the limits for different values of  $L_o$**

$L_o$ [dBr]	$P_{TNo}$ [pWp]	$L_{TNo}$ [dBmp]
-5,0	231,6	-66,4
-6,0	225,1	-66,5
-7,0	220,0	-66,6

Compliance shall be checked by the method described in subclause A.4.5.1.2.

### 5.4.2.2 Input connection

NOTE: Two components of noise should be considered. One of these (noise arising from the encoding process) is dependent upon the input relative level. The other (power supply noise from the feeding bridge) shall be corrected by the input relative level for calculation at the PBX output test point  $T_o$ . ITU-T Recommendation Q.551 [31], annex A, provides further guidance on these issues.

The total psophometric power allowed at the PBX output test point  $T_o$  with a relative input level of  $L_i$  shall be:

$$P_{TNI} \leq P_{AN} * 10^{-0,1L_i} + 10^{0,1(90+L_{INI})} [pWOp]$$

and the total noise level shall be:

$$L_{TNI} \leq (10 \log \left| \frac{P_{TNI}}{1pW} \right| - 90) [dBmOp]$$

where:

- $P_{TNI}$ : total weighted noise power for the input connection of the digital PBX;
- $P_{AN}$ : weighted noise power in pWp caused by analogue functions according to ITU-T Recommendation Q.551 [31], subclause 3.4, i.e. 200 pWp;
- $L_{INI}$ : idle channel noise (weighted) in dBmOp for the input connection of a digital PBX according to ITU-T Recommendation Q.551 [31], subclause 3.4, i.e. -67 dBmOp;
- $L_i$ : input relative level in dBr of a half connection of a digital PBX;
- $L_{TNI}$ : total weighted noise level for the input connection of the digital PBX.

EXAMPLE: Examples of the limits for different values of  $L_o$  are listed in table 2.

**Table 2: Examples of the limits for different values of  $L_i$**

$L_i$ [dBr]	$P_{TNI}$ [pWOp]	$L_{TNI}$ [dBmOp]
0	399,5	-64,0
+1,0	358,4	-64,5
+2,0	325,7	-64,9

Compliance shall be checked by the method described in subclause A.4.5.1.1.

### 5.4.3 Single frequency noise of interfaces K2, L2, M2 and M4

The level of any unwanted single frequency (in particular the sampling frequency and its multiples), measured selectively with a bandwidth of 80 Hz in the frequency range from 4 kHz to 72 kHz at the interface of an output connection shall not exceed -50 dBm0.

NOTE: In this case "unwanted" refers to self generated noise such as feed-through of sampling frequencies and not to tones used for signalling or for normal traffic.

Compliance shall be checked by the method described in subclause A.5.1.4.

## 5.5 Crosstalk

A sine-wave test signal applied to an analogue interface of any input connection or a digitally simulated sine-wave test signal applied to PBX input test point  $T_i$  of any output connection, at the reference frequency of 1 020 Hz and at a level of 0 dBm0, shall not produce a level measured selectively in any other half connection (Near End Crosstalk (NEXT) and Far End Crosstalk (FEXT)) exceeding the corresponding values given in table 3.

**Table 3: Crosstalk requirements (NEXT, FEXT) by using a sending signal of 0 dBm0**

	Between L2 / L2 and L2 / K2	Between K2/K2	Between M4/M4 and 4-wire/2-wire
Input (FEXT)	-73 dBm0	-73 dBm0	-73 dBm0
Input (NEXT)	-73 dBm	-73 dBm	-73 dBm0
Output (FEXT)	-73 dBm	-73 dBm	-73 dBm0
Output (NEXT)	-73 dBm0	-66 dBm0	-73 dBm0

There are no requirements for crosstalk between the send and receive path (go-to-return) on a 4-wire interface.

Compliance shall be checked by the methods described under subclause A.4.4.

## 5.6 Total distortion including quantizing distortion

With a sine-wave test signal at the reference frequency of 1 020 Hz applied to the 2-wire interface of an input connection, or with a digitally simulated sine-wave signal of the same characteristic applied to the PBX input test point  $T_i$  of an output connection, the signal-to-total distortion ratio, measured at the corresponding outputs of the half connection with a proper noise weighting, specified in table 4 of ITU-T Recommendation G.223 [10], shall lie above the limits for the applicable interface given in subclause 5.6.1 or 5.6.2.

NOTE 1: The sinewave test signal is chosen to obtain results independent of the spectral content of the PBX noise.

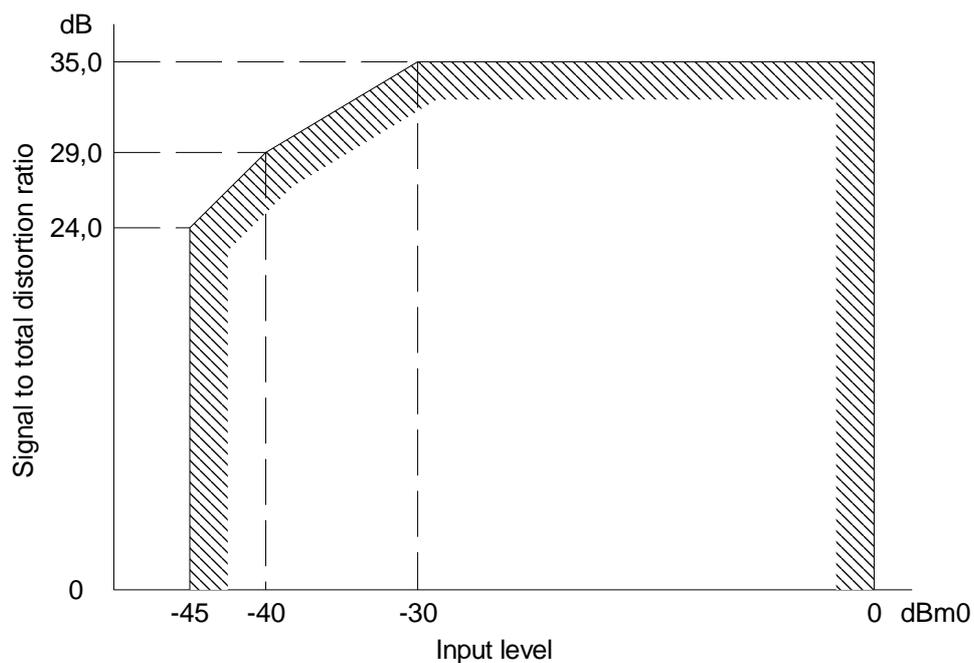
NOTE 2: These values include the limits for the encoding process and the allowance for the noise contributed via signalling circuits from the power supply and other analogue sources (e.g. analogue coupling). ITU-T Recommendation Q.551 [31], annex A, provides further guidance on these issues.

### 5.6.1 Values of total distortion of interfaces without a feeding bridge

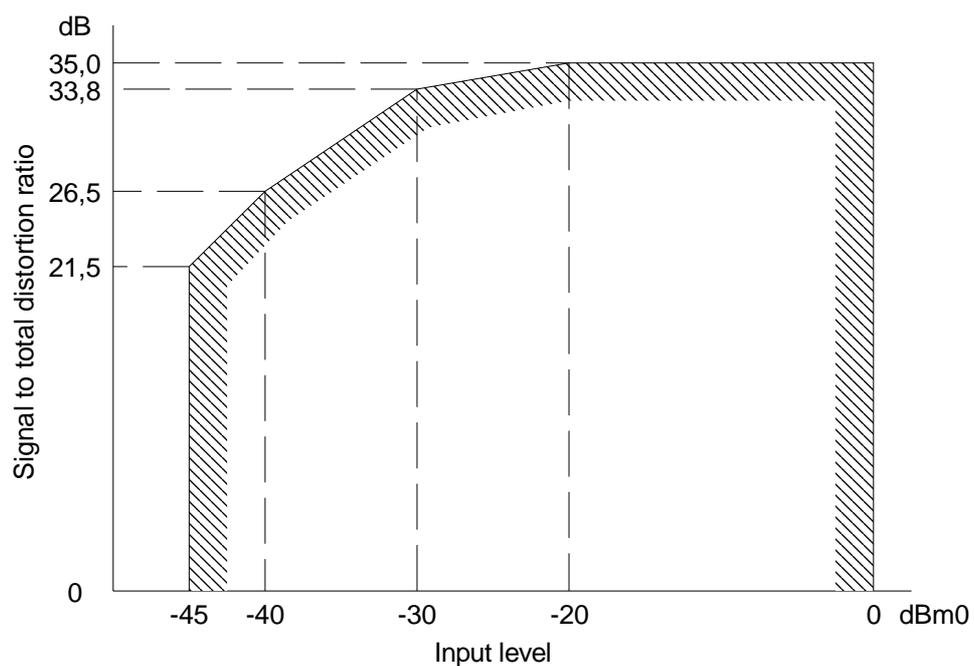
The signal-to-total distortion ratio for a half connection at interfaces without feeding bridges shall lie above the limits shown:

- in figure 9, for equipment with signalling on separate wires (some M21 interfaces, some M22 interfaces and some M4 interfaces);
- in figure 10, for equipment with signalling on the speech wires (all K2 interfaces and some M22 interfaces).

Compliance shall be checked by the methods described in subclauses A.4.2.1.4 and/or A.4.2.2.4.



**Figure 9: Limits for signal-to-total distortion ratio as a function of input level. Input or output connection. Signalling on separate wires without feeding bridge**



**Figure 10: Limits for signal to-total distortion ratio as a function of input level. Input or output connection. Signalling on the speech wires without feeding bridge**

## 5.6.2 Values of total distortion of interfaces with a feeding bridge

The signal-to-total distortion ratio required for a half connection at interfaces with feeding bridges shall be:

$$\frac{S}{N_T} \geq L_s + L_r - 10 \log(10^{0,1(L_s + L_r - \frac{S}{N})} + 2 * 10^{-7}) [dB]$$

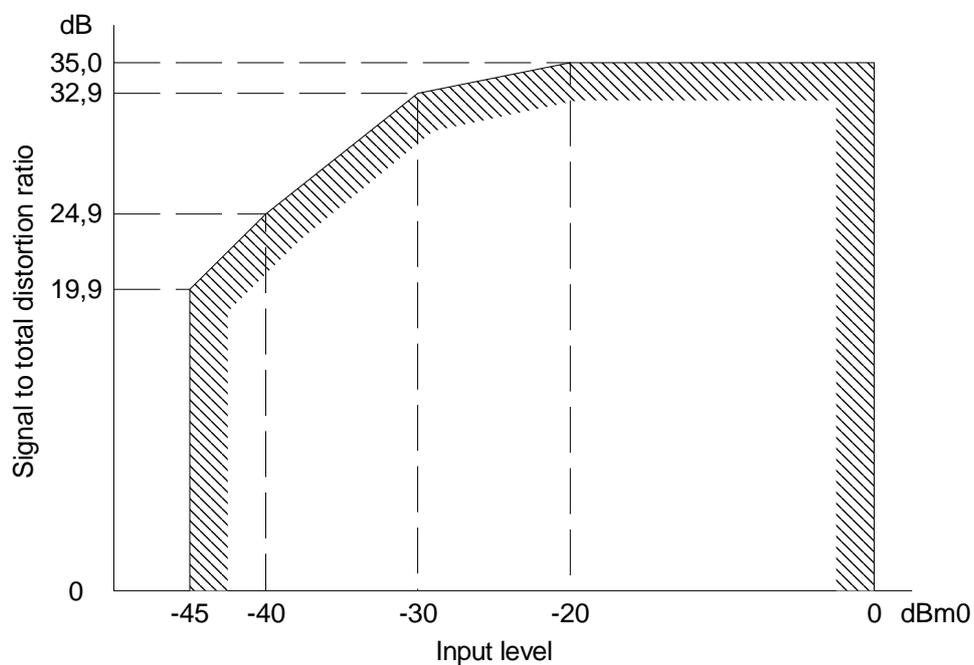
where:

- S/NT: resulting signal-to-total distortion ratio for input or output connections in digital PBXs;
- $L_s$ : signal level of the measuring signal in dBm0;
- $L_i$ : for input connections, input relative level  $L_i$  in dBr; for output connections, output relative level  $L_o$  in dBr;
- S/N: signal-to-total distortion ratio in dB given in figure 9 for the same value of  $L_s$ .

NOTE 1: As an example, one resulting template for an input connection and one for an output connection are shown in figures 11 and 12, respectively. The relative levels are assumed to be  $L_i = 0$  dBr and  $L_o = -7$  dBr.

NOTE 2: For an input connection the calculation above is assumed to be the worst case. No band limiting effect of the encoder on the noise was taken into account.

Compliance shall be checked by the methods described in subclauses A.4.2.1.4 and/or A.4.2.2.4.



**Figure 11: Limits for signal-to-total distortion ratio as a function of input level including analogue noise. Input connection ( $L_i = 0$  dBr). Interfaces L2 and M2 with feeding bridges**

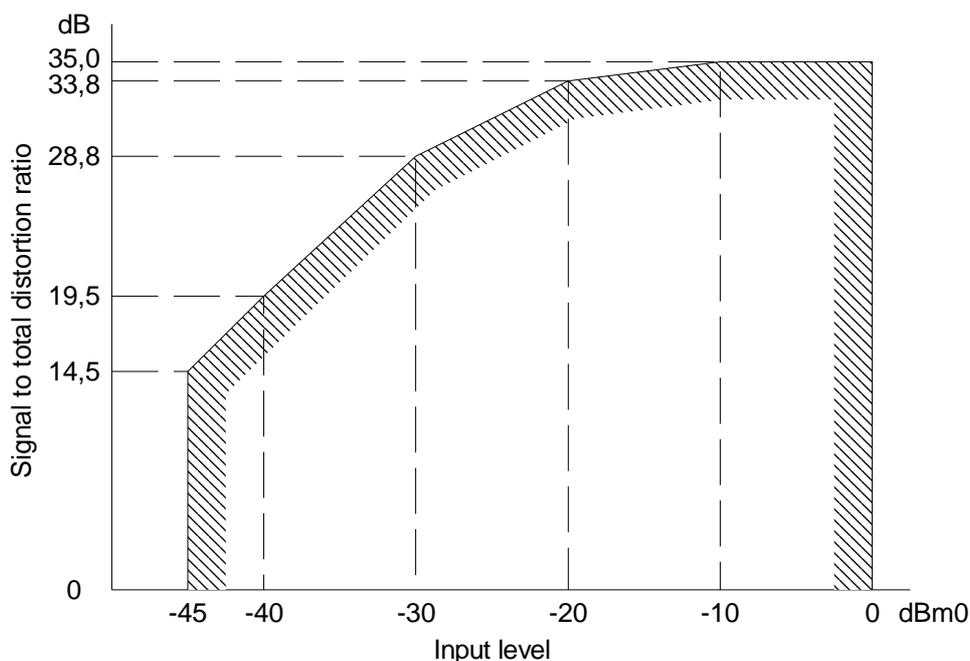


Figure 12: Limits for signal-to-total distortion ratio as a function of input level including analogue noise. Output connection ( $L_o = -7$  dBr). Interfaces L2 and M2 with feeding bridges

## 5.7 Discrimination against out-of-band signals applied to the K2, L2, M2 and M4 input interfaces

### 5.7.1 Input signals above 4,6 kHz

With a sine-wave signal in the range from 4,6 kHz to 72 kHz applied to the 2-wire and/or 4-wire interface of an input connection at a level of -25 dBm0, the level of any image frequency produced in the time slot corresponding to the input connection shall be at least 25 dB below the level of the test signal.

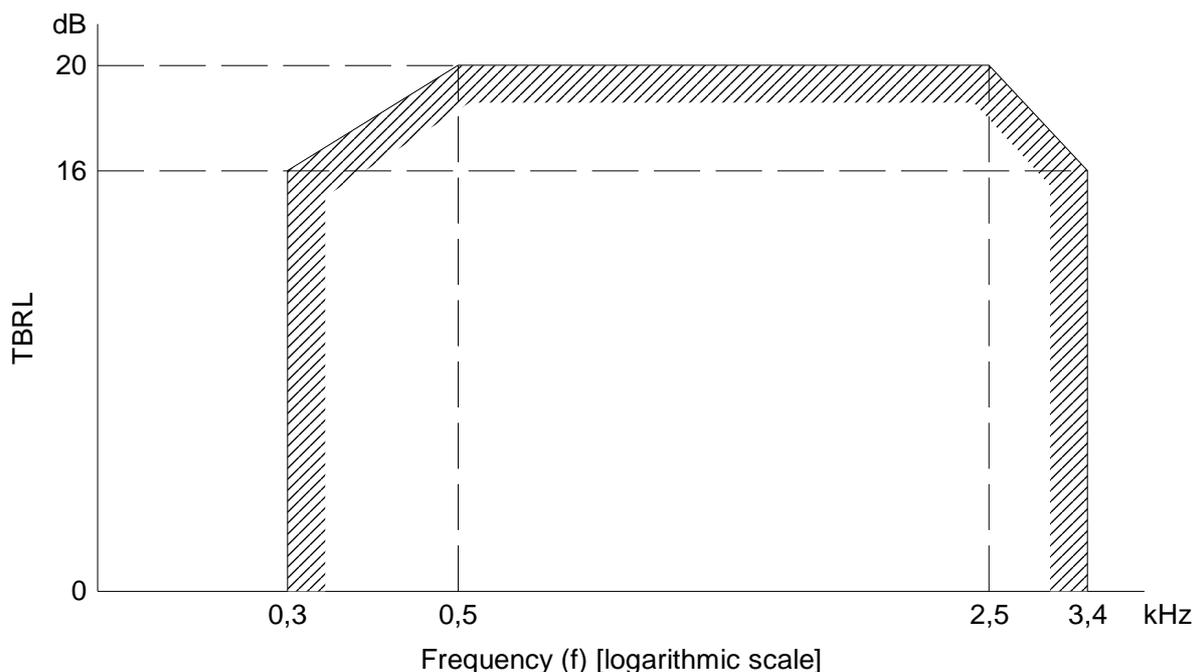
Compliance shall be checked by the methods described in subclause A.4.2.1.5.

## 5.8 Echo and stability of interfaces K2, L2 and M2

### 5.8.1 Terminal Balance Return Loss (TBRL)

Following the test procedure as given in subclause A.4.3.2 the TBRL, measured when terminating the 2-wire interface with the nominal value of the PBX impedance (see subclause 5.1), shall exceed the limits shown in figure 13.

NOTE: In special cases (e.g. very long lines, loaded lines, level controlled (by line feeding) telephone sets) it might be necessary to have special arrangements for the line balancing network and the test network.



**Figure 13: Limits for TBRL**

## 5.8.2 Stability loss

The stability loss measured according to subclause A.4.3.2 from the input test point to the output test point, with worst case terminating conditions, simulated by a short circuit on the 2-wire interfaces L2 or M21 shall be at least a value stated by the supplier at all frequencies in the range 200 Hz to 3 600 Hz.

Where the interface is designed for a minimum line length, a simulation of this line shall be present when terminating the interface during compliance test.

NOTE 1: In some PBXs the 4-wire speech path is not being closed during call set-up (i.e., while dialling or before the terminating equipment has answered the call), thus preventing the effects which may arise due to short-circuit and open-circuit termination conditions.

NOTE 2: Where the digital PBX is connected to the public digital exchange using a 4-wire line, the half connection of the digital PBX may provide the total stability loss of the entire path across the public network. The value of stability loss that is required for a 2-wire interface is a matter of national control provided that the requirements of ITU-T Recommendation G.122 [9] are met. A stability loss of 6 dB at all frequencies between 200 Hz and 3 600 Hz will ensure that the ITU-T Recommendation G.122 [9] requirements are met. However, a stability loss between 6 dB and 0 dB will formally comply with the requirements of ITU-T Recommendation G.122 [9] but further study is required to provide guidance in this area.

NOTE 3: In cases where the input impedance is not equal to the balance impedance (see note in subclause 5.8.1), the stability loss under short-circuit terminating conditions may result in lower values than in the case of equal impedances.

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# 6 Characteristics of digital interfaces

## 6.1 Coding law

The coding law of the digital interface shall be A-law according to ITU-T Recommendation G.711 [12].

## 6.2 Transmission loss

The NL of a digital half-connection shall have a value stated by the supplier.

NOTE 1: If there is a loss or gain between the interface and the test point, this is considered as SL as defined in subclause 3.1.4.2.

The difference between the measured value of the transmission loss and the stated NL shall lie within the ranges -0,15 dB to +0,15 dB, for input and output loss.

NOTE 2: These differences may apply when bit integrity is not preserved between interface and test point and may arise for example from design tolerances and adjustment increments, e.g. when the interface uses A-law coding and the test point uses  $\mu$ -law coding.

## 6.3 Bit sequence independence

No limitation should be imposed by the PBX on the number of consecutive binary ones or zeros or any other binary pattern within the 64 kbit/s paths through the PBX.

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# 7 Characteristics of system specific (non-analogue) MS interfaces

## 7.1 Equipment Impairment Factor, $I_e$

If the supplier has stated the coding scheme to be different from ITU-T Recommendation G.711 [12], the Equipment Impairment Factor  $I_e$  shall be stated by the supplier.

It is required that the value of the Equipment Impairment Factor  $I_e$  shall be:  $I_e \leq 20$ .

NOTE: For up to date information on  $I_e$  values for various codec types, Appendix I to ITU-T Recommendation G.113 [8] may provide guidance (Appendix I/G.113 [8] is intended to be updated regularly).

A compliance test for this requirement is for further study.

## 7.2 Transmission loss

The NL of a digital half-connection shall have a value stated by the supplier.

NOTE 1: If there is a loss or gain between the interface and the test point, this is considered as SL as defined in subclause 3.1.4.2.

The difference between the measured value of the transmission loss and the stated NL shall lie within the ranges -0,15 dB to +0,15 dB, for input and output loss.

NOTE 2: These differences may apply when bit integrity is not preserved between interface and test point and may arise for example from design tolerances and adjustment increments, e.g. when the interface uses proprietary coding and the test point uses A-law or  $\mu$ -law coding.

A compliance test for this requirement is for further study.

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## 8 System specific telephones (wired or cordless)

### 8.1 General

#### 8.1.1 Applicability of transmission characteristics

The transmission characteristics of system specific telephones (wired or cordless) apply between the acoustic reference points (Mouth Reference Point (MRP) and Ear Reference Point (ERP)) of the telephony terminal and the PBX digital test points, see figure 3. In cases where the PBX supplier does not provide the Portable Part (PP) of a cordless system but - solely - a standardized air interface the following transmission characteristics can be verified using a Reference Portable Part (RPP). If the transmission system between the telephony terminal and the PBX contains analogue elements, the requirements apply at zero line length between the telephony terminal and the PBX or at the minimum line length specified by the supplier where this is not equal to zero.

The requirements of clause 8 do not apply to telephony terminals connected to a L interface.

The supplier shall state the coding scheme used for the system specific telephony terminal. This information is required to determine the applicability of the following subclauses and for transmission planning. See ITU-T Recommendation G.113 [8] for further guidance.

If the supplier has stated that the coding scheme of the system specific telephone set is according to ITU-T Recommendation G.711 [12], with  $I_e = 0$ , the requirements of all subclauses in 8.2 except for 8.2.7.2 shall be applied.

If the supplier has stated that the coding scheme of the system specific telephone set is different from ITU-T Recommendation G.711 [12], with  $I_e > 0$ , the requirements of subclauses 8.2.7.2 shall be applied, only. The applicability of the remaining subclauses of 8.2 is for further study.

**NOTE:** It is assumed that - in modern PBXs - the interface between the system specific Telephone set and the PBX will be digital. System specific telephone sets often will - concerning the transmission technology - basically follow other standards (e.g., DECT). In such cases - preferably - the transmission requirements of that very standard should be applied between the acoustic interface of the system specific telephone set and the digital test points of the PBX. However, it should be recognized that the principle of supplier's declaration regarding the parameters delay, RLR and SLR as outlined in the present document shall be retained.

#### 8.1.2 Volume control

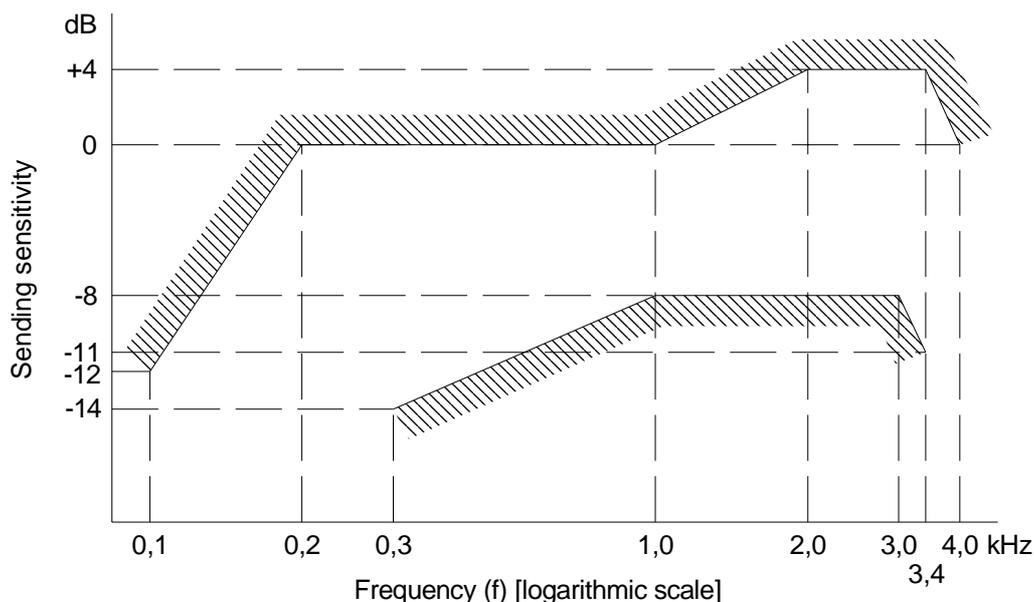
Unless stated otherwise, the requirements shall apply at the settings - controlled by the user - which are equal or closest to the declared nominal positions of the receive volume control.

## 8.2 Speech performance characteristics for 3,1 kHz handset telephones (wired or cordless)

### 8.2.1 Sensitivity - frequency response

#### 8.2.1.1 Send Sensitivity

The send sensitivity - frequency response (from the MRP to the output test point) shall be within the limits shown in figure 14. All sensitivity values are dB on an arbitrary scale.

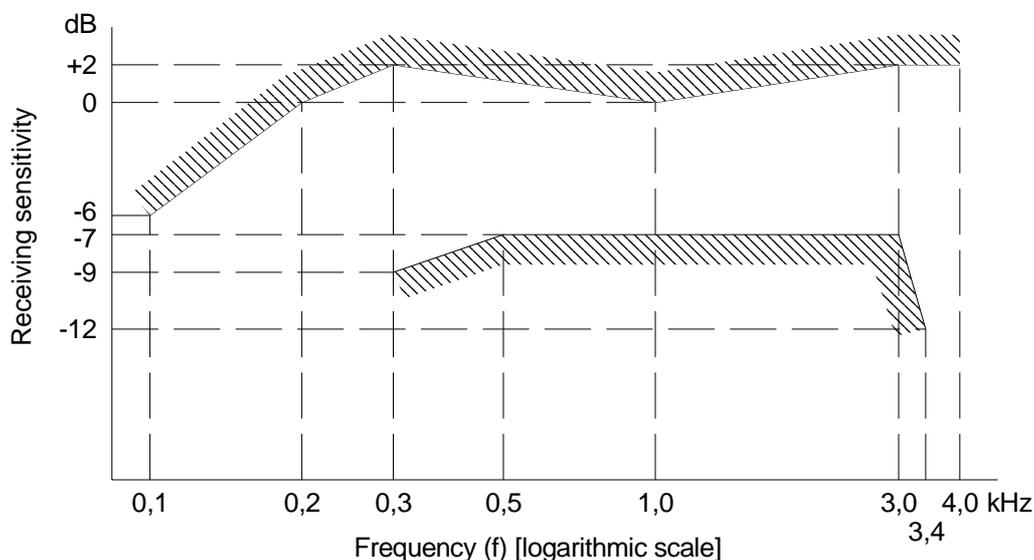


**Figure 14: Send sensitivity/frequency mask**

Compliance shall be checked by the methods described in subclause A.5.2.1.1.

### 8.2.1.2 Receive Sensitivity

The receive sensitivity - frequency response (from the input test point to the ERP) shall be within the limits shown in figure 15. All sensitivity values are dB on an arbitrary scale.



**Figure 15: Receive sensitivity/frequency mask**

Compliance shall be checked by the methods described in subclause A.5.2.1.2.

## 8.2.2 Send and Receive Loudness Ratings (SLR and RLR)

The supplier shall state the nominal values of SLR and RLR.

NOTE: It is understood as "good engineering practice" that the SLR and RLR - as stated by the supplier - are being derived from an overall transmission planning effort. Guidance on transmission planning can be found in EG 201 050 [1] and in ITU-T Recommendation G.108 [7].

The tolerances on SLR and RLR, including tolerances in the digital pads if present, are  $\pm 4,0$  dB.

Where a user-controlled receiving volume control is provided, the RLR shall meet the nominal value for at least one setting of the control.

Compliance shall be checked by the methods described in subclause A.5.2.2.

## 8.2.3 Sidetone

### 8.2.3.1 Talker sidetone

The value of the SideTone Masking Rating (STMR) shall be between 13 dB and 18 dB when the measured values are corrected to the declared nominal values for SLR and RLR (SLR<sub>nom</sub> and RLR<sub>nom</sub>), except for analogue system specific telephony terminals, where the value of the STMR shall be > 7 dB without correction.

For system specific cordless telephones the value of STMR shall be between 10 and 18 dB when the measured values are corrected in accordance to the declared nominal values for SLR and RLR (SLR<sub>nom</sub> and RLR<sub>nom</sub>).

NOTE: Correction to the nominal values can be calculated using the formula:

$$\text{STMR} = \text{STMR}_{\text{meas}} - (\text{SLR}_{\text{meas}} - \text{SLR}_{\text{nom}} + \text{RLR}_{\text{meas}} - \text{RLR}_{\text{nom}}).$$

Compliance shall be checked by the methods described in subclause A.5.2.3.1.

NOTE: For modern leak tolerant handset designs the STMR measurement may give different results when measured on a type 1 artificial ear as compared to traditional types of telephones not providing any built in acoustical leak. Such telephones in general should be measured on type 3.2, 3.3 or 3.4 artificial ears. ITU-T Recommendation P.79 [29] recognizes the differences and provides W-weights for unsealed conditions which should be used. This should be clearly stated in the related documentation. Further work is needed in order to verify the sidetone limits for such types of telephones.

### 8.2.3.2 Listener sidetone

The value of the Listener Side Tone Rating (LSTR) shall be not less than 13 dB when the measured values are corrected in accordance to the declared nominal values for SLR and RLR (SLR<sub>nom</sub> and RLR<sub>nom</sub>), except for system specific cordless telephony terminals.

For system specific cordless telephony terminals the value of the LSTR shall be not less than 10 dB and in case where noise rejection capabilities are declared by the supplier the LSTR shall be not less than 15 dB when the measured values are corrected with respect to the declared nominal values for SLR and RLR (SLR<sub>nom</sub> and RLR<sub>nom</sub>).

NOTE 1: Correction the nominal values can be calculated using the formula:

$$\text{LSTR} = \text{LSTR}_{\text{meas}} - (\text{SLR}_{\text{meas}} - \text{SLR}_{\text{nom}} + \text{RLR}_{\text{meas}} - \text{RLR}_{\text{nom}}).$$

NOTE 2: For modern leak tolerant handset designs the direct assessment of LSTR is not possible. This is the case as well for all measurements where type 3.x artificial ears are used. Under such conditions the LSTR only can be estimated by measuring the D-factor and using the estimation described in ITU-T Recommendation P.79 [29] formula E.1:

$$\text{LSTR} = \text{STMR} + \text{D}.$$

Alternatively if requested by the terminal supplier the value of the weighted average D (the difference of send sensitivities between diffuse and direct sound field) shall not be less than +2 dB. For system specific cordless telephony terminals the weighted average D shall not be less than -5 dB and with noise rejection not be less than 0 dB.

For 2-wire analogue system specific telephony terminals there is no requirement for LSTR and/or the value of the weighted average D (it is assumed that those terminals are equipped with traditionally shaped handsets).

Compliance shall be checked by the methods described in subclauses A.5.2.3.2 and A.5.2.3.3.

## 8.2.4 Echo Loss at the interface KD

The EL of the system specific telephony terminal shall be measured at the interface KD with a power weighting over the voice frequency band, in accordance with ITU-T Recommendation G.122 [9]. Echo can derive from one or more echo paths. Each echo path shall fulfil the requirements listed in table 4:

**Table 4: Required Echo Loss at the interface KD**

One-way delay of the echo-path	required Echo Loss	Remarks
< 5 ms	> 22 dB	
5-20 ms	> 30 dB	When there is (a) no echo-path with a one-way delay of less than 5 ms and (b) the EL of the path with a one-way delay of 5 .. 20 ms is in the range 30 .. 46 dB, then an Artificial EL of $24 \pm 2$ dB shall be inserted with a one way delay less than 5 ms from the interface KD.
> 20 ms	> 46 dB	

NOTE: The purpose of the Artificial EL is to ensure that an echo control device in an external network will work properly.

The manufacturer shall declare the number of echo paths, their associated one-way delay and the chosen solution.

Compliance shall be checked by the methods described in subclause A.5.2.4.

## 8.2.5 Talker Echo Loudness Rating (TELR)

The Talker Echo Loudness Rating (TELR) shall be measured at the acoustic interface of the system specific telephony terminal with a power weighting over the voice frequency band, in accordance with ITU-T Recommendation G.122 [9] to test the hybrids and the performance of the network echo control inside the PBX.

The correct working of the soft suppressor of cordless system specific telephones will not be tested.

The manufacturer shall declare the number of echo paths, their associated one way delay and the characteristics of the echo control device.

Each echo path shall fulfil the requirements. If echo paths cannot be separated by the stated test methods, because of too low delay difference between them, then the requirements stated for Case 1 shall apply for the sum of those echo paths.

Where a user-controlled receiving volume control is provided the TELR shall meet the requirements at the setting where the RLR is equal (or closest) to the nominal value.

NOTE: Correction to the nominal values can be calculated using the formula:

$$\text{TELR} = \text{TELR}_{\text{meas}} - (\text{SLR}_{\text{meas}} - \text{SLR}_{\text{nom}} + \text{RLR}_{\text{meas}} - \text{RLR}_{\text{nom}}).$$

Case 1: Connection to an interface KD:

Dependent on the one way delay of the echo path the TELR requirement is given in table 5.

**Table 5: Required Talker Echo Loudness Rating for a connection to an interface KD**

One way delay of echo path	TELRL
< 1,5 ms	covered by STMR, no additional requirements for TELRL
1,5 - 15 ms	> 24 dB
> 15 ms	> 48 dB

Compliance shall be checked by the methods described in subclause A.5.2.5 Case 1.

Case 2: Connection to an interface K2:

Dependent on the one way delay of the echo path the TELRL requirement is given in table 6.

**Table 6: Required Talker Echo Loudness Rating for a connection to an interface K2**

One way delay of echo path	TELRL
< 5 ms	covered by STMR, no additional requirements for TELRL
5 - 20 ms	> 24 dB
> 20 ms	> 48 dB

Compliance shall be checked by the methods described in subclause A.5.2.5 Case 2.

Case 3: Network echo control:

If the one way delay of the system specific telephone is > 5 ms the network echo shall be controlled by an echo device. The test network echo path has a delay (2-way) of 50 ms and a loss of 15 dB.

Dependent on the one way delay between the system specific telephony terminal and the interface K the TELRL requirement is given in table 7.

**Table 7: Required talker echo loudness rating for network echo control**

One way delay between system specific telephone and interface KD alt.K2	TELRL
5 - 20 ms	> 34 dB
> 20 ms	> 48 dB

Compliance shall be checked by the methods described in subclause A.5.2.5 Case 3.

## 8.2.6 Stability loss

The attenuation from the input test point to the output test point shall be at least a value stated by the supplier. This requirement applies at all frequencies in the range 200 Hz to 3 600 Hz with the handset lying on and the transducers facing a hard surface.

NOTE: See also subclause 9.5.

Compliance shall be checked by the methods described in subclause A.5.2.6.

## 8.2.7 Transmission impairments

### 8.2.7.1 Total Distortion, including Quantizing Distortion

The requirements in this subclause are only applicable if the supplier has stated the coding scheme to be in accordance with ITU-T Recommendation G.711 [12] and if the Equipment Impairment Factor,  $I_e = 0$ .

#### 8.2.7.1.1 Sending

The system specific telephony terminal shall meet the requirements of one of the subclauses 8.2.7.1.1.1 or 8.2.7.1.1.2.

##### 8.2.7.1.1.1 Method 1 (Pseudo random noise stimulus)

The test signal shall consist of a band-limited noise signal conforming to ITU-T Recommendation O.131 [20]. The ratio of signal-to-total distortion (harmonic and quantizing) power of the digitally encoded signal output by the system specific telephony terminal shall lie above the limits shown in figure 16 unless the sound pressure at the MRP is greater than +5 dBPa.

Compliance shall be checked by the methods described in subclause A.5.2.7.1.1.

##### 8.2.7.1.1.2 Method 2 (Sinewave test signal)

The test signal shall be a sine-wave with a frequency in the range 1 004 Hz to 1 025 Hz. The ratio of signal-to-total distortion (harmonic and quantizing) power of the digitally encoded signal output by the system specific telephony terminal, when passing through a noise weighting as specified in table 4 of ITU-T Recommendation G.223 [10], shall lie above the limits shown in figure 17 unless the sound pressure at the MRP is greater than +10 dBPa.

Compliance shall be checked by the methods described in subclause A.5.2.7.1.2.

#### 8.2.7.1.2 Receiving

The system specific telephony terminal shall meet the requirements of one of the subclauses 8.2.7.1.2.1 or 8.2.7.1.2.2.

##### 8.2.7.1.2.1 Method 1 (Pseudo random noise stimulus)

The test signal shall consist of a band-limited noise signal conforming to ITU-T Recommendation O.131 [20]. The ratio of signal-to-total distortion (harmonic and quantizing) power of the signal in the artificial ear shall lie above the limits shown in figure 18 unless the signal in the artificial ear is greater than +5 dBPa or is less than -50 dBPa.

Compliance shall be checked by the methods described in subclause A.5.2.7.2.1.

##### 8.2.7.1.2.2 Method 2 (Sinewave test signal)

The test signal shall be a sine-wave with a frequency in the range 1 004 Hz to 1 025 Hz. The ratio of signal-to-total distortion (harmonic and quantizing) power of the signal in the artificial ear, when passing through a noise weighting as specified in table 4 of ITU-T Recommendation G.223 [10], shall lie above the limits shown in figure 19 unless the signal in the artificial ear is greater than +10 dBPa or is less than -50 dBPa.

Compliance shall be checked by the methods described in subclause A.5.2.7.2.2.

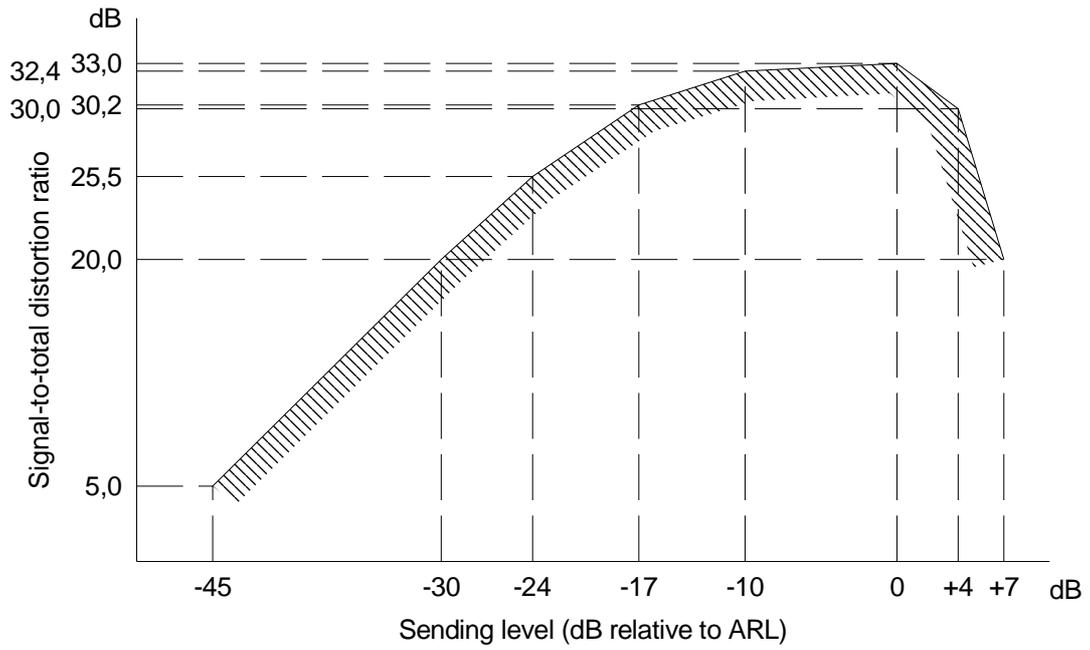


Figure 16: Limits of signal-to-distortion ratio, sending, method 1

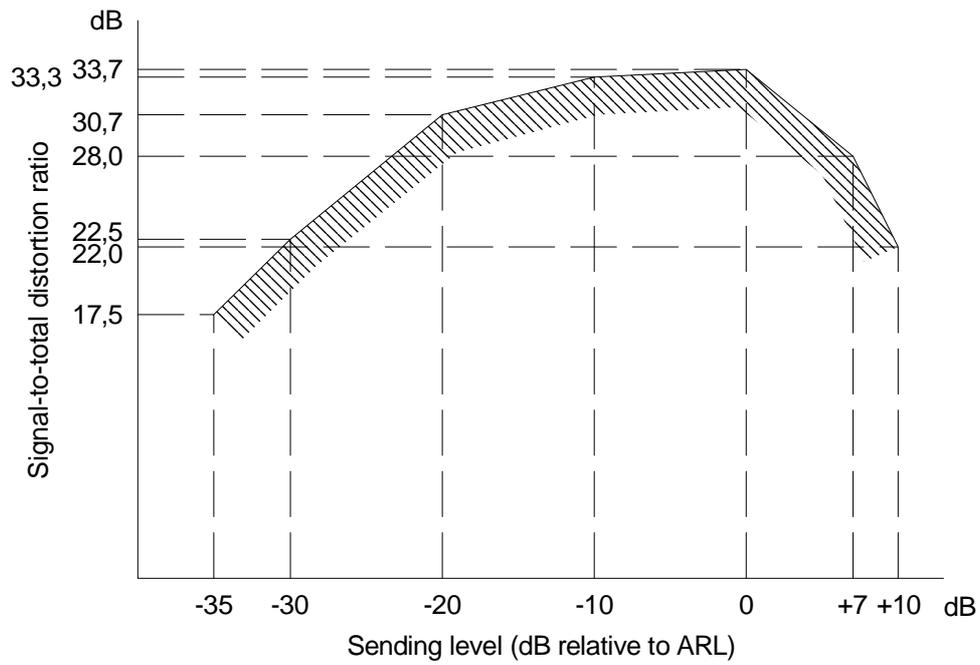
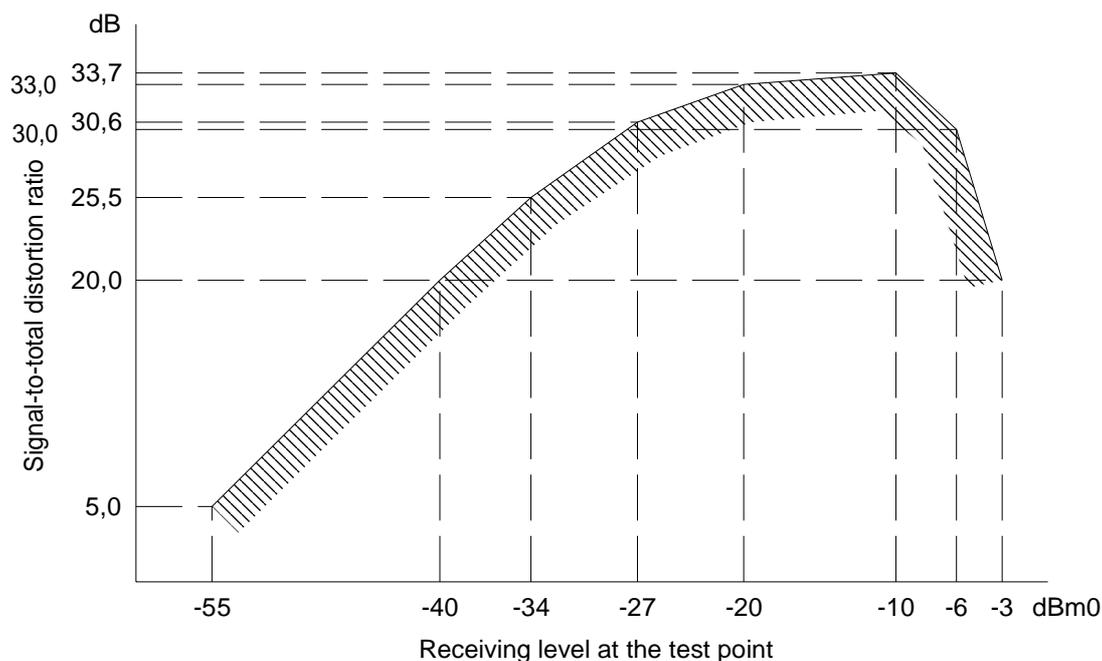
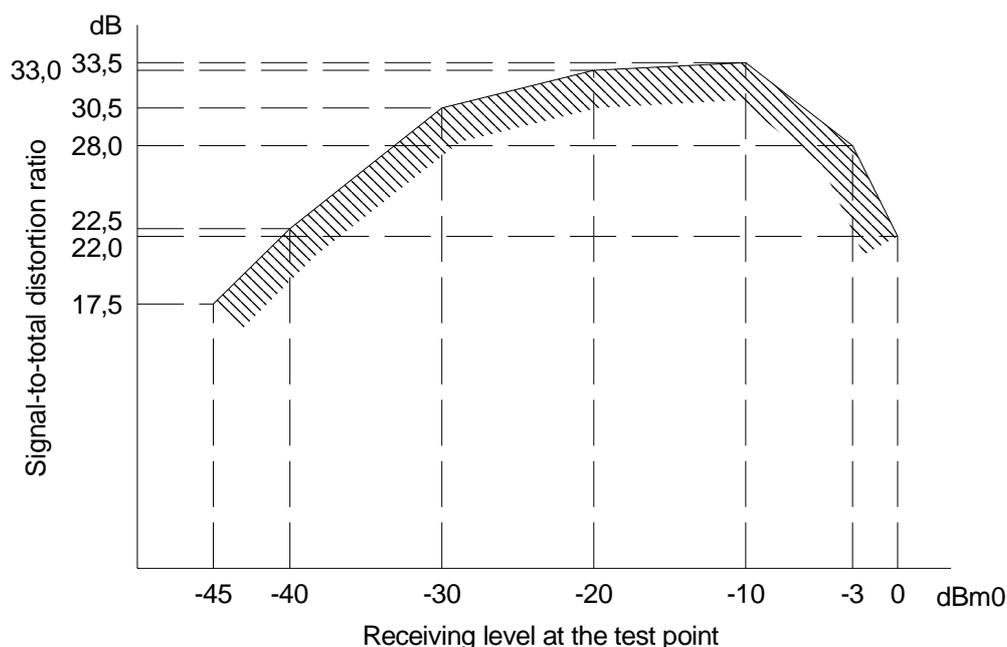


Figure 17: Limits for signal-to-distortion ratio, sending, method 2



**Figure 18: Limits of signal-to-distortion ratio, receiving, method 1**



**Figure 19: Limits for signal-to-distortion ratio, receiving, method 2**

### 8.2.7.1.3 Sidetone distortion

The third harmonic distortion generated by the system specific telephony terminal shall not be greater than 10 %.

Compliance shall be checked by the methods described in subclause A.5.2.7.3.

### 8.2.7.2 Equipment Impairment Factor, $I_e$

If the supplier has stated the coding scheme to be different from ITU-T Recommendation G.711 [12], the Equipment Impairment Factor  $I_e$  shall be stated by the supplier.

It is required that the value of the Equipment Impairment Factor  $I_e$  shall be:  $I_e \leq 20$ .

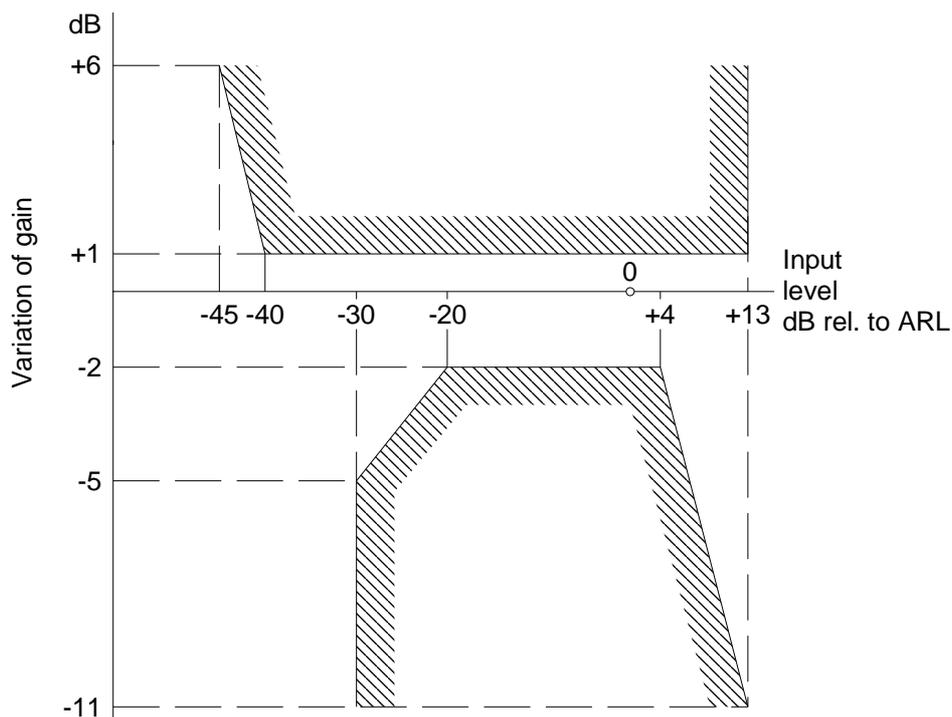
NOTE: For up to date information on  $I_e$  values for various codec types, Appendix I to ITU-T Recommendation G.113 [8] may provide guidance (Appendix I/G.113 [8] is intended to be updated regularly).

A compliance test for this requirement is for further study.

## 8.2.8 Variation of gain with input level

### 8.2.8.1 Sending

The gain variation relative to the gain for Acoustic Reference Level (ARL) shall be within the limits shown in figure 20. The test signal shall be a sine-wave with a frequency in the range 1 004 Hz to 1 025 Hz.

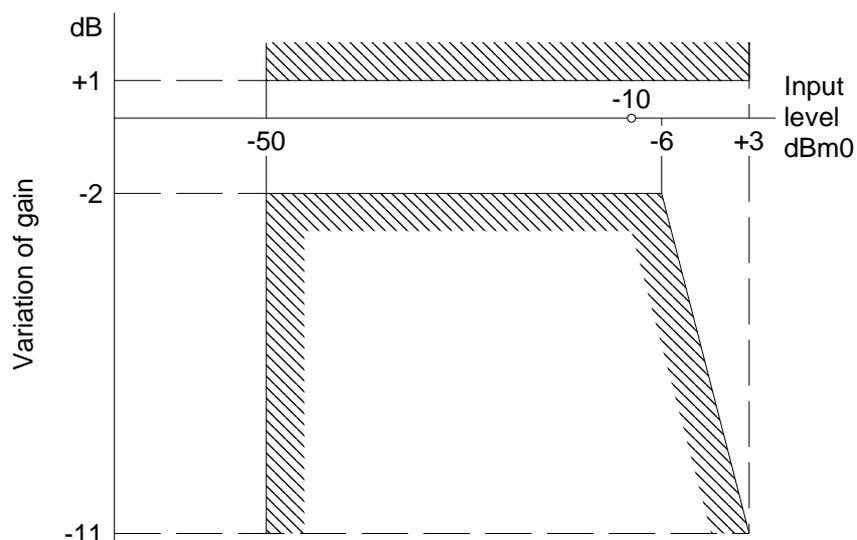


**Figure 20: Variation of gain with input level (sending)**

Compliance shall be checked by the methods described in subclause A.5.2.8.1.

### 8.2.8.2 Receiving

The gain variation relative to the gain at an input level of -10 dBm0 shall be within the limits shown in figure 21. The test signal shall be a sine-wave with a frequency in the range 1 004 Hz to 1 025 Hz.



**Figure 21: Variation of gain with input level (receiving)**

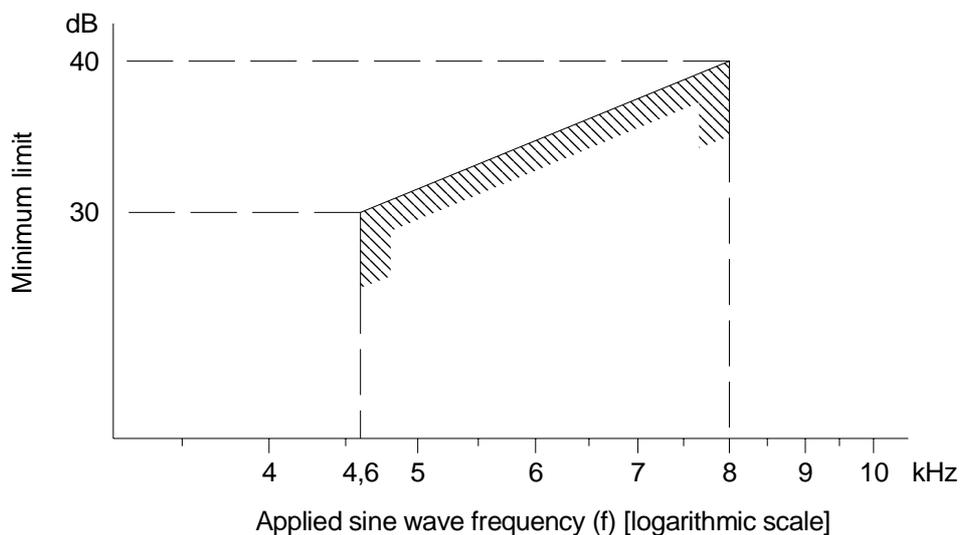
Compliance shall be checked by the methods described in subclause A.5.2.8.2.

## 8.2.9 Out-of-band signals

These requirements do not apply for the analogue (wired) system specific telephony terminal.

### 8.2.9.1 Discrimination against out-of-band input signals (sending)

With any sine-wave signal between 4,6 kHz and 8 kHz applied at the MRP at a level of -4,7 dBPa, the level of any image signal in the frequency range 300 Hz to 3,4 kHz produced at the output test point shall be less than a reference level obtained at 1 kHz (-4,7 dBPa at MRP) by at least the amount (in dB) described in figure 22.

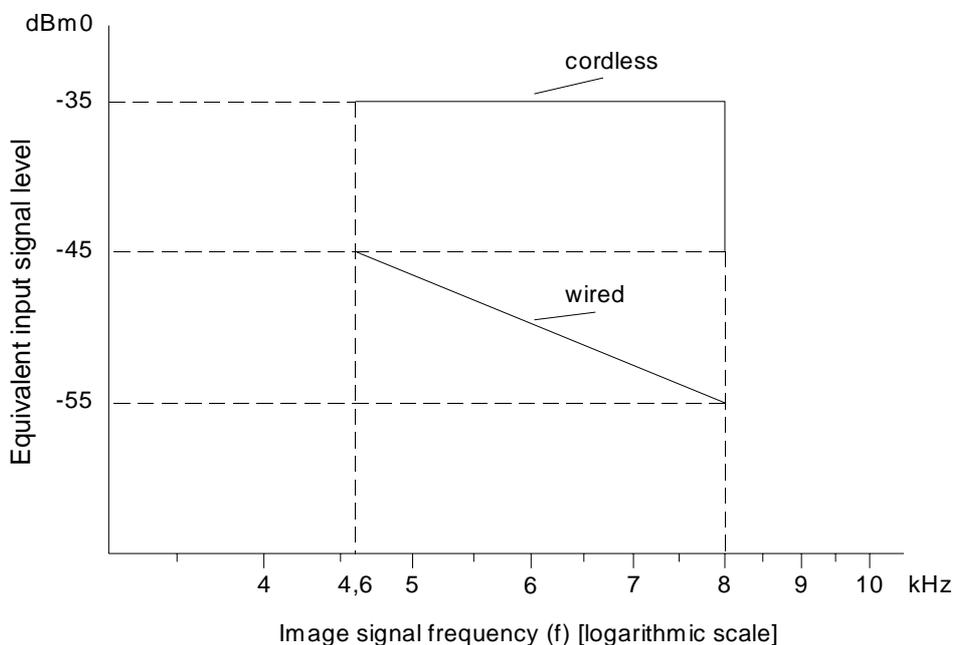


**Figure 22: Discrimination levels (sending)**

Compliance shall be checked by the methods described in subclause A.5.2.9.1.

### 8.2.9.2 Spurious out-of-band signals (receiving)

With a digitally simulated sine-wave signal in the frequency range of 300 Hz to 3,4 kHz and at a level of -10 dBm0 applied at the input test point, the level of spurious out-of-band image signals in the frequency range of 4,6 kHz to 8 kHz measured selectively in the artificial ear shall be less than the in-band acoustic level produced by a digital signal at 1 kHz set at the level described in figure 23 for wired or cordless system specific telephony terminals, respectively.



**Figure 23: Discrimination levels (receiving)**

Compliance shall be checked by the methods described in subclause A.5.2.9.2.

## 8.2.10 Noise

If the transmission system between the telephony terminal and the PBX contains analogue elements, the noise in sending and/or receiving direction shall not exceed a level which is 3 dB higher than the respective levels defined in subclauses 8.2.10.1 and 8.2.10.2.

### 8.2.10.1 Sending

The noise in the sending direction shall not exceed  $-(64 + \text{SLR}_{\text{nom}} - 7)$  dBm0p.

Compliance shall be checked by the methods described in subclause A.5.2.10.1.

### 8.2.10.2 Receiving

The noise in the artificial ear contributed by the receiving equipment alone shall not exceed -57 dBPa (A) when driven by a PCM signal corresponding to the decoder output value number 1.

Compliance shall be checked by the methods described in subclause A.5.2.10.2.

### 8.2.10.3 Level of sampling frequency (receiving)

The level of the sampling frequency (8 000 Hz) measured selectively in the artificial ear shall not exceed -70 dBPa.

This requirement does not apply for the analogue (wired) system specific telephony terminal.

Compliance shall be checked by the methods described in subclause A.5.2.10.3.

---

## 9 Characteristics for connections between two interfaces

### 9.1 General

Information about performance when interconnecting two interfaces applies only where this interconnection is intended, and when the interfaces are interconnected via the switch matrix. These interfaces can be electrical or acoustic interfaces.

NOTE: The information in this clause is mainly for the benefit of transmission planners.

### 9.2 Transmission loss between interfaces

The value of transmission loss between interfaces shall be stated by the supplier.

NOTE: In the case of system specific telephony terminals this includes also the values for SLR and RLR.

### 9.3 Quantizing distortion units (qdu)

For codecs complying to ITU-T Recommendation G.711 [12], the number of qdu should be stated by the supplier.

NOTE 1: The parameter qdu applies not only to A/D-D/A conversions but also to other processes influencing the digital bit-stream. Those processes are, for example, the insertion of digital loss or gain, signal addition in conference circuits, use of digital echo cancellers, etc. For coding laws other than A-law/ $\mu$ -law (e.g. according to ITU-T Recommendations G.726 [14], G.727 [15] or G.728 [16]), the parameter qdu has been replaced by the Equipment Impairment Factor,  $I_e$  (see subclause 9.4). See ITU-T Recommendation G.113 [8] for further guidance.

NOTE 2: The number of qdu is 1 between two analogue interfaces if no digital loss pad is introduced in the connection, or if the digital pad has a value equal to 6 dB ( $20 \cdot \log(2) = 6,02$  dB).

### 9.4 Equipment Impairment Factor, $I_e$

If the supplier has stated the coding scheme to be different from ITU-T Recommendation G.711 [12], the Equipment Impairment Factor  $I_e$  shall be stated by the supplier.

It is required that the value of the Equipment Impairment Factor  $I_e$  shall be:  $I_e \leq 20$ .

NOTE: For up to date information on  $I_e$  values for various codec types, Appendix I to ITU-T Recommendation G.113 [8] may provide guidance (Appendix I/G.113 [8] is intended to be updated regularly).

A compliance test for this requirement is for further study.

### 9.5 Mean one-way transmission time

The mean one way transmission time in a connection between two interfaces including the acoustic interfaces of system specific telephones shall be a value stated by the supplier.

## 9.6 Stability loss

### 9.6.1 Stability loss of interfaces connected to a KD interface

The nominal stability loss of connections to a KD interface shall be at least 6 dB at all frequencies in the range 200 Hz to 3 600 Hz, when measured from the input of the KD interface to the output of the KD interface. However, where the national transmission plan ensures that extra loss is added in the public network for international calls, the stability loss value in this clause shall be reduced by the value of such extra loss.

Termination of 2-wire interfaces connected to KD shall be as specified in subclause 5.8.2. Termination of a system specific telephony terminal interface connected to KD shall be as specified in subclause 8.2.5.

### 9.6.2 Stability loss of interfaces connected to M4, MD or MS interfaces

The nominal stability loss of connections to M4, MD or MS interfaces shall be at least 6 dB at all frequencies in the range 200 Hz to 3 600 Hz, when measured from the input of the M4, MD or MS interface to the output of the M4, MD or MS interface. Termination of 2-wire interfaces connected to M4, MD or MS shall be as specified in subclause 5.8.2. Termination of a system specific telephony terminal interface connected to M4, MD or MS shall be as specified in subclause 8.2.5.

Where the PBX is connected to transmission equipment there may be a need to adjust the relative levels of the M4 interface to such values that the stability loss of the PBX in question is less than 6 dB.

NOTE: In these cases the loss in the transmission system will ensure that the 6 dB stability margin is still met.

## Annex A (normative): Digital PBX transmission characteristic measurements

### A.1 General

#### A.1.1 Common measurement configurations

##### A.1.1.1 Operational conditions

There is a general rule, that all measurements of transmission characteristics shall be performed under nominal operating conditions, unless stated otherwise. This is mainly relevant to all 2-wire and 4-wire analogue interfaces involved in a connection. In many cases it is necessary that the test equipment includes additional auxiliary test equipment, to simulate nominal operating conditions e.g. DC-feed (see figure A.1). For more information, see clause A.3.

If test equipment are used to establish the test connections (e.g. signalling adapters) it shall be switched off after reaching the talking state or, where this is not possible, their influence on the test results shall be negligible.

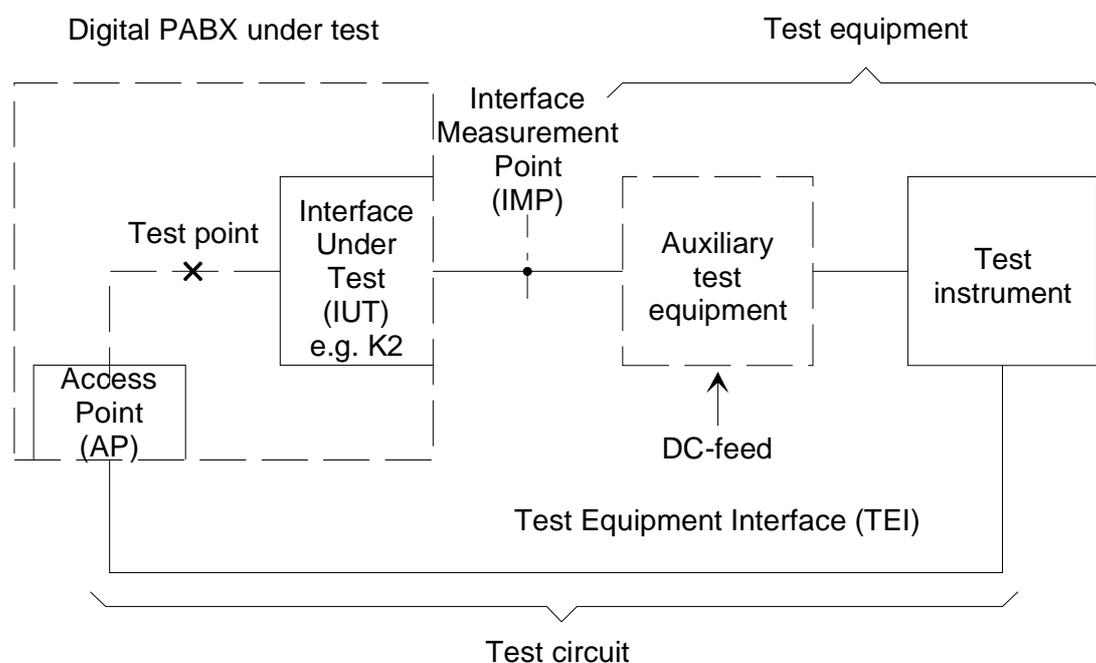


Figure A.1: Basic measurement configuration

#### A.1.2 Digital signal processing

All digital signal processing devices, which affect bit integrity of the 64 kbit/s speech-path within a digital PBX, e.g. digital loss or gain, digital echo control devices etc., shall be rendered inoperative, when measuring the transmission parameters of the present document. However, if the NL is implemented by a digital loss or gain, the parameters "Nominal value" and "Tolerance" of the relative levels for input and output connections shall be measured with digital loss or gain switched operative (see also clause 4).

If the supplier has stated the coding scheme of system specific circuitry to be different from ITU-T Recommendation G.711 [12] the measurements in this annex do not apply. In this case, the value of the Equipment Impairment Factor is  $I_e > 0$ , and appropriate compliance testing is for further study.

If sinewave measurements are not possible, e.g., due to the use of codecs in the transmission, appropriate test signals can be found in the ITU-T Recommendations P.50 [23], P.501 [30] and P.59 [27].

### A.1.3 Reference frequency

The reference frequency shall be 1 020 Hz for test frequency generating circuits or instruments, that provide reference test frequencies. The specified frequency tolerance shall be +2 Hz to -7 Hz.

### A.1.4 Impedance

Unless otherwise specified, measurements at analogue interfaces shall be made under matched conditions to the nominal impedance  $Z_r$  of the Interface Under Test (IUT). The interpretation of this statement is, that the nominal PBX impedance is used as the internal impedance of the test signal generator and the analogue level meter, i.e. test instruments with integrated test impedances.

NOTE: For more flexibility it may be preferable to use a low-impedance generator and a high-impedance meter in conjunction with a suitable external test impedance, which corresponds to an exact matching to the nominal PBX impedance.

### A.1.5 Measurement points

As far as analogue 2-wire or 4-wire interfaces are considered, the Interface Measurement Point (IMP) shall be at the first point of isolation as indicated by the PBX supplier, which provides testing access to the PBX and all external cabling. This means, that all cabling between this point and the interface card in the system, are included in the test results.

NOTE: For the test point used in conjunction with input/output-measurements and its access, see subclause 3.1.2.

### A.1.6 Test Instruments

For the choice of test instruments the following features shall be considered:

The test instrumentation consists of the following four functional units:

- an analogue signal generator A to apply test signals to the IMP of the PBX under test e.g. via an auxiliary test equipment (see also subclause A.1.5 and clause A.3). For more information, see subclause 3.2 of ITU-T Recommendation O.133 [22];
- an analogue signal analyser B to process received signals from the IMP of the PBX under test e.g. via an auxiliary test equipment (see also subclause A.1.5 and clause A.3). For more information, see subclause 3.3 of ITU-T Recommendation O.133 [22];
- a digital signal generator C to apply test-signals to the Access Point (AP) or the Test Equipment Interface (TEI) of the PBX under test (see also clause A.2). For more information, see subclause 3.4 of ITU-T Recommendation O.133 [22];
- a digital signal analyser D to process signals received from the AP or the TEI of the PBX under test (see also clause A.2). For more information, see subclause 3.5 of ITU-T Recommendation O.133 [22].

As a general objective the accuracy of the test instruments shall be an order of magnitude better than the relevant performance limits of the PBX under test.

In some cases it may not be possible to meet this objective due to technical and cost limitations.

For guidance to the capability and the accuracy of the test instrumentation refer to annex B.

## A.1.7 Test levels

At the reference frequency, test levels at analogue interfaces are defined in terms of apparent power relative to 1 mW.

Where no value is given, the test level shall be -10 dBm0. However, test levels may be restricted to a maximum absolute input and output power level as stated by the supplier.

At frequencies different from the reference frequency, test levels are defined as having the same voltage as the test level at the reference frequency. Measurements are based on the use of a test generator with a frequency independent electro motive force (emf).

## A.1.8 Disturbing effects

Where the digital input of the test point is not used, a quiet code shall be applied.

Measurements, which involve low output signal levels, or when measuring individual spectral components of a signal, shall be performed using frequency selective equipment. A bandwidth of 80 Hz is recommended.

## A.1.9 Alternative test methods

Laboratories may use other test methods provided they are equivalent to those specified in the present document.

Where the supplier requests other test methods as described in this annex the supplier shall provide sufficient information about how to perform such tests.

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# A.2 Test point and access to the test point

## A.2.1 Basic principle

In the present document, most of the parameters specified are for input half connections and output half connections. In these cases the parameters are referred to a "test point" as given in subclause 3.1.2.1 and figure 3. However, this is only a virtual point for specification purposes and might be considered as a "reference point".

For measurements, one or more specific AP shall be available to provide a suitable "path" between the test instrument and the test point. In this path, a part, or all of the switching network will be included. To ensure, that the influence on the results of this path is negligible, bit integrity is required.

NOTE: This physical access to the test point might be advantageous also for maintenance purposes. However, there is no obligation to provide AP on production systems in the field.

## A.2.2 Physical nature of test access

For measurement purposes, an AP shall be digital in its nature. To avoid additional adaptation equipment between AP and test instrument, the following interface types shall be used with the test access:

- 64 kbit/s co-directional, according to clause 1 of ITU-T Recommendation G.703 [11];
- 2 048 kbit/s, according to clause 6 of ITU-T Recommendation G.703 [11];
- 192 kbit/s, according to ITU-T Recommendation I.430 [17].

The synchronization of the test instrument from the digital PBX under test shall be ensured.

The coding law of the test point shall be either A-law or  $\mu$ -law according to ITU-T Recommendation G.711 [12].

NOTE: A-law is preferred.

## A.2.3 Set-up of test connections

Measurements of half connections are normally performed such that a complete bi-directional connection between the AP, via the test point (switching matrix) and the IUT is established.

The responsibility for the following measurement arrangements lies with the supplier:

- it shall be possible to measure all specified input and output parameters as given in the present document;
- this applies for all types of interfaces provided by the PBX such as K, L and M;
- as far as modifications of PBX configurations have an impact on the transmission parameters, each modified configuration shall be available for compliance testing.

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## A.3 Auxiliary test equipment

### A.3.1 General

As already mentioned in subclause A.1.1.2, measurements shall be performed as far as possible under nominal operating conditions. For this purpose, test feeding bridges in conjunction with a separate DC power supply and hold circuits are used at analogue interfaces, not only to keep the measured connection in the talking state, but also to provide a DC flowing, since the transmission characteristics of interfaces may vary with DC.

Furthermore, some modern test instruments (see subclause A.1.6) may only consist of an analogue or digital signal generator and signal receiver, but may not include additional bridge circuits as necessary, e.g. for return loss measurements. In those cases, external equipment shall be used in conjunction with the main PCM test instrument. Where artificial cables are included in the test circuit their characteristics shall be defined and standardized.

Every auxiliary test equipment which is part of the test circuit, shall have negligible influence on the test results.

**NOTE:** The values of inductances and capacitances used in auxiliary test equipment, may be sufficient for measurements with nominal input or test impedances of  $600\Omega$  resistive, but not for all capacitive complex impedances.

Considering all these facts, the following subclauses will give minimum requirements for all important auxiliary test equipment, to ensure, that their influence on the test results is negligible.

### A.3.2 DC power supply

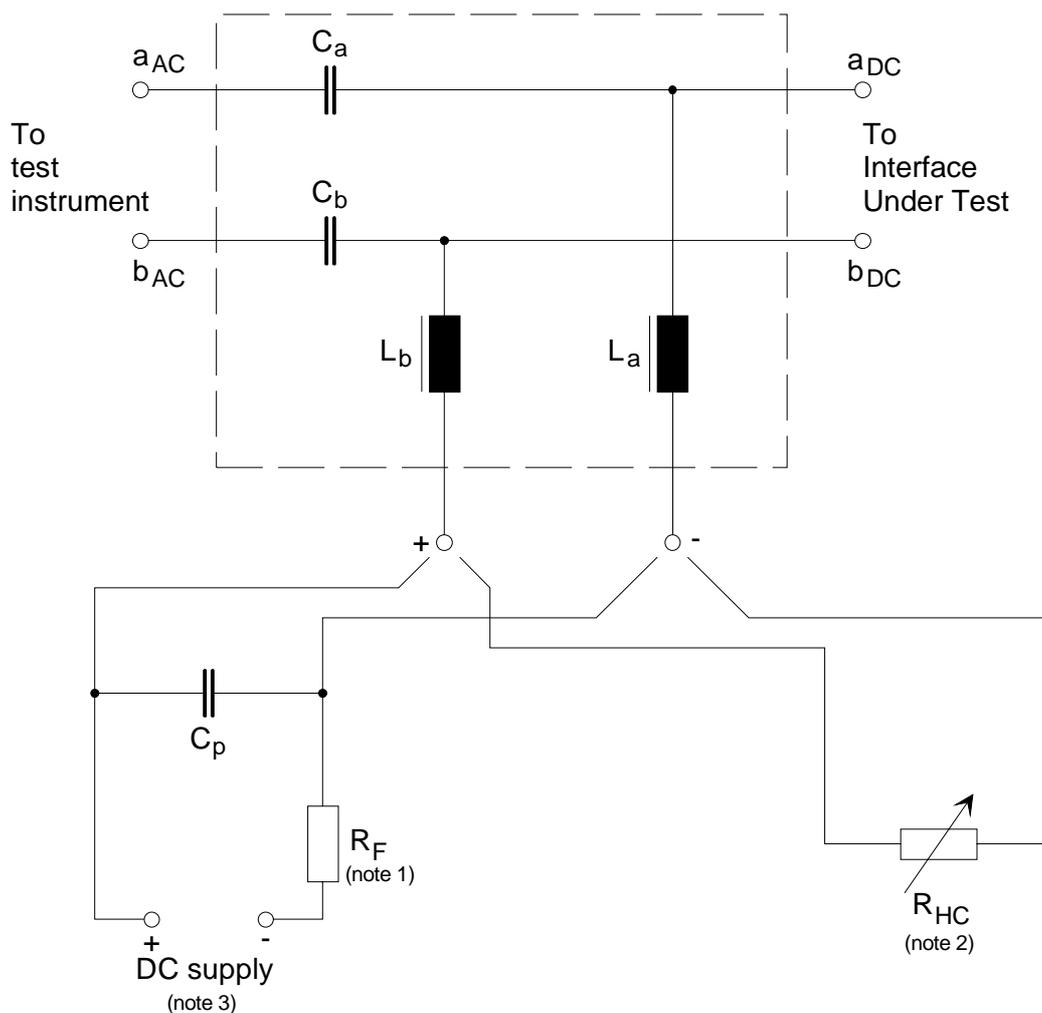
If DC power supply units are used in conjunction with a feeding bridge as part of the test circuit, any superimposed noise voltage shall have negligible influence on the test results. More information is given in the relevant subclauses of clause A.4.

### A.3.3 Transmission Decoupling Unit (TDU)

A TDU is used to either feed a DC into the appropriate analogue 2-wire or 4-wire point of the system under test, or to provide a DC loop. Where these assumptions do not apply there is no need to insert a TDU.

The basic circuit of a TDU is shown in figure A.2. The realization shall provide also a negligible influence when used in common mode configuration as necessary for impedance unbalance measurements, in conjunction with DC power supply which is connected to ground.

If TDUs with active elements are used, linearity over the full range of test signal level and the respective noise performance shall be taken into account.



NOTE 1: The value of the resistor  $R_F$  is the value quoted for the nominal resistance of the feeding arrangements being used. The actual value of  $R_F$  is adjusted to allow for the resistance value of inductors  $L_a$  and  $L_b$ .

NOTE 2: The variable resistor  $R_{HC}$  should be adjustable to give the required range of holding resistance.  $R_{HC}$  should allow for the resistances of inductors  $L_a$  and  $L_b$ .

NOTE 3: The DC supply should be such, that the full range of DC to be tested can be achieved. This could be by use of a low impedance DC voltage source in series with a variable resistor which replaces  $R_F$  or a variable constant current source.

**Figure A.2: Basic circuit diagram of a Transmission Decoupling Unit (TDU)**

The following characteristics of a TDU have to be considered as minimum requirements and shall be met over the full range of DC.

NOTE: Measurements of the following high values for a single TDU, mainly return loss and insertion loss requirements in the full DC range may be difficult or impossible. Therefore, it is recommended to connect two TDUs of the same type in a suitable configuration and perform the measurements including both TDUs. In this case, the requirements for insertion loss is 1,0 dB and 0,1 dB respectively and for return loss 6 dB less than the following values for a single TDU.

Return loss:	$\geq 33$ dB	in the range from	200 Hz	to	$< 500$ Hz
	$\geq 40$ dB	in the range from	500 Hz	to	$< 2\ 500$ Hz
	$\geq 33$ dB	in the range from	2 500 Hz	to	4 000 Hz

measured with reference to a capacitive complex impedance.

Insertion loss:	for	50 Hz	to	200 Hz < 0,5 dB
	for	200 Hz	to	4 000 Hz < 0,05 dB
	for	4 000 Hz	to	72 kHz < 0,5 dB

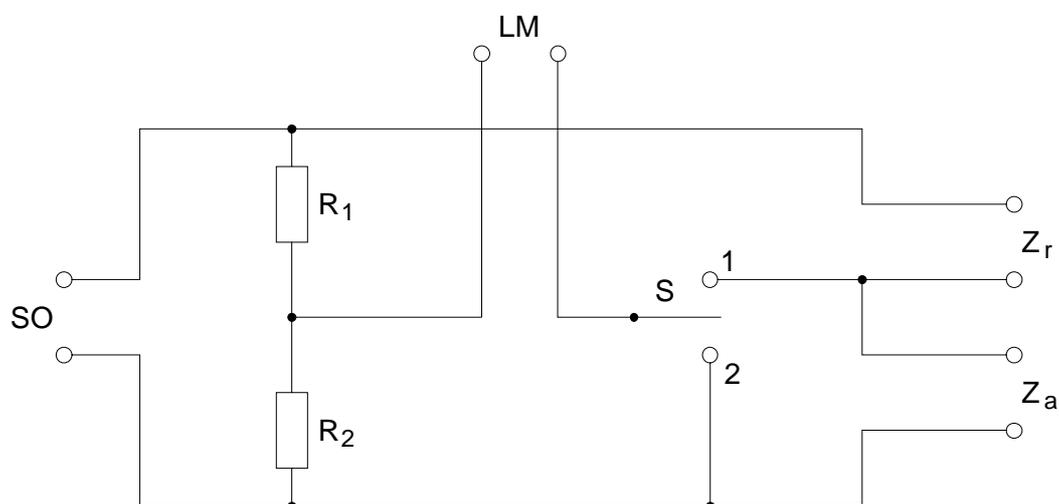
Together with its DC power supply which is connected to ground a TDU shall meet the following inherent balance requirements:

Inherent balance:	for	50 Hz	to	20 kHz: LCL and LCTL $\geq$ 60 dB
	for	200 Hz	to	3 400 Hz: LCL and LCTL $\geq$ 75 dB

measured according to figures 1 and 3 of ITU-T Recommendation O.9 [18], with respect to the bridged leads "+" and "-" of the TDU.

### A.3.4 External hybrid for return loss measurements

The hybrid shown in figure A.3 may be used for return loss measurements at 2-wire and 4-wire analogue ports.



- $R_1, R_2$  Resistors in the range from 100  $\Omega$  to 800  $\Omega$  (preferably 600  $\Omega$ ), matched to each other  $\leq$  0,2 %.
- S Switch (for the use of this switch see clause A.4).
- SO Sinewave oscillator, output balanced, earth free, low impedance:  $\leq$  10  $\Omega$ .
- LM Level meter, input balanced, earth free, high impedance  $\geq$  20 k $\Omega$ .
- $Z_r$  Connection point for reference impedance test network.
- $Z_a$  Connection point to item under test.

**Figure A.3: Return Loss measuring Hybrid (RLH)**

If the above mentioned values are met, then the inherent return loss in the frequency range from 200 Hz to 4 000 Hz of such an arrangement is more than 45 dB. For the purpose of testing the accuracy of such an equipment, values of 600  $\Omega \pm 0,1$  % each are recommended for  $Z_r$  and  $Z_a$ .

### A.3.5 Test Equipment Interface (TEI)

The interface of the test equipment connected to the digital IUT shall be capable of providing the signalling and supervision necessary for the PBX to be working in all test modes.

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## A.4 Specific measurements

### A.4.1 General guidance on measurement arrangements

In general, it is assumed in the following, that measurement set-ups are in accordance with state-of-the-art measurement technology.

DC paths as well as signalling procedures - as far as required to set up the test path - should be executed and terminated properly - according to manufacturer's specifications - thus not or negligible influencing the AC measurements.

In cases, where DC paths or inband signalling may impact the speech path under consideration it is advised to repeat the measurements for a reasonable number of times - in order to eliminate spurious effects.

When testing a 4-wire interface, the input or output connection which is not used in the measurement being carried out, shall be terminated in its nominal impedance  $Z_T$ .

### A.4.2 Analogue interfaces, half connection measurements

#### A.4.2.1 Input connections

##### A.4.2.1.1 Input transmission loss / input short-term variation of loss with time

- a) Connect the IMP and the AP as shown in figure A.6 for 2-wire interfaces and figure A.7 for 4-wire interfaces, where:

A = signal generator (sine-wave);

C = digital signal generator;

D = digital level measuring instrument.

- b) Set A at the IMP to provide the input level of - 10 dBm<sub>0</sub> as stated for the IUT at a frequency of 1 020 Hz.
- c) Measure the output level at the AP on D and record the value.

##### A.4.2.1.2 Input variation of gain with input level

- a) Connect the IMP and the AP as shown in figure A.6 for 2-wire interfaces and figure A.7 for 4-wire interfaces, where:

A = signal generator (sine-wave);

C = digital signal Generator;

D = digital level measuring instrument (frequency selective).

- b) Set A at the IMP to provide a representative series of input levels in the range specified in the present document at a frequency of 1 020 Hz.

Set C at the AP to input a quiet code (see subclause A.1.8).

NOTE: To avoid overloading the codec, it may be necessary to perform this test using the actual input relative level of the interface as required in subclause 5.2.

- c) Measure the output level at the AP on D and record the value for each input level used.

#### A.4.2.1.3 Input loss distortion with frequency

- a) Connect the IMP and the AP as shown in figure A.6 for 2-wire interfaces and figure A.7 for 4-wire interfaces, where:  
A = signal generator (sine-wave);  
C = digital signal generator;  
D = digital level measuring instrument.
- b) Set A at the IMP to provide the input level of -10 dBm<sub>0</sub> as stated for the IUT at a representative series of frequencies in the range specified in the present document. One of the frequencies used for measurement shall be the reference frequency 1 020 Hz.
- c) Measure the output levels at the AP on D and record the value for each input frequency used.

#### A.4.2.1.4 Input total distortion including quantizing distortion

- a) Connect the IMP and the AP as shown in figure A.6 for 2-wire interfaces and figure A.7 for 4-wire interfaces, where:  
A = signal generator (sine-wave);  
C = digital signal generator;  
D = digital level measuring instrument.  
  
A and D shall form part of the same instrument, which shall be capable of performing total distortion measurements.
- b) Set A at the IMP to provide a representative series of input levels in the range specified in the present document at a frequency of 1 020 Hz.  
  
Set C at the AP to input a quiet code (see subclause A.1.8).
- c) Measure the total distortion and record the value for each input level used.

#### A.4.2.1.5 Discrimination against out-of-band signals applied to the input interface

- a) Connect the IMP and the AP as shown in figure A.6 for 2-wire interfaces and figure A.7 for 4-wire interfaces, where:  
A = signal generator (sine-wave 4,6 kHz to 72 kHz);  
C = digital signal generator;  
D = digital level measuring instrument.
- b) Set A at the IMP to provide an input level of -25 dBm<sub>0</sub> as stated for the IUT at a representative series of frequencies in the range specified in the present document.  
  
Set C at the AP to input a quiet code (see subclause A.1.8).
- c) Measure the output levels at the AP on D and record the value for each input frequency used. If the result is less than 25 dB below the input level of the test signal when D is in the voice frequency bandwidth mode, then individual spectral frequency measurements shall be performed to determine compliance.

NOTE: See subclause A.1.8 for information on frequency selective measurements.

#### A.4.2.2 Output connections

For these connections, D is required to enable synchronization of the test apparatus.

#### A.4.2.2.1 Output transmission loss / output short-term variation of loss with time

- a) Connect the IMP and the AP as shown in figure A.8 for 2-wire interfaces and figure A.9 for 4-wire interfaces, where:
  - B = level measuring instrument;
  - C = digital signal generator;
  - D = digital level measuring instrument.
- b) Set C at the AP to provide the input level of -10 dBm<sub>0</sub> as stated for the IUT at a frequency of 1 020 Hz.
- c) Measure the output level at the IMP on B and record the value.

#### A.4.2.2.2 Output variation of gain with input level

- a) Connect the IMP and the AP as shown in figure A.8 for 2-wire interfaces and figure A.9 for 4-wire interfaces, where:
  - B = level measuring instrument (frequency selective);
  - C = digital signal generator;
  - D = digital level measuring instrument.
- b) Set C at the AP to provide a representative series of input levels in the range specified in the standard at a frequency of 1 020 Hz.
- c) Measure the output level at the IMP on B and record the value for each input level used.

#### A.4.2.2.3 Output loss distortion with frequency

- a) Connect the IMP and the AP as shown in figure A.8 for 2-wire interfaces and figure A.9 for 4-wire interfaces, where:
  - B = level measuring instrument;
  - C = digital signal generator;
  - D = digital level measuring instrument.
- b) Set C at the AP to provide an input level of -10 dBm<sub>0</sub> as stated for the IUT at a representative series of frequencies in the range specified in the present document. One of the frequencies used for measurement shall be the reference frequency 1 020 Hz.
- c) Measure the output level at the IMP on B and record the value for each input frequency.

#### A.4.2.2.4 Output total distortion including quantizing distortion

- a) Connect the IMP and the AP as shown in figure A.8 for 2-wire interfaces and figure A.9 for 4-wire interfaces, where:
  - B = level measuring instrument;
  - C = digital signal generator;
  - D = digital level measuring instrument.

C and B shall form part of the same instrument, which shall be capable of performing total distortion measurements.

- b) Set C at the AP to provide a representative series of input levels in the range specified in the present document at a frequency of 1 020 Hz.
- c) Measure the output total distortion and record the value for each level used.

## A.4.3 Analogue interfaces impedance measurements

### A.4.3.1 Return loss

Return loss may be determined by direct impedance measurements and calculation. Alternatively, return loss measuring hybrids as shown in figure A.3 may be used and the following measurement procedures carried out.

- a) Connect the IMP and the AP as shown in figure A.10 for 2-wire interfaces and figure A.11 for 4-wire interfaces, where:

- A = analogue signal generator (sine-wave, low impedance);
- B = level measuring instrument (high input impedance > 20 k $\Omega$ );
- C = digital signal generator;
- D = digital level measuring instrument;
- RLH = Return Loss Hybrid.

NOTE: The digital level measuring instrument D is required to enable synchronization of the test apparatus.

- b) Set C to input a quiet code.
- c) Connect the RLH to the IMP and terminate the leads  $Z_r$  of RLH with the respective value as stated in the standard for the IUT. Adjust the signal generator A to give an input level of -10 dBm<sub>0</sub> at SO at a frequency of 1 020 Hz.
- d) Operate S of RLH to position 2 and adjust the level meter B to give a 0 dB reading.
- e) Operate S of RLH to position 1.
- f) Read off the return losses at the specified frequencies.

Some test instruments are providing the RLH as an integral part with a direct readout of return loss values. In those cases the reference impedance  $Z_r$  shall be connected to the respective sockets of the instrument and steps c) to e) are not applicable.

- g) For 4-wire interfaces connect the RLH to the output IMP and  $Z_r$  to the input IMP, and repeat steps d) through f).

### A.4.3.2 TBRL, stability

The measurement configurations for TBRL and stability are nearly similar. They only differ in the used termination at the IMP. These measurements are only applicable to 2-wire interfaces.

- a) Connect the AP as shown in figure A.12 where:
- C = digital signal generator;
  - D = digital level measuring instrument.
- b) Terminate the IMP with the nominal test network as specified for this type of interface when performing TBRL measurements. Terminate the IMP with either open or short circuit when performing stability measurements.
- c) Set C at the AP to provide the input level of -10 dBm<sub>0</sub> as stated for the IUT at a representative series of frequencies in the range specified in the present document.
- d) Measure the output levels  $p_{out}$  at the AP on D the digital level measuring instrument. Calculate the TBRL using the formula:

$$TBRL = -p_{out} - L_i + L_o - 10 \quad [dB]$$

where  $L_i$  and  $L_o$  are the nominal relative input and output levels of the IUT.

Calculate the stability loss using the formula:

$$\text{stability loss} = -p_{\text{out}} - 10 \quad [\text{dB}]$$

- e) Record the result for each input frequency used.

## A.4.4 Analogue interfaces, crosstalk

Reference shall be made to "the interfering half connection" (which is defined as that half connection which has the test signal injected) and "the target half connection" (which is defined as the half connection at which the measurement is made).

When considering those interfaces which require to be assessed for crosstalk examination, the physical proximity and geographical relationship between interfaces shall be required. This shall be necessary to limit the number of combinations which are tested to acceptable levels.

To be able to carry out the crosstalk measurements access to two half connections at the same time shall be provided. Thus, if the AP is a single 64 kbit/s co-directional channel as mentioned in subclause A.2.2 (a), two such APs is required; if the AP is a multi-channel system as mentioned in subclause A.2.2 (b) and (c) two channels shall be capable of being used simultaneously.

Each access channel used shall be identified as Access Point Connection 1 (APC 1) and Access Point Connection 2 (APC 2), respectively.

The half connections used in the crosstalk measurements shall be set up to be in the conversational state.

Measurements shall be carried out by use of a frequency selective level measuring instrument.

### A.4.4.1 Input connections

#### A.4.4.1.1 Far End Crosstalk (FEXT)

- a) Having determined the interfaces which are to be used as the interfering half connection and as the target half connection, connect the IMPs and the APs as shown in figure A.13 for 2-wire interfaces, in figure A.14 for 4-wire interfaces and in figure A.15 for measurements between 4-wire and 2-wire interfaces, where:

$A_1, A_2$  = analogue signal generators (sine-wave);

$C_1, C_2$  = digital signal generators;

$D_1$  = digital level measuring instrument.

- b) Set  $A_1$  at the IMP of the target half connection, to provide a low-level activating signal.

NOTE 1: Suitable activating signals are, for example, a band limited noise signal (see ITU-T Recommendation O.131 [20]) at a level in the range -50 dBm0 to -60 dBm0 or a sine-wave signal at a level in the range -33 dBm0 to -40 dBm0.

NOTE 2: Care should be taken in the choice of frequency and the filtering characteristics of the measuring apparatus such that the activating signal does not significantly affect the accuracy of the crosstalk measurement.

- c) Set  $C_1$  and  $C_2$  at the APs to input a quiet code (see subclause A.1.8).
- d) Set  $A_2$  at the IMP of the interfering half connection, to provide a sine-wave test signal at the reference frequency of 1 020 Hz at a level of 0 dBm0.
- e) Measure the level of the 1 020 Hz sine-wave in  $D_1$  at the APC 1 of the target half connection, and record the value.

#### A.4.4.1.2 Near End Crosstalk (NEXT)

- a) Having determined the interfaces which are to be used as the interfering half connection and as the target half connection, connect the IMPs and the APs as shown in figure A.13 for 2-wire interfaces, in figure A.14 for 4-wire interfaces and in figure A.15 for measurements between 4-wire and 2-wire interfaces, where:

$A_2$  = analogue signal generator (sine-wave);

$B_1$  = analogue level measuring instrument;

$C_1, C_2$  = digital signal generators.

- b) Set  $C_1$  and  $C_2$  at the APs, to input a quiet code (see subclause A.1.8).
- c) Set  $A_2$  at the IMP of the interfering half connection, to provide a sine-wave test signal at the reference frequency of 1 020 Hz at a level of 0 dBm0.
- d) Measure the level of the 1 020 Hz sine-wave on  $B_1$  at the IMP of the target half connection, and record the value.

#### A.4.4.2 Output connections

##### A.4.4.2.1 Far End Crosstalk (FEXT)

- a) Having determined the interfaces which are to be used as the interfering half connection and as the target half connection, connect the IMPs and the APs as shown in figure A.13 for 2-wire interfaces, in figure A.14 for 4-wire interfaces and in figure A.15 for measurements between 4-wire and 2-wire interfaces, where:

$B_1$  = analogue level measuring instrument;

$C_1, C_2$  = digital signal generators.

- b) Set  $C_1$  at the APC 1 to input a quiet code (see subclause A.1.8).
- c) Set  $C_2$  at the APC 2 to provide a digitally simulated sine-wave test signal at the reference frequency 1 020 Hz at a level of 0 dBm0.
- d) Measure the level of the 1 020 Hz sine-wave on  $B_1$  at the IMP of the target half connection, and record the value.

##### A.4.4.2.2 Near End Crosstalk (NEXT)

- a) Having determined the interfaces which are to be used as the interfering half connection and as the target half connection, connect the IMPs and the APs as shown in figure A.13 for 2-wire interfaces, in figure A.14 for 4-wire interfaces and in figure A.15 for measurements between 4-wire and 2-wire interfaces, where:

$A_1$  = analogue signal generators (sine-wave);

$C_1, C_2$  = digital signal generators;

$D_1$  = digital level measuring instrument.

- b) Set  $A_1$  at the IMP of the target half connection, to provide a low-level activating signal.

NOTE 1: Suitable activating signals are, for example, a band limited noise signal (see ITU-T Recommendation O.131 [20]) at a level in the range -50 dBm0 to -60 dBm0 or a sine-wave signal at a level in the range -33 dBm0 to -40 dBm0.

NOTE 2: Care should be taken in the choice of frequency and the filtering characteristics of the measuring apparatus such that the activating signal does not significantly affect the accuracy of the crosstalk measurement.

- c) Set  $C_1$  at the APC 1 to input a quiet code (see subclause A.1.8).
- d) Set  $C_2$  at the APC 2 to provide a digitally simulated sine-wave test signal at the reference frequency 1 020 Hz at a level of 0 dBm0.

- e) Measure the level of the 1 020 Hz sine-wave on  $D_1$  at the APC 1 of the target half connection, and record the value.

## A.4.5 Analogue interfaces, noise measurements

### A.4.5.1 Weighted noise measurements

The method described here is concerned with the measurement of the total noise at analogue interfaces. The total noise is due to the noise generated by analogue sources, including the PBX power supply, together with noise arising from the encoding / decoding processes. The noise levels due to these sources are influenced by the design and complexity of the interfaces and by the relative levels employed.

PBXs employ a number of different types of interface and the relative levels of a particular interface may vary with the type of connection served. The resultant large number of possible interface connection combinations makes it difficult to carry out noise measurements on complete connections. Half connection measurements are therefore preferred, and in this case, the noise on both the analogue and digital sides of an interface shall be measured.

Measurements are made on the digital side of an interface (i.e. on an input connection) with a digital signal analyser. Analogue measurements on an output connection are made with an analogue signal analyser, which may be a simple psophometer which conforms to the Recommendations of ITU-T Recommendation O.41 [19]. The digital signal analyser selects a digital signal from any time slot and decodes it. In order to minimize errors the instrument's decoder shall conform to the "ideal" as described in ITU-T Recommendation G.711 [12].

The noise measurements are weighted psophometrically as described in ITU-T Recommendation O.41 [19]. The minimum noise measuring range shall be -80 dBmp to -20 dBmp.

Noise measurements shall be made with the interfaces terminated in impedances which match their output impedances. These impedances are usually complex and hence an impedance converter shall be connected between the terminated interface and the analogue signal analyser. The impedance converter shall present a very high input impedance to the interface and a very low output impedance to the analyser.

A TDU shall be used when interfaces are required to carry line current. The TDU is used to supply this current or, to provide a DC loop, as appropriate for the IUT. Adjustments to the internal components and / or to the TDU's power supply are made to provide the nominal line current before noise measurements are carried out.

#### A.4.5.1.1 Input connections

- a) Connect the IMP and the AP as shown in figure A.16 for 2-wire interfaces and figure A.17 for 4-wire interfaces, where:  
C = digital signal generator;  
D = digital signal analyser.
- b) Set C to apply a quiet code (see subclause A.1.8).
- c) Measure the weighted noise level on D and record the value.

#### A.4.5.1.2 Output connections

- a) Connect the IMP and the AP as shown in figure A.18 for 2-wire interfaces and figure A.19 for 4-wire interfaces, where:  
B = analogue signal analyser;  
C = digital signal generator;  
E = termination, appropriate to the type of digital test access interface used.
- b) Set C to apply a quiet code (see subclause A.1.8).
- c) Measure the weighted noise level on B and record the value.

The input and output relative levels of a measured interface shall be taken into account when assessing noise performance. Reference shall be made to subclause 5.4 of the present document to determine the permitted noise levels.

A significant amount of noise may be generated by the TDU, its associated power supply and by the impedance converter. The noise of the test circuit, including these auxiliary equipment, but without IUT shall be  $< -85$  dBm. When measuring the noise generated by the test circuit, the IUT shall be replaced by a resistor R with the same value as the input DC resistance of the IUT. The resistor R is used to establish the appropriate current in the TDU. The noise correction for the TDU alone may be determined by removing the impedance converter and observing the indicated noise across  $Z_T$  with B connected directly to the TDU's output terminals.

## A.5 Electro-acoustic measurements

### A.5.1 General measurement arrangement

All measurements including a system specific telephony terminal, are performed between the acoustic interface of the telephone handset and the digital test access point of the digital PBX under test. The telephony terminal is connected to its corresponding interface of the PBX and a connection is established between the telephony terminal under test and the test AP. The general test configuration valid for all electro-acoustic measurements in clause A.5 is shown in figure A.20.

All measured values shall, where applicable, be corrected to the nominal values of SLR and RLR as stated by the supplier.

Beside the general issues as given in clauses A.1 to A.3, some additional specifications, described in the following subclauses, shall be considered in conjunction with electro-acoustic measurements.

#### A.5.1.1 Electro-acoustic test equipment

The artificial ear shall conform to the ITU-T Recommendation P.57 [25].

If the LRGP Position according to ITU-T Recommendation P.64 [28] is used the artificial mouth shall conform to ITU-T Recommendation P.51 [24]. Alternatively the HATS position as described in ITU-T Recommendation P.64 [28] can be used. The artificial mouth shall conform with P.58 [26] when HATS is used, the artificial ear shall conform to ITU-T Recommendation P.57 [25], type 3.3 or type 3.4.

When using other than the type 1 artificial ear according to ITU-T Recommendation P.57 [25], the test results shall be corrected to ERP by the correction characteristic specified in ITU-T Recommendation P.57 [25]. When these artificial ears of type 3.2, 3.3 or 3.4 are used, no leakage correction shall be made in the calculations of RLR, SideTone Masking Rating (STMR) and LSTR (i.e.  $L_E = 0$ ).

The types of ears as well as the position used shall be stated in the test report.

#### A.5.1.2 Accuracy of test equipment

Unless specified otherwise, the accuracy of measurements made by test equipment shall be better than the values given in table A.1.

**Table A.1: Accuracy of measurements made by test equipment**

Item	Accuracy
Electrical signal power	$\pm 0,2$ dB for levels $> -50$ dBm
Electrical signal power	$\pm 0,4$ dB for levels $< -50$ dBm
Sound pressure	$\pm 0,7$ dB
Time	$\pm 5$ %
Frequency	$\pm 0,2$ %

Unless specified otherwise, the accuracy of the signals generated by the test equipment shall be better than the values given in table A.2.

**Table A.2: Accuracy of signals generated by test equipment**

Quantity	Accuracy
Sound pressure level at MRP	$\pm 1$ dB for 200 Hz to 4 kHz $\pm 3$ dB for 100 Hz to 200 Hz and 4 kHz to 8 kHz
Electrical excitation levels	$\pm 0,4$ dB (see note 1)
Frequency generation	$\pm 2$ % (see note 2)
NOTE 1: Across the whole frequency range.	
NOTE 2: When measuring sampled systems, it is advisable to avoid measuring at sub-multiples of the sampling frequency. There is a tolerance of $\pm 2$ % on the generated frequencies, which may be used to avoid this problem, except for 4 kHz where only the -2 % tolerance may be used.	

### A.5.1.3 Ideal codec approach and specification

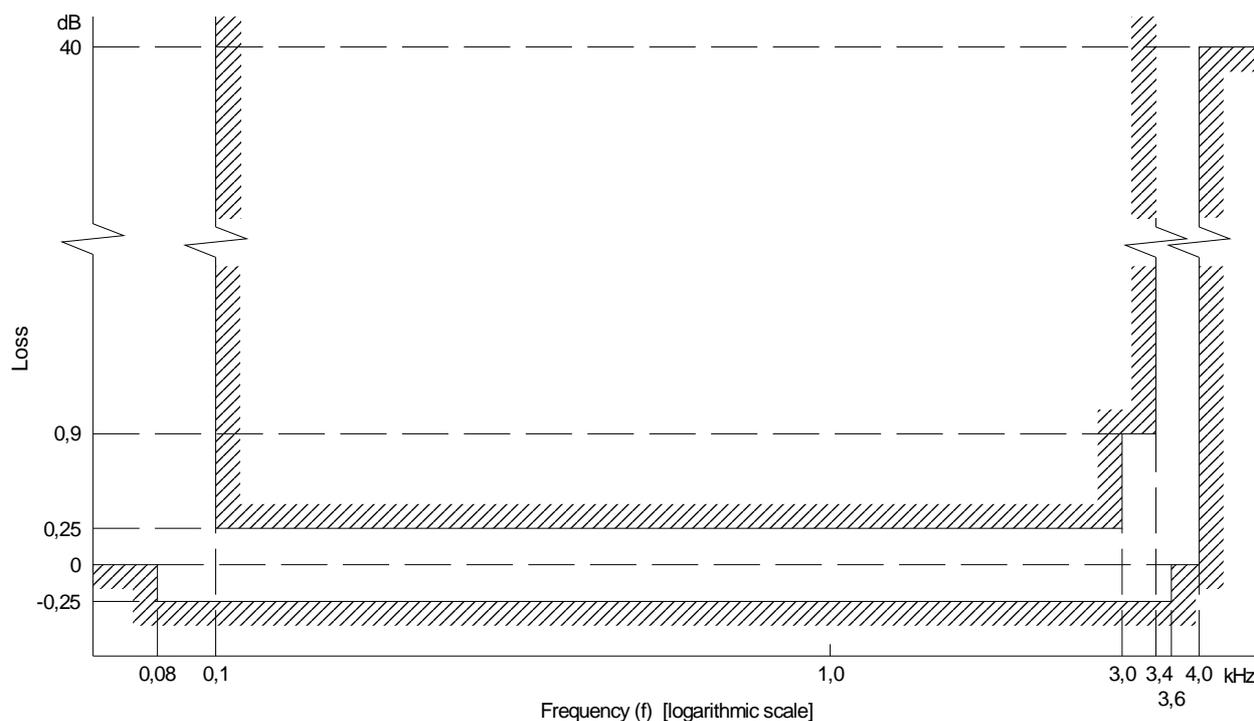
#### A.5.1.3.1 Codec approach

As an option, an ideal codec may be used to convert the digital input and output bitstream of the test access point to the equivalent analogue values, so that existing test procedures, mainly for electro-acoustic measurements and equipment, without the ability to generate or analyse digital signals, can be used. This codec shall be a high quality codec, whose characteristics are as close as possible to ideal. The specification for such a codec is given below.

#### A.5.1.3.2 Codec specification

A practical implementation of an ideal codec may be called a reference codec (see clause 4 of ITU-T Recommendation O.133 [22]). For the reference codec, characteristics such as attenuation/frequency distortion, idle channel noise, quantizing distortion, etc., shall be better than the requirements specified in ITU-T Recommendation G.712 [13], so as not to mask the corresponding parameters of the set under test. A suitable reference codec may be realized by using:

- at least 14 bit linear A / D and D / A converters of high quality and transcoding the output signal to the A-law PCM format;
- a filter response that meets the requirements of figure A.4.



**Figure A.4: Attenuation/frequency distortion of the sending or receiving sides of the reference codec**

**Definition of the analogue 0 dBr point:**

D / A converter: a Digital Test Sequence (DTS) representing the PCM equivalent of an analogue sinewave signal whose root mean square (rms) value is 3,14 dB (A-law) below the maximum full-load capacity of the codec, shall generate 0 dBm across a 600  $\Omega$  load;

A / D converter: a 0 dBm signal generated from a 600  $\Omega$  source, shall give the DTS representing the PCM equivalent of an analogue sinewave signal, whose rms value is 3,14 dB (A-law) below the maximum full-load capacity of the codec.

DTS is defined as a periodic sequence of character signals as defined in table 5 of ITU-T Recommendation G.711 [12].

NOTE: For further information, see figure 6 of ITU-T Recommendation G.101 [4].

**Analogue interface:** The output and input impedances, return loss and longitudinal conversion losses of the analogue interface of the reference codec shall be in accordance with subclause 3.1.1 of ITU-T Recommendation O.133 [22].

**Digital interface:** The fundamental requirements for the reference codec digital interface are given in the appropriate ITU-T Recommendations (e.g., ITU-T Recommendation G.703 [11]).

### A.5.1.4 Selective measurements

It shall be the responsibility of the test house to select an appropriate bandwidth for selective measurements.

For single frequency noise measurements the procedures of subclauses A.4.5.1.1 and A.4.5.1.2 are followed with the digital and analogue signal analysers in the frequency selective mode. Both in-band and out-of-band single frequency noise components may then be measured.

### A.5.1.5 Use of digital loss or gain pads

According to the rules given in clause 4, the use of digital loss or gain pads in the speech path shall be stated by the supplier. If the pads are included in the path between test point of the PBX and system specific telephony terminal, these pads shall be switched inoperative during all transmission measurement, with the exception of:

- SLR (see subclause A.5.2.2.1);
- RLR (see subclause A.5.2.2.2);
- Echo Loss (see subclause A.5.2.4);
- TELR (see subclause A.5.2.5);
- Stability loss (see subclause A.5.2.6).

Basically all transmission measurements in conjunction with a system specific telephony terminal, are performed only up to the test point of the PBX. If digital pads are included in the path between test point and the interface KD of the PBX (to be stated by the supplier), test results of SLR, RLR, EL and stability loss shall be corrected with the nominal values of the digital loss or gain pads in both transmission directions.

### A.5.1.6 Use of echo control devices

If the supplier declares that an echo control device is needed in order to meet the requirements of the present document it shall be switched operative in all cases if not stated otherwise.

### A.5.1.7 Use of a Reference Portable Part (RPP)

In cases where the PBX supplier does not provide the PP of a cordless system but - solely - a standardized air interface the transmission characteristics can be verified using a RPP.

The RPP shall provide the equivalent of true air interface measurements and therefore shall not contain circuitry which will modify the true air interface speech frequency performance. For measurement purposes, the RPP shall have a test access point as specified in relevant standards.

## A.5.2 Specific electro-acoustic measurements

### A.5.2.1 Sensitivity - frequency response

#### A.5.2.1.1 Sending Sensitivity

- a) The handset is mounted in the Loudness Rating Guard ring Position (LRGP) (see ITU-T Recommendation P.64 [28]). The earpiece is sealed to the knife-edge of an artificial ear. Alternatively the HATS position (see ITU-T Recommendation P.64 [28]) can be used. The pressure force used for handset application shall be indicated in the test report.
- b) A sinewave signal with a sound pressure level of -4,7 dBPa shall be applied at the MRP as described in ITU-T Recommendation P.64 [28].
- c) Measurements shall be made at one-twelfth octave intervals as given by the R.40 series of preferred numbers in ISO 3 [36] for frequencies from 100 Hz to 4 kHz inclusive.
- d) At each frequency, the output level for a sound pressure level of -4,7 dBPa shall be measured and the sending sensitivity shall be expressed in dBV/Pa.

#### A.5.2.1.2 Receiving Sensitivity

- a) The handset is mounted in the Loudness Rating Guard ring Position (LRGP) (see ITU-T Recommendation P.64 [28]). The earpiece is sealed to the knife-edge of an artificial ear. Alternatively the HATS position (see ITU-T Recommendation P.64 [28]) can be used. The pressure force used for handset application shall be indicated in the test report.
- b) A digital signal generator shall be connected at the digital test access point of the PBX, delivering a signal equivalent to a sinewave level of -16 dBm0 (can be derived from clause 11 of ITU-T Recommendation P.64 [28]).
- c) Measurements shall be made at one twelfth-octave intervals as given by the R.40 series of preferred numbers in ISO 3 [36] for frequencies from 100 Hz to 4 kHz inclusive.
- d) At each frequency, the sound pressure in the artificial ear shall be measured by connecting a suitable measuring set to the artificial ear and the receiving sensitivity shall be expressed in dBPa/V.

### A.5.2.2 Loudness Ratings (LR)

#### A.5.2.2.1 Send Loudness Rating (SLR)

- a) The connection is established and the handset is mounted as described in subclause A.5.2.1.1. The sending sensitivity shall be measured as described in A.5.2.1.1 but at each of the 14 frequencies (bands 4 to 17) given in table 1 of ITU-T Recommendation P.79 [29].
- b) The SLR shall be calculated according ITU-T Recommendation P.79 [29].

NOTE: ITU-T Recommendation P.64 [28] allows the use of alternative signal sources for measurement of LRs. If such a signal source is used, it is the responsibility of the test house to ensure that the method used is equivalent to that described above.

#### A.5.2.2.2 Receive Loudness Rating (RLR)

- a) A connection is established and the handset is mounted as described in subclause A.5.2.1.2. The receiving sensitivity shall be measured as described in A.5.2.1.2 at each of the 14 frequencies (bands 4 to 17) given in table 1 of ITU-T Recommendation P.79 [29].
- b) The RLR shall be calculated according to ITU-T Recommendation P.79 [29].

- c) The artificial ear sensitivity shall be corrected using the leakage correction of table 2 of ITU-T Recommendation P.79 [29] if artificial ear type 1 is used.

NOTE: ITU-T Recommendation P.64 [28] allows the use of alternative signal sources for measurement of LRs. If such a signal source is used, it is the responsibility of the test house to ensure that the method used is equivalent to that described above.

### A.5.2.3 Sidetone

For the tests described in subclauses A.5.2.3.1 and A.5.2.3.2, the digital input of the test access point shall be driven by a PCM signal corresponding to decoder value number 1.

#### A.5.2.3.1 Talker sidetone

- a) A connection is established and the handset is mounted as described in subclause A.5.2.1.1. A sinewave signal with a sound pressure level of -4,7 dBPa shall be applied at the MRP. For each frequency (bands 1 to 20) given in table 3 of ITU-T Recommendation P.79 [29], the sound pressure in the artificial ear shall be measured. The sensitivity of the sidetone path i.e. the sidetone path loss, expressed in dB, shall be calculated.
- b) Where a user controlled volume control is provided, the measurements shall be carried out at a setting, which is as close as possible to the declared nominal value of the RLR.
- c) The STMR, expressed in dB, shall be calculated according to ITU-T Recommendation P.79 [29].

NOTE: ITU-T Recommendation P.64 [28] allows the use of alternative signal sources for measurement of LRs. If such a signal source is used, it is the responsibility of the test house to ensure that the method used is equivalent to that described above.

#### A.5.2.3.2 Listener sidetone

- a) The diffuse sound field is calibrated in the absence of any local obstacles. The averaged field shall be uniform to within  $\pm 3$  dB within a radius of 0,15 m of the MRP, when measured in one-third octave bands according to IEC 61260 [35] from 100 Hz to 8 kHz (bands 1 to 20).

NOTE 1: The pressure intensity index, as defined in ISO 9614-1 [37], may prove to be a suitable method for assessing the diffuse field.

NOTE 2: Where more than one loudspeaker is used to produce the desired sound field, the loudspeakers may require to be fed with non coherent electrical signals to eliminate standing waves and other interference effects.

- b) For measurement of LSTR a connection is established and the handset is mounted as described in subclause A.5.2.1.1.
- c) Where a user controlled volume control is provided, the measurements shall be carried out at a setting which is as close as possible to the declared nominal value of the RLR.
- d) Where adaptive techniques or voice switching circuits are not used (need to be declared by the supplier), the spectrum of the diffuse sound field shall be a band limited "pink noise" (50 Hz to 10 kHz) according to annex B of ITU-T Recommendation P.64 [28], to within  $\pm 3$  dB and the level shall be adjusted to 70 dB(A) (-24 dBPa(A)). The tolerance for this level adjustment is  $\pm 1$  dB. In other cases the level shall be adjusted to 50 dB(A) (-44 dBPa(A)), with a tolerance of  $\pm 1$  dB.
- e) Measurements shall be made on one-third octave bands according to IEC 61260 [35] for the 20 bands centred at 100 Hz to 8 kHz (bands 1 to 20). For each band the sound pressure in the artificial ear shall be measured by connecting a suitable measuring set to the artificial ear.

NOTE 3: There may be problems with the signal to noise ratio. If it is less than 10 dB in any band, the microphone noise level and the noise level of any out-of-band signals need to be subtracted from the measured sidetone level (power subtraction).

- f) The listener sidetone path loss is expressed in dB and the LSTR shall be calculated according to ITU-T Recommendation P.79 [29].

### A.5.2.3.3 D factor

The sending sensitivity,  $S_{si}(\text{direct})$  (from MRP to the electrical interface) in free field is measured according to A.5.2.1.1 but with the pink noise signal as specified above. The sensitivity is measured for the 14 1/3-octave bands centred at 200 to 4 000 Hz. The sensitivity is expressed in dBV/Pa.

The diffuse sound field is adjusted according to a) and d). The sending sensitivity,  $S_{si}(\text{diff})$  (from MRP to the electrical interface) in diffuse field is measured for the 14 1/3-octave bands centred at 200 to 4 000 Hz. The sensitivity is expressed in dBV/Pa.

The value of the D-factor shall be calculated according to ITU-T Recommendation P.79 [29], annex E, formulas E.2 and E.3, over the bands from 4 to 17, using the coefficients  $K_i$  from the table E.1.

### A.5.2.4 Echo Loss at the interface KD

The test configuration is shown in figure A.20.

- a) A connection is established between the system specific telephony terminal and the interface KD.
- b) The handset is suspended in free air in such a way, that the inherent mechanical coupling of the handset is not effected. The testing shall be made under free field condition (the deviation from ideal free field conditions shall be less than 1 dB). The ambient noise level shall be less than 30 dB<sub>S<sub>PL</sub></sub> (A).
- c) The attenuation from digital input to digital output of the interface KD shall be measured separately for each echo path declared by the supplier, using a suitable of band limited (300 Hz to 3 400 Hz) test signal with a level of -10 dBm<sub>0</sub>. Suitable test signals can be found in ITU-T Recommendation P.501 [30]. Suitable test signals may be pulsed pink noise or a Composite Source Signal.
- d) A training sequence consisting of 10 s artificial voice male and female each is applied before the actual measurement. The EL at the interface KD is calculated by means of Fast Fourier Transformation (FFT) for each echo path separately. The averaged output power density spectrum is referred to averaged power density spectrum of the test signal using the identical parts of the test signal.
- e) In general the echo path may consist of various echo paths resulting from echoes at different points of the connection. These typically result in different echo impulse responses which are separate in time. If the declared echo paths cannot be separated, a separation method as described in annex B shall be used in order to separate the individual echoes. Care should be taken to use an appropriate test signal with a repetition period > the expected maximum echo delay and to use the correct window settings in order to extract the individual echo impulses from the impulse response derived from the inverse Fourier transformation as described in annex B.
- f) Finally the EL is calculated according to ITU-T Recommendation G.122 [9].

If no interface KD is available for testing, the tests should be made between the system specific terminal and the test access point. In this case the sum of the losses in both directions of the path „test point to interface KD" shall be added to the measured value.

### A.5.2.5 Talker Echo Loudness Rating

For the TELR tests a reference telephone e.g. a reference portable part according to TBR 10 [3] is required which allows the defined electrical access to the terminal. The test configurations for cases 1 and 2 are shown in figures A.21 and A.22, respectively.

In cases where only the acoustical access to the terminal is available the test shall be conducted as described in annex B of TBR 10 [3]. If different delays than those described in TBR 10 [3] are expected, the method needs to be adapted accordingly.

Case 1: Connection to an interface KD:

- a) A connection is established between the system specific telephony terminal and the interface KD leaving the transmit and receive direction of the KD interface completely separated.
- b) The attenuation from the electrical input of the reference terminal to the electrical output of the system specific reference telephone shall be measured separately for each echo path inside the PBX declared by the supplier, using a band limited (300 Hz to 3 400 Hz) test signal with an appropriate level (e.g.  $-10$  dBm0). Suitable test signals can be found in ITU-T Recommendation P.501 [30]. Suitable test signals may be pulsed pink noise or a Composite Source Signal.
- c) A training sequence consisting of 10 s artificial voice male and female each is applied before the actual measurement. The TELR at the acoustical interface is calculated by means of Fast Fourier Transformation (FFT) for each echo path separately. The averaged output power density spectrum is referred to averaged power density spectrum of the test signal using the identical parts of the test signal.
- d) In general the echo path may consist of various echo paths resulting from echoes at different points of the connection. These typically result in different echo impulse responses which are separate in time. If the declared echo paths cannot be separated, a separation method as described in annex B shall be used in order to separate the individual echoes. Care should be taken to use an appropriate test signal with a repetition period the expected maximum echo delay and to use the correct window settings in order to extract the individual echo impulses from the impulse response derived from the inverse Fourier transformation as described in annex B.
- e) Finally the TELR is calculated according to ITU-T Recommendation G.122 [9].

Case 2: Connection to an interface K2:

- a) A connection is established between the system specific telephony terminal and the interface K2, which shall be terminated with its nominal impedance.
- b) The attenuation from the electrical input of the (system specific) reference terminal to electrical output of the reference telephone shall be measured separately for each echo path inside the PBX declared by the supplier, using a band limited (300 Hz to 3 400 Hz) test signal with an appropriate level (e.g.  $-10$  dBm0). Suitable test signals can be found in ITU-T Recommendation P.501 [30]. Suitable test signals may be pulsed pink noise or a Composite Source Signal.
- c) A training sequence consisting of 10 s artificial voice male and female each is applied before the actual measurement. The TELR at the acoustical interface is calculated by means of Fast Fourier Transformation (FFT) for each echo path separately. The averaged output power density spectrum is referred to averaged power density spectrum of the test signal using the identical parts of the test signal.
- d) In general the echo path may consist of various echo paths resulting from echoes at different points of the connection. These typically result in different echo impulse responses which are separate in time. If the declared echo paths cannot be separated, a separation method as described in annex B shall be used in order to separate the individual echoes. Care should be taken to use an appropriate test signal with a repetition period  $>$  the expected maximum echo delay and to use the correct window settings in order to extract the individual echo impulses from the impulse response derived from the inverse Fourier transformation as described in annex B.
- e) Finally the TELR is calculated according to ITU-T Recommendation G.122 [9].

Case 3: Network echo control:

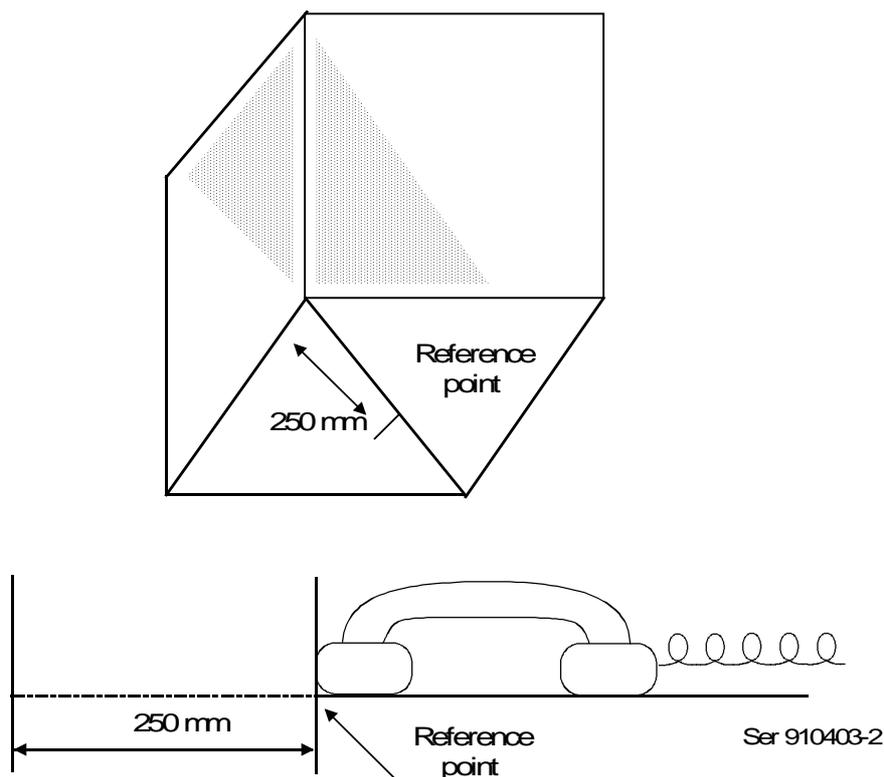
- a) A connection is established
  - aa) between the system specific telephony reference terminal and the interface KD,
  - bb) between the system specific telephony reference terminal and the interface K2,which shall be terminated with the test network echo path according to figures A.23 and A.24, respectively.
- b) The attenuation from the electrical input of the (system specific) reference terminal to electrical output of the reference telephone shall be measured separately for each echo path inside the PBX declared by the supplier, using a band limited (300 Hz to 3 400 Hz) test signal with an appropriate level (e.g.  $-10$  dBm0). Suitable test signals can be found in ITU-T Recommendation P.501 [30]. Suitable test signals may be pulsed pink noise or a Composite Source Signal.

- c) A training sequence consisting of 10 s artificial voice male and female each is applied before the actual measurement. The TELR at the acoustical interface is calculated by means of Fast Fourier Transformation (FFT) for each echo path separately. The averaged output power density spectrum is referred to averaged power density spectrum of the test signal using the identical parts of the test signal.
- d) In general the echo path may consist of various echo paths resulting from echoes at different points of the connection. These typically result in different echo impulse responses which are separate in time. If the declared echo paths cannot be separated, a separation method as described in annex B shall be used in order to separate the individual echoes. Care should be taken to use an appropriate test signal with a repetition period > the expected maximum echo delay and to use the correct window settings in order to extract the individual echo impulses from the impulse response derived from the inverse Fourier transformation as described in annex B.
- e) Finally the TELR of the test network echo path is calculated according to ITU-T Recommendation G.122 [9].

### A.5.2.6 Stability loss

The measurement of stability loss is performed independent, if the system specific telephony terminal is an analogue or digital telephony terminal, connected to its appropriate interface of the PBX.

- a) A connection is established between the system specific telephony terminal and the test access point.
- b) The handset, with the transmission circuit fully active, shall be positioned on one inside surface that is of three perpendicular plane, smooth, hard surfaces forming a corner. Each surface shall extend 0,5 m from the apex of the corner. One surface shall be marked with a diagonal line, extending from the corner formed by the three surfaces and a reference position 250 mm from the corner, as shown in figure A.5:



**Figure A.5: Position of handset for stability measurements**

- c) With an input signal of -10 dBm0, the attenuation from digital input to digital output of the test access point shall be measured, using a sinewave at one-twelfth octave intervals for frequencies from 200 Hz to 3 600 Hz under the following conditions:
  - the handset, with the transmission circuit fully active, shall be positioned on the defined surface as follows:
    - 1) the mouthpiece and earcup shall face towards the surface;

- 2) the handset shall be placed centrally, the diagonal line with the earcap nearer to the apex of the corner;
- 3) the extremity of the handset shall coincide with the normal to the reference point, as shown in figure A.5.

## A.5.2.7 Distortion

### A.5.2.7.1 Sending

#### A.5.2.7.1.1 Method 1

- a) A connection is established between the system specific telephony terminal and the test access point of the PBX. The handset is mounted at the LRGP and the earpiece is sealed to the knife-edge of the artificial ear. Alternatively the HATS position (see ITU-T Recommendation P.64 [28]) can be used. The pressure force used for handset application shall be indicated in the test report.
- b) A band-limited noise signal corresponding to ITU-T Recommendation O.131 [20], shall be applied at the MRP. The level of this signal is adjusted until the output at the test access point is -10 dBm<sub>0</sub>. The level of the signal at the MRP in dBPa is then the ARL.
- c) The test signal shall be applied at the following levels relative to ARL:  
-45 dB, -40 dB, -35 dB, -30 dB, -24 dB, -20 dB, -17 dB, -10 dB, -5 dB, 0 dB, 4 dB, 7 dB.
- d) The ratio of signal to total distortion power of the digital signal output shall be measured (see annex A of ITU-T Recommendations Q.551 [31] and O.131 [20]).

#### A.5.2.7.1.2 Method 2

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) A sine-wave signal with a frequency in the range 1 004 Hz to 1 025 Hz shall be applied at the MRP. The level of this signal is adjusted until the output of the test access point is -10 dBm<sub>0</sub>. The level of the signal at the MRP in dBPa is then the ARL.
- c) The test signal shall be applied at the following levels relative to ARL:  
-35 dB, -30 dB, -25 dB, -20 dB, -15 dB, -10 dB, -5 dB, 0 dB, 7 dB, 10 dB.
- d) The ratio of the signal to total distortion power of the digital signal output shall be measured with the psophometric noise weighting (see ITU-T Recommendations Q.551 [31] and O.132 [21]).

### A.5.2.7.2 Receiving

#### A.5.2.7.2.1 Method 1

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) A digitally simulated band-limited noise signal corresponding to ITU-T Recommendation O.131 [20] shall be applied at the input of the test access point at the following levels:  
-55 dBm<sub>0</sub>, -50 dBm<sub>0</sub>, -45 dBm<sub>0</sub>, -40 dBm<sub>0</sub>, -34 dBm<sub>0</sub>, -30 dBm<sub>0</sub>, -27 dBm<sub>0</sub>, -20 dBm<sub>0</sub>, -15 dBm<sub>0</sub>, -10 dBm<sub>0</sub>, -6 dBm<sub>0</sub>, -3 dBm<sub>0</sub>.
- c) The ratio of signal to total distortion power shall be measured in the artificial ear (see annex A of ITU-T Recommendations Q.551 [31] and O.131 [20]).

#### A.5.2.7.2.2 Method 2

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.

- b) A digitally simulated sine-wave signal with a frequency in the range 1 004 Hz to 1 025 Hz shall be applied at the input of the test access point at the following levels:  
-45 dBm0, -40 dBm0, -35 dBm0, -30 dBm0, -25 dBm0, -20 dBm0, -15 dBm0, -10 dBm0, -3 dBm0, 0 dBm0.
- c) The ratio of the signal-to-total distortion power shall be measured with the psophometric noise weighting in the artificial ear (see ITU-T Recommendations Q.551 [31] and O.132 [21]).

### A.5.2.7.3 Sidetone

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) An instrument capable of measuring the third harmonic distortion of signals with fundamental frequencies in the range of 315 Hz to 1 kHz shall be connected to the artificial ear.
- c) The digital input of the test access point shall be driven by a PCM signal, corresponding to decoder value number 1.
- d) A pure-tone signal of -4,7 dBPa shall be applied at the MRP at frequencies of 315 Hz, 500 Hz and 1 kHz. For each frequency, the third harmonic distortion shall be measured in the artificial ear.

## A.5.2.8 Variation of gain with input level

### A.5.2.8.1 Sending

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) A sine-wave signal with a frequency in the range 1 004 Hz to 1 025 Hz shall be applied at the MRP. The level of this signal is adjusted, until the output at the test access point is -10 dBm0. The level of the signal at the MRP in dBPa is then the ARL.
- c) The test signal shall be applied at the following levels relative to ARL:  
-45 dB, -40 dB, -35 dB, -30 dB, -25 dB, -20 dB, -15 dB, -10 dB, -5 dB, 0 dB, 4 dB, 10 dB, 13 dB.
- d) The variation of gain relative to the gain for the ARL shall be measured.

NOTE: Selective measurement may be used to avoid the effects of ambient noise.

### A.5.2.8.2 Receiving

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) A digitally simulated sine-wave signal with a frequency in the range 1 004 Hz to 1 025 Hz shall be applied at the digital interface at the following levels:  
-50 dBm0, -45 dBm0, -40 dBm0, -35 dBm0, -30 dBm0, -25 dBm0, -20 dBm0, -15 dBm0, -10 dBm0, -6 dBm0, 0 dBm0, 3 dBm0.
- c) The variation of gain relative to the gain at an input level of -10 dBm0 shall be measured in the artificial ear.

NOTE: Selective measurement may be used to avoid the effects of ambient noise.

## A.5.2.9 Out-of-band signals

### A.5.2.9.1 Discrimination against out-of-band input signal

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) Input signals at frequencies of 4,65 kHz, 5 kHz, 6 kHz, 6,5 kHz, 7 kHz and 7,5 kHz are applied at the MRP with a level of -4,7 dBPa.

- c) The level of any inband image frequency at the output of the test access point shall be measured selectively.

#### A.5.2.9.2 Spurious out-of-band signals

- a) A connection is established and the handset is mounted as described in subclause A.5.2.7.1.1.
- b) Input signals at the frequencies 500 Hz, 1 000 Hz, 2 000 Hz, and 3 150 Hz are applied at the input of the test access point with a level of -10 dBm0.
- c) The level of spurious out-of-band image signals at frequencies of up to 8 kHz shall be measured selectively in the artificial ear.

### A.5.2.10 Noise

#### A.5.2.10.1 Sending

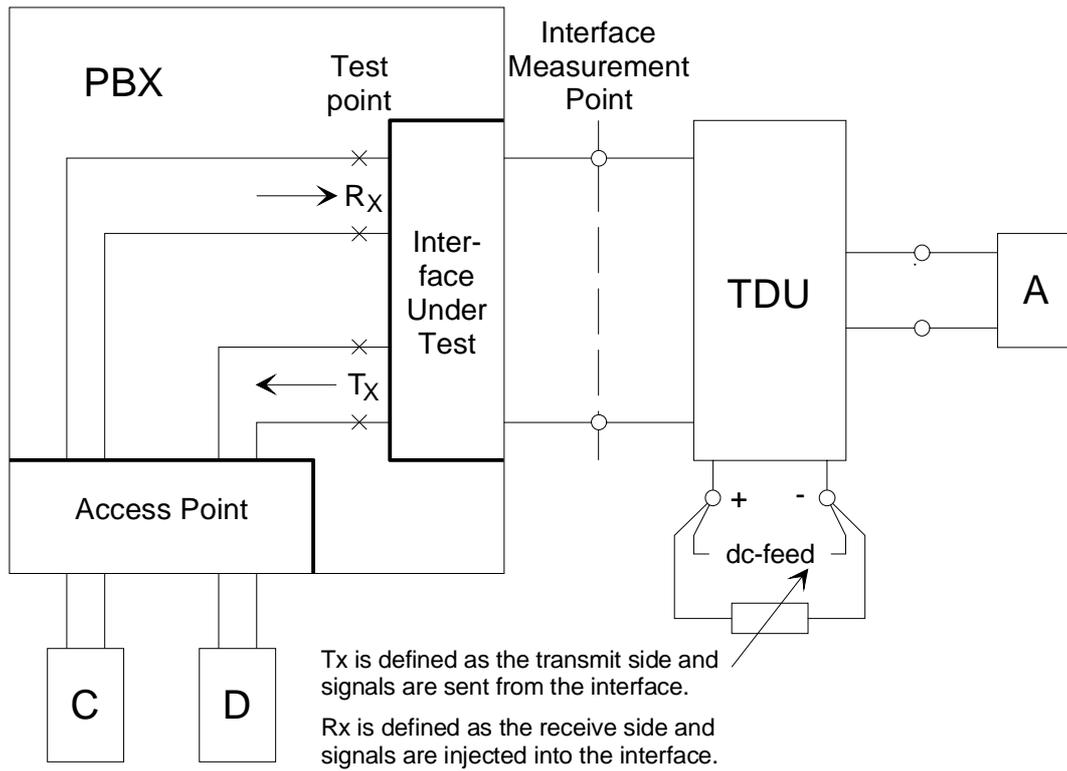
- a) A connection between the system specific telephony terminal and the test access point is established and the handset mounted at the LRGP with the earpiece sealed to the knife-edge of the artificial ear in a quiet environment (ambient noise less than 30 dB<sub>SPL(A)</sub>). Alternatively the HATS position (see ITU-T Recommendation P.64 [28]) can be used. The pressure force used for handset application shall be indicated in the test report.
- b) The noise level at the output of the test AP shall be measured with apparatus including psophometric weighting according to table 4 of ITU-T Recommendation G.223 [10].

#### A.5.2.10.2 Receiving

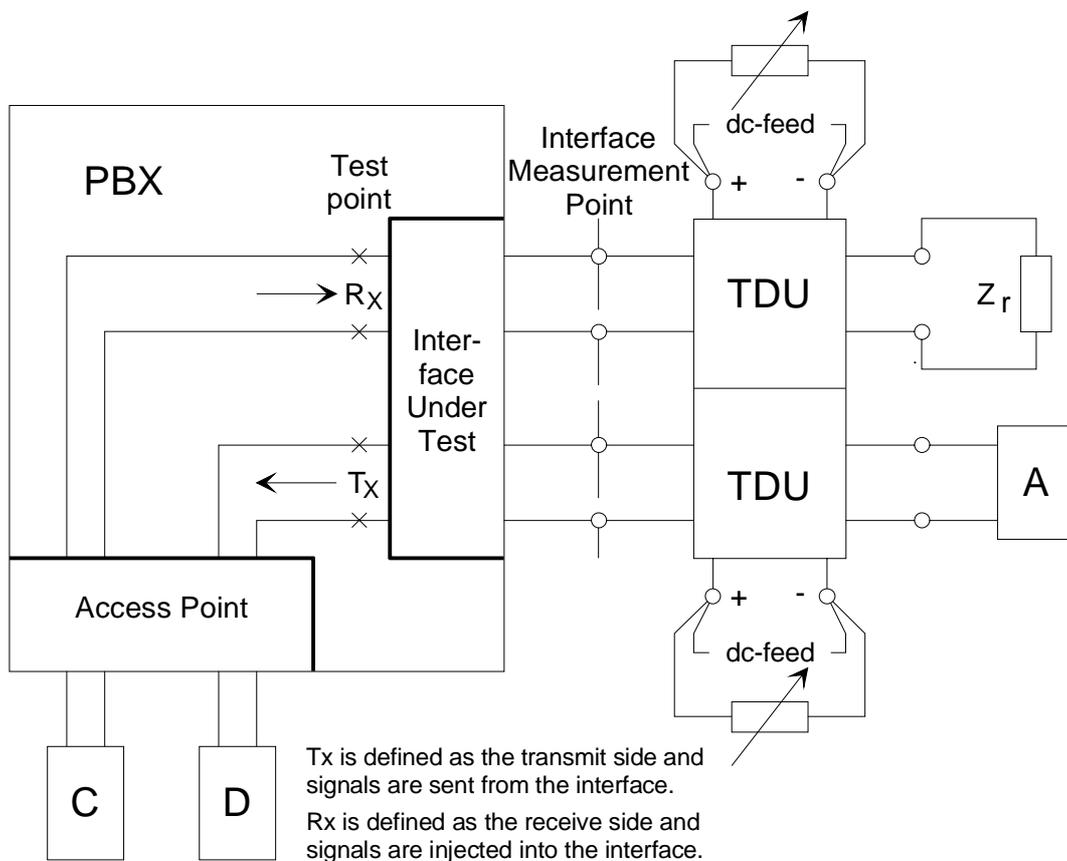
- a) A connection is established and the handset is mounted as described in subclause A.5.2.10.1. The ambient noise shall not exceed 30 dB<sub>SPL(A)</sub>.
- b) A signal corresponding to decoder output value number 1 shall be applied at the input of the test AP.
- c) Where a user controlled volume control is provided, the measurements shall be carried out at a setting, which is as close as possible to the declared nominal value of the RLR.
- d) The level of the noise shall be measured in the artificial ear.

#### A.5.2.10.3 Level of sampling frequency (receiving)

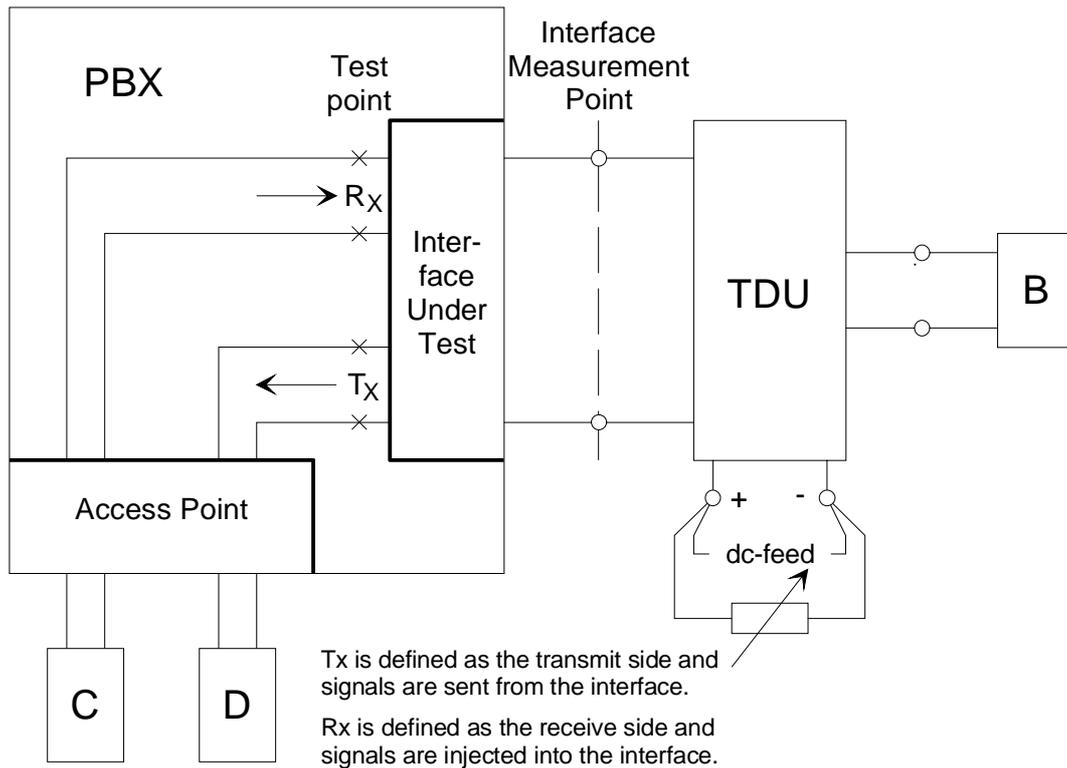
Under the same conditions as specified in subclause A.5.2.10.2, the level at 8 kHz in the artificial ear shall be measured selectively.



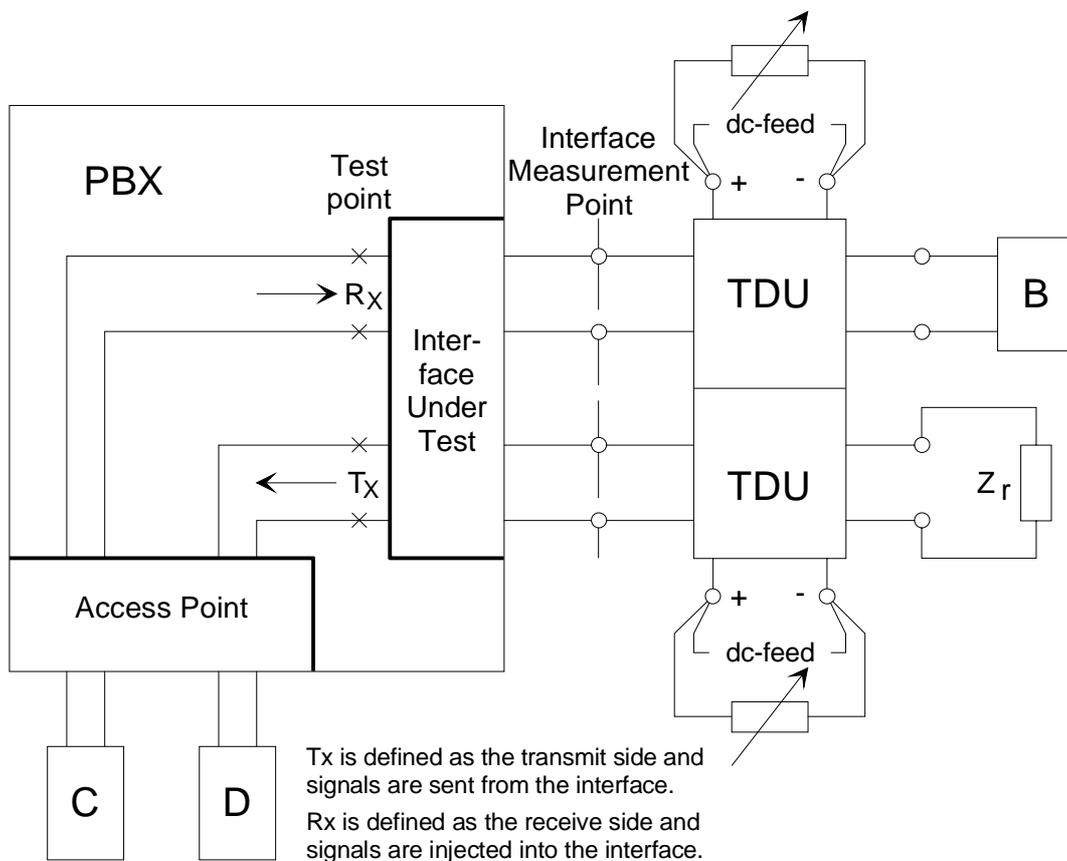
**Figure A.6: 2-wire analogue interface, input connection**



**Figure A.7: 4-wire analogue interface, input connection**



**Figure A.8: 2-wire analogue interface, output connection**



**Figure A.9: 4-wire analogue interface, output connection**

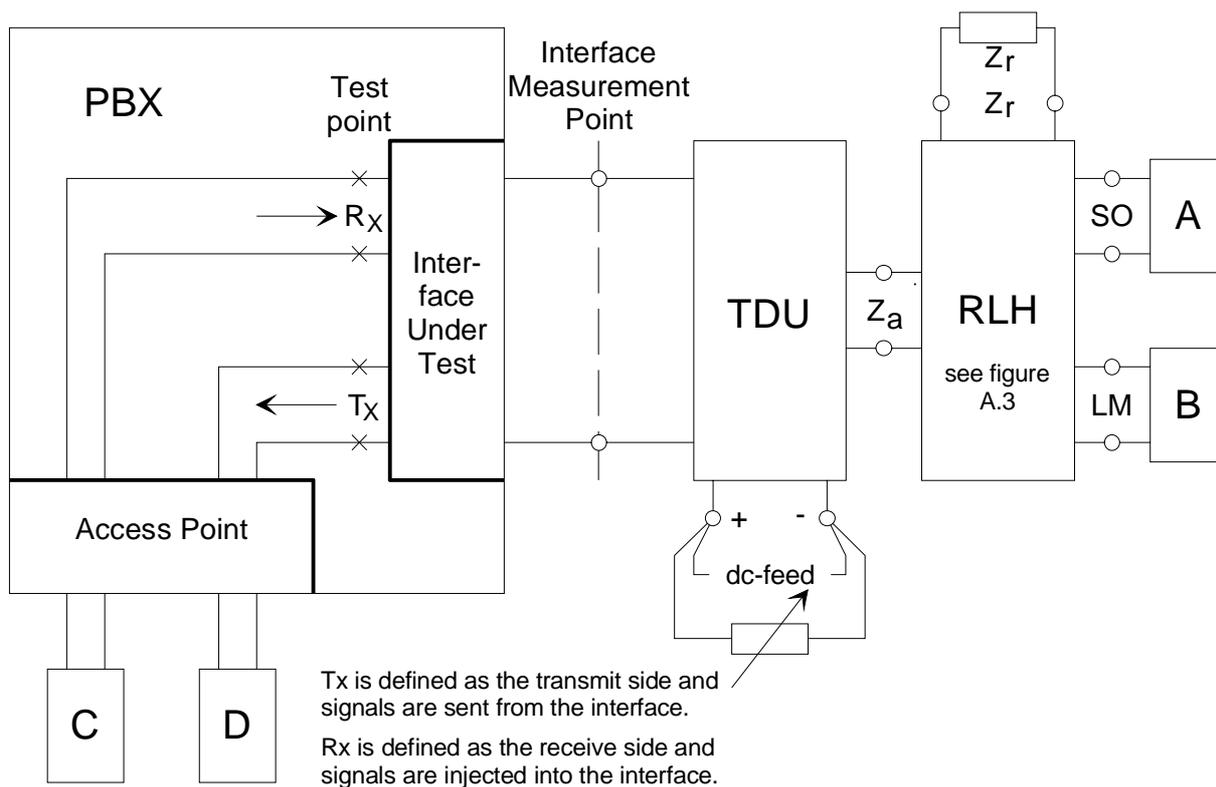


Figure A.10: 2-wire analogue interface, return loss

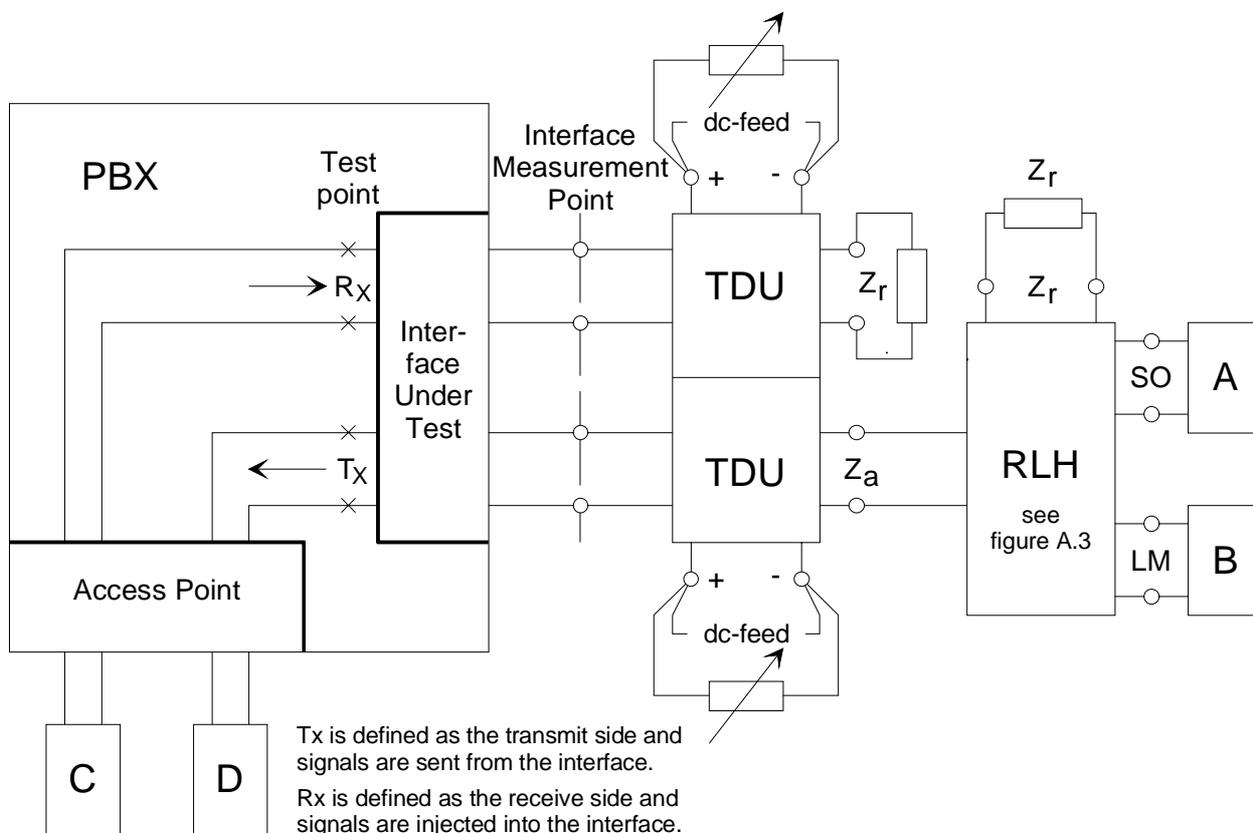


Figure A.11: 4-wire analogue interface, return loss (shown only for the transmit side)

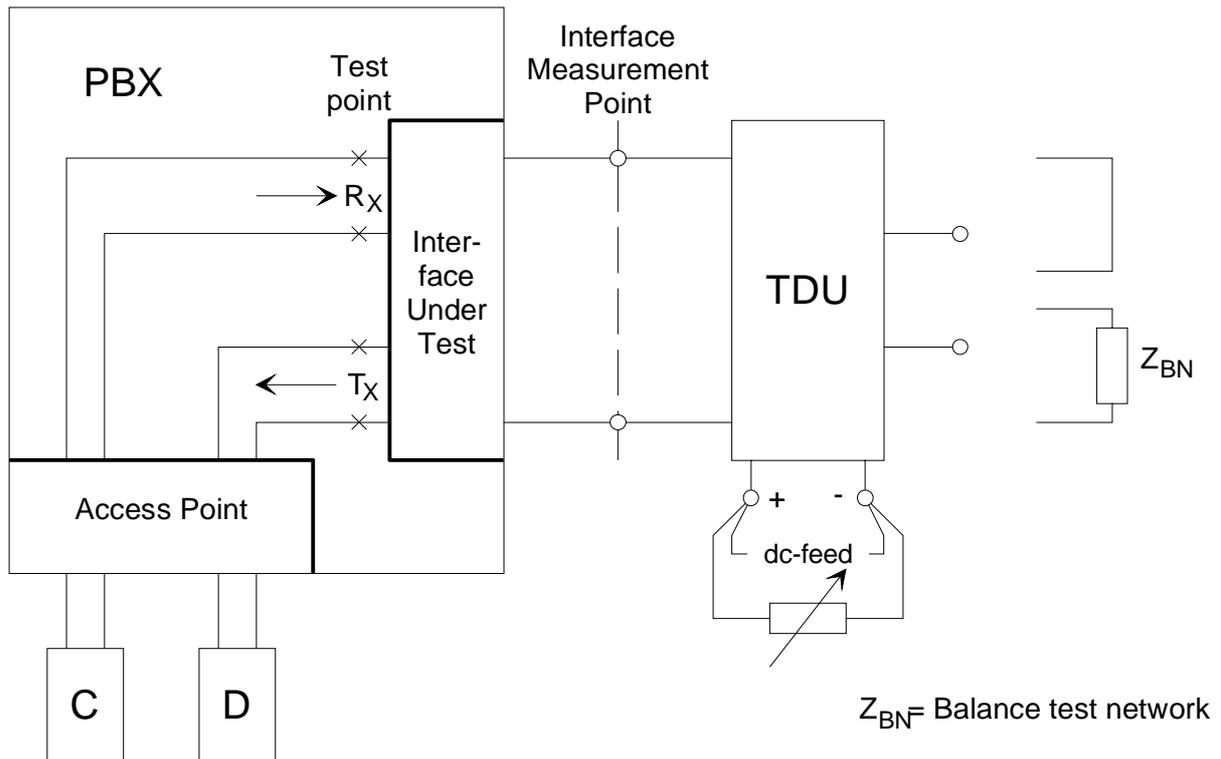
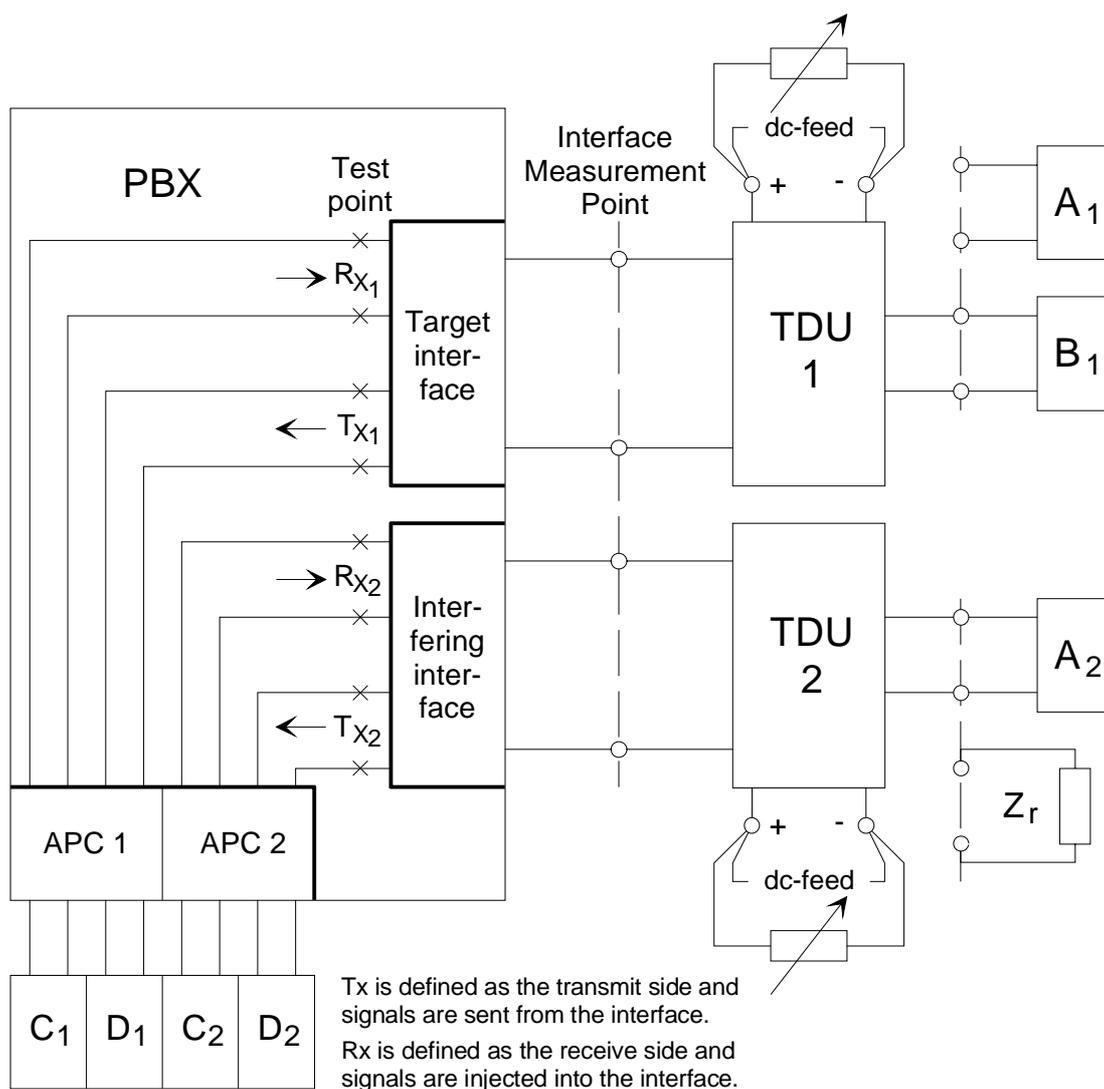
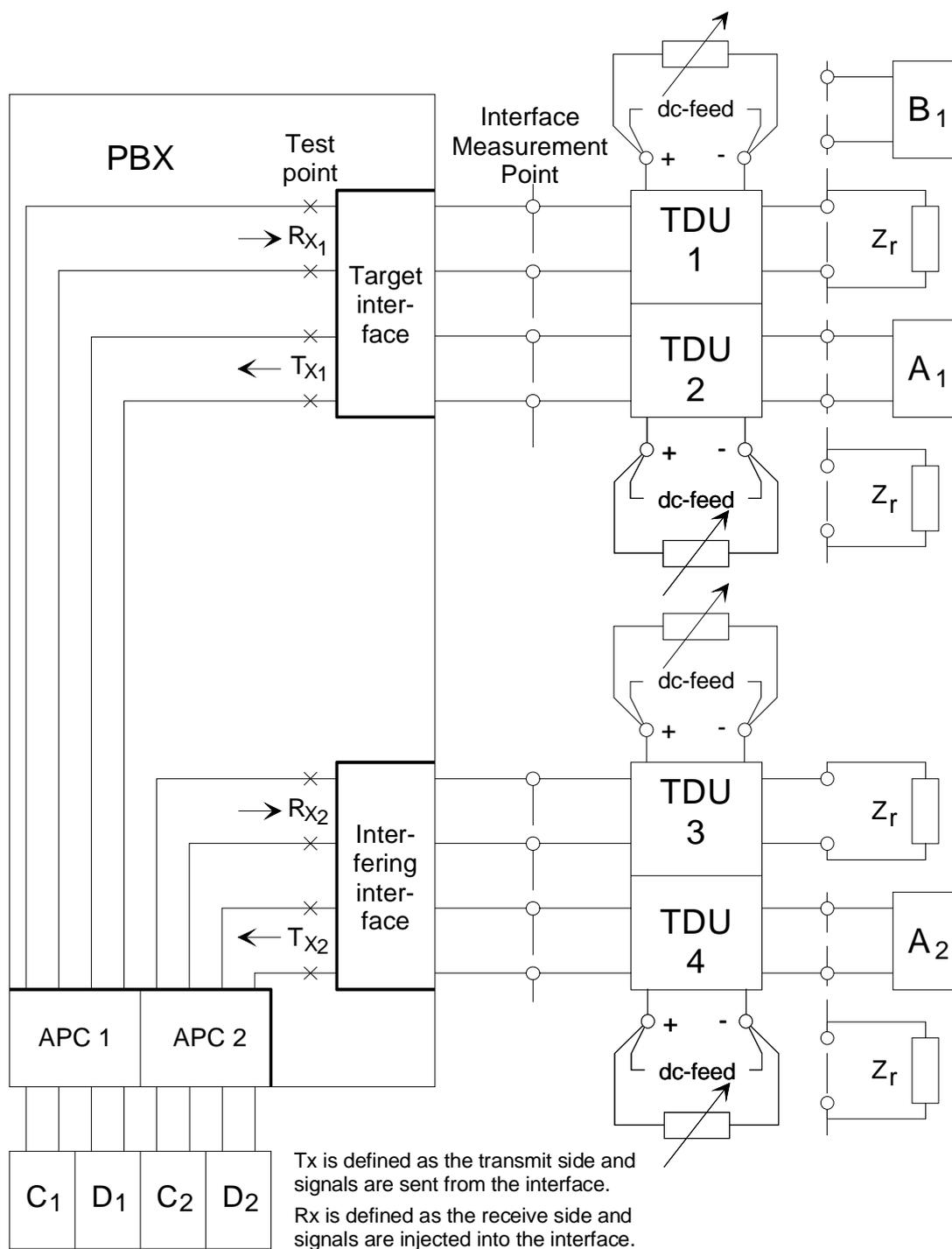


Figure A.12: Terminal Balance Return Loss, stability



Case No.	Connection	NEXT/FEXT	TDU 1	TDU 2	C <sub>1</sub>	C <sub>2</sub>	D <sub>1</sub>	D <sub>2</sub>
1	Input	FEXT	A <sub>1</sub> Activating	A <sub>2</sub> Sending	Quiet Code	Quiet Code	Measuring	
2	Input	NEXT	B <sub>1</sub> Measuring	A <sub>2</sub> Sending	Quiet Code	Quiet Code		
3	Output	FEXT	B <sub>1</sub> Measuring	Z <sub>r</sub>	Quiet Code	Sending		
4	Output	NEXT	A <sub>1</sub> Activating	Z <sub>r</sub>	Quiet Code	Sending	Measuring	

Figure A.13: Crosstalk measurements on 2-wire analogue interfaces



Case No.	Connec-tion	NEXT/FEXT	TDU 1	TDU 2	TDU 3	TDU 4	C <sub>1</sub>	C <sub>2</sub>	D <sub>1</sub>	D <sub>2</sub>
1	Input	FEXT	Z <sub>r</sub>	A <sub>1</sub> Activating	Z <sub>r</sub>	A <sub>2</sub> Sending	Quiet Code	Quiet Code	Measuring	
2	Input	NEXT	B <sub>1</sub> Measuring	Z <sub>r</sub>	Z <sub>r</sub>	A <sub>2</sub> Sending	Quiet Code	Quiet Code		
3	Output	FEXT	B <sub>1</sub> Measuring	Z <sub>r</sub>	Z <sub>r</sub>	Z <sub>r</sub>	Quiet Code	Sending		
4	Output	NEXT	Z <sub>r</sub>	A <sub>1</sub> Activating	Z <sub>r</sub>	Z <sub>r</sub>	Quiet Code	Sending	Measuring	

Figure A.14: Crosstalk measurements on 4-wire analogue interfaces

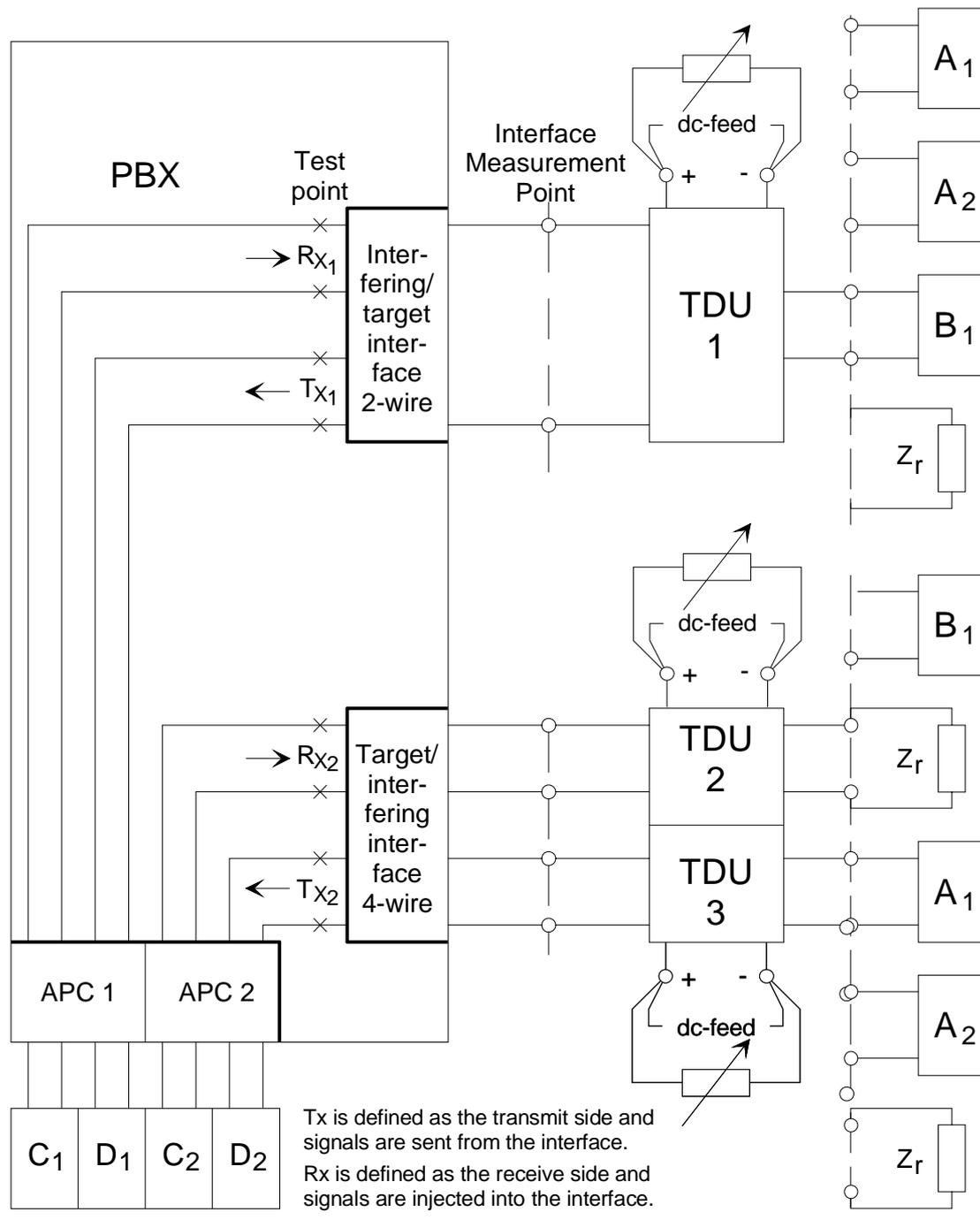


Figure A.15 (1 of 2): Crosstalk measurements between 4-wire and 2-wire analogue interfaces

Interfering interface: 2-wire      Target interface: 4-wire

Case No.	Connection	NEXT/FEXT	TDU 1	TDU 2	TDU 3	C <sub>1</sub>	C <sub>2</sub>	D <sub>1</sub>	D <sub>2</sub>
1	Input	FEXT	A <sub>2</sub> Sending	Z <sub>r</sub>	A <sub>1</sub> Activating	Quiet Code	Quiet Code		Measuring
2	Input	NEXT	A <sub>2</sub> Sending	B <sub>1</sub> Measuring	Z <sub>r</sub>	Quiet Code	Quiet Code		
3	Output	FEXT	Z <sub>r</sub>	B <sub>1</sub> Measuring	Z <sub>r</sub>	Sending	Quiet Code		
4	Output	NEXT	Z <sub>r</sub>	Z <sub>r</sub>	A <sub>1</sub> Activating	Sending	Quiet Code		Measuring

Interfering interface: 4-wire    Target interface: 2-wire

Case No.	Connection	NEXT/FEXT	TDU 1	TDU 2	TDU 3	C <sub>1</sub>	C <sub>2</sub>	D <sub>1</sub>	D <sub>2</sub>
1	Input	FEXT	A <sub>1</sub> Activating	Z <sub>r</sub>	A <sub>2</sub> Sending	Quiet Code	Quiet Code	Measuring	
2	Input	NEXT	B <sub>1</sub> Measuring	Z <sub>r</sub>	A <sub>2</sub> Sending	Quiet Code	Quiet Code		
3	Output	FEXT	B <sub>1</sub> Measuring	Z <sub>r</sub>	Z <sub>r</sub>	Quiet Code	Sending		
4	Output	NEXT	A <sub>1</sub> Activating	Z <sub>r</sub>	Z <sub>r</sub>	Quiet Code	Sending	Measuring	

Figure A.15 (2 of 2): Crosstalk measurements between 4-wire and 2-wire analogue interfaces

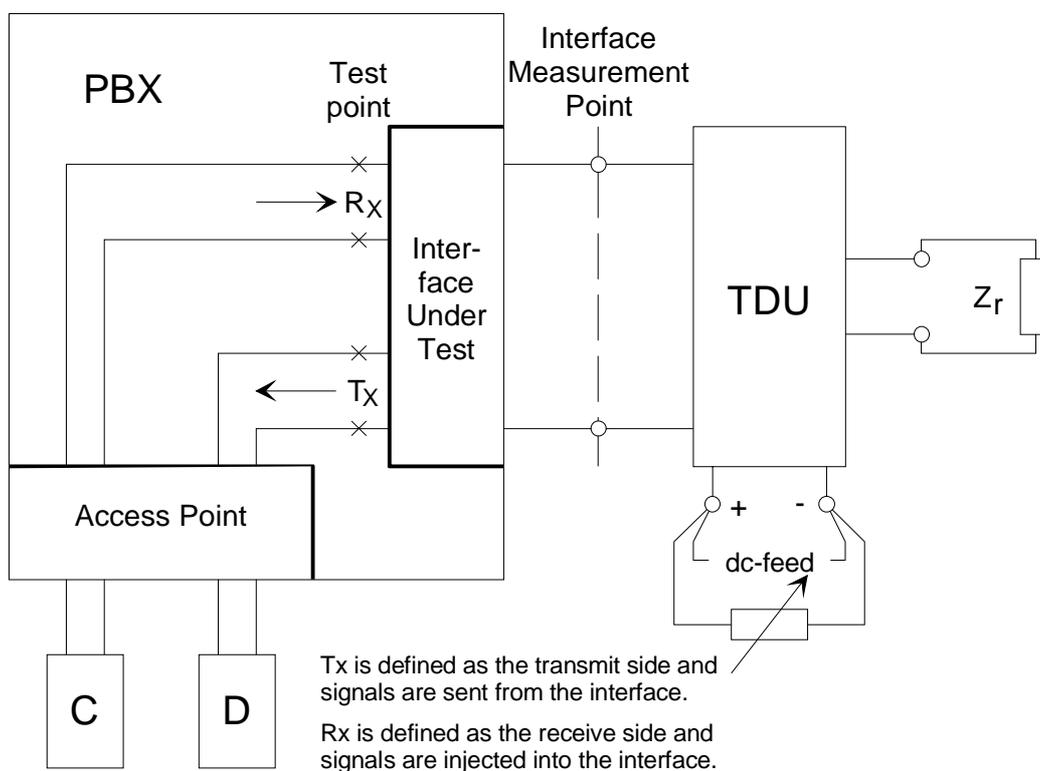


Figure A.16: 2-wire analogue interface, input connection noise measurement

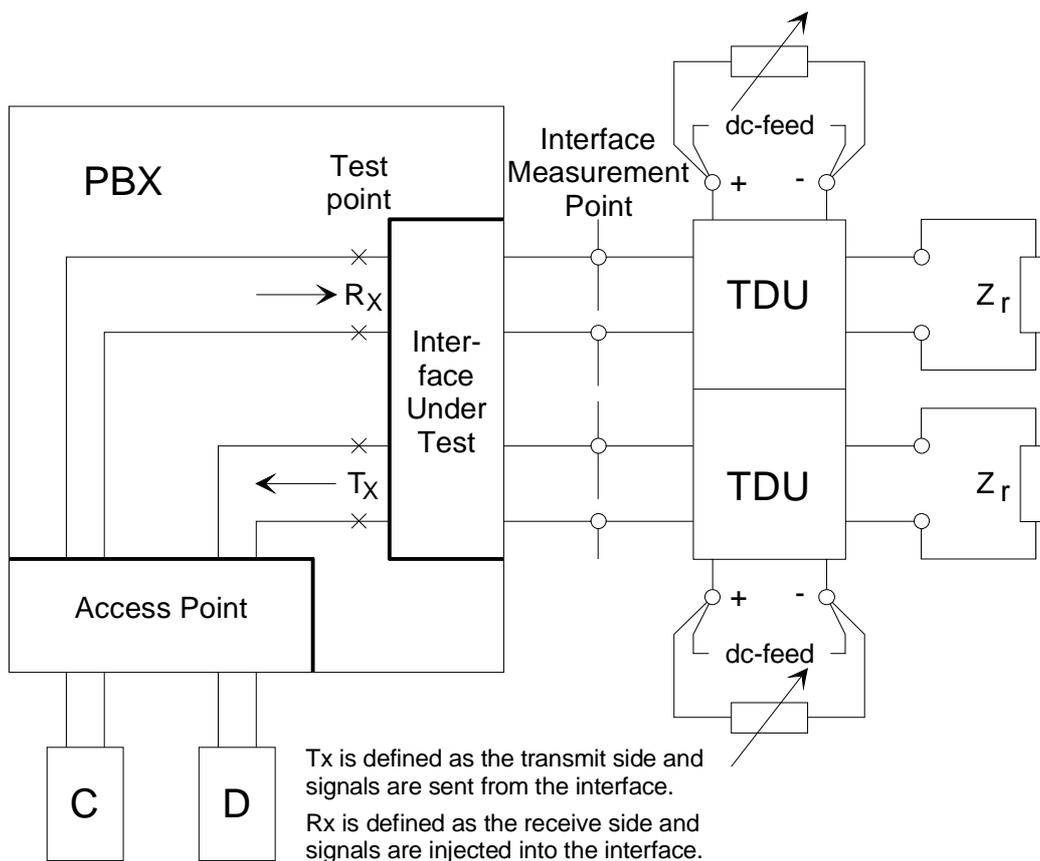


Figure A.17: 4-wire analogue interface, input connection noise measurement

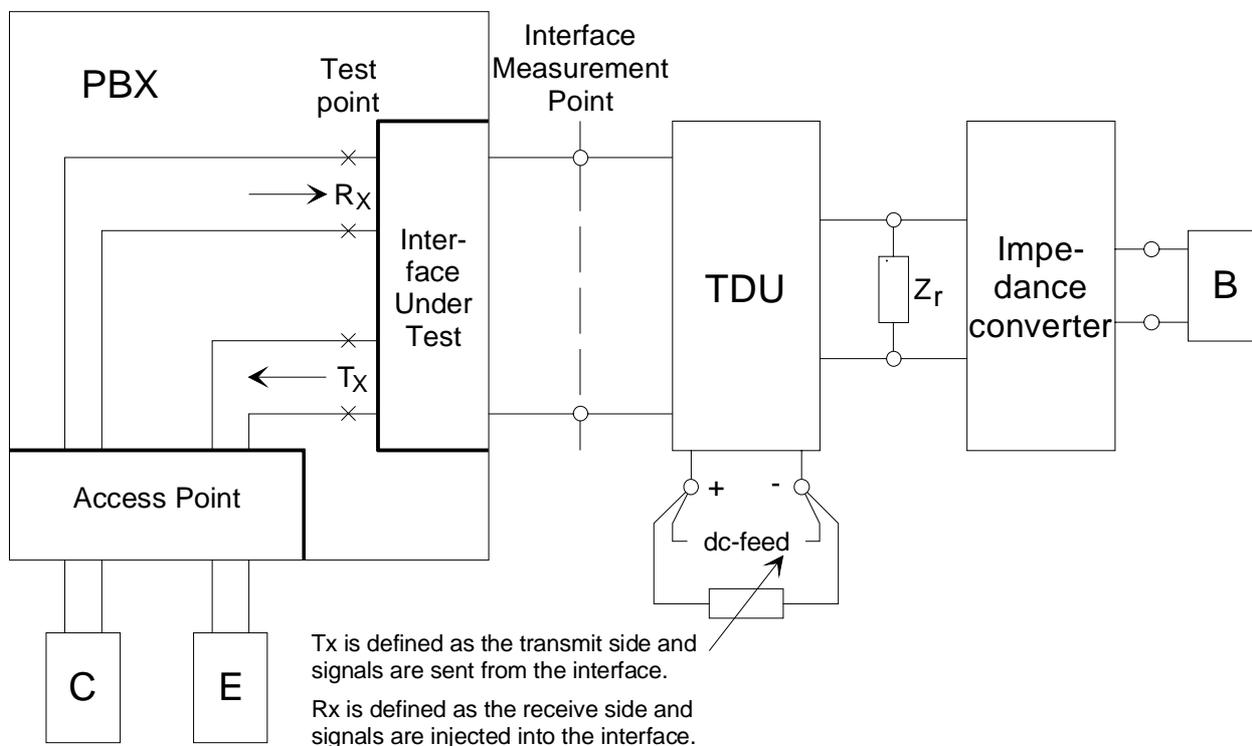


Figure A.18: 2-wire analogue interface, output connection noise measurement

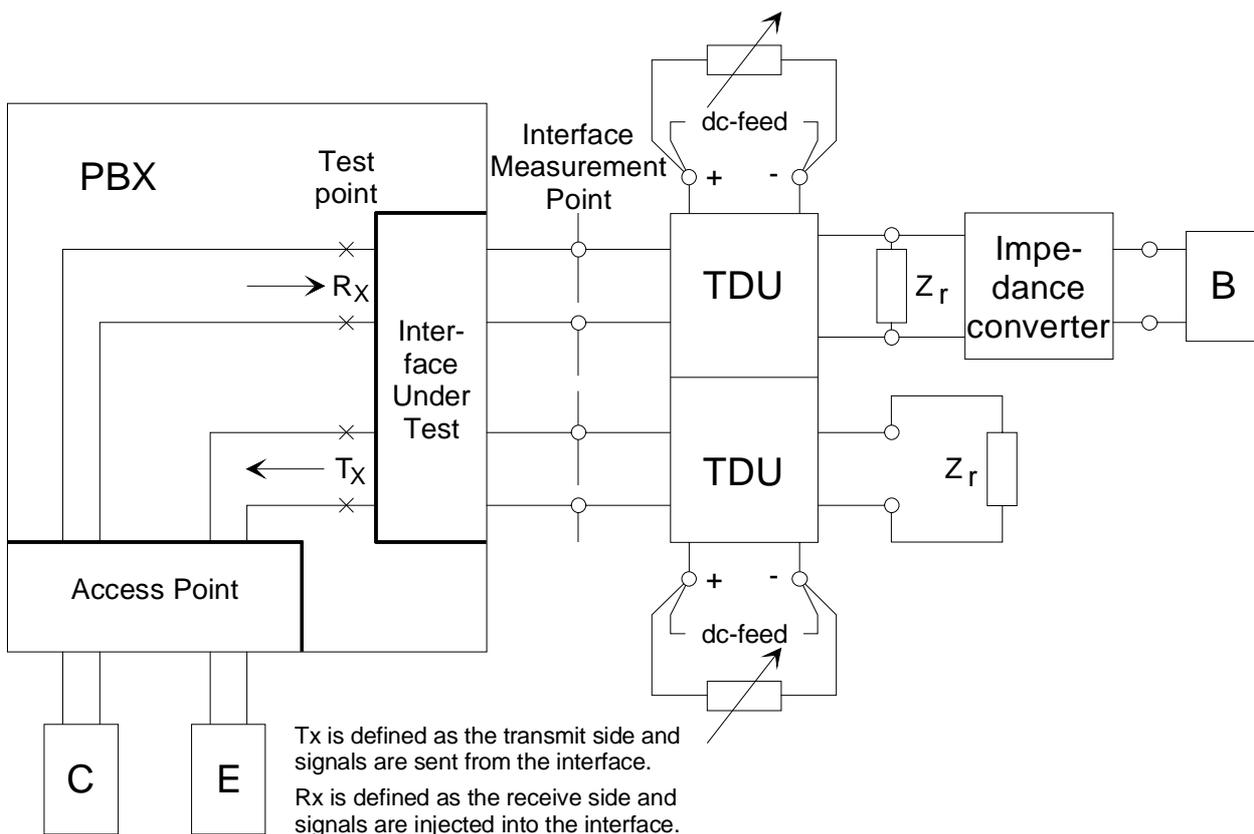


Figure A.19: 4-wire analogue interface, output connection noise measurement

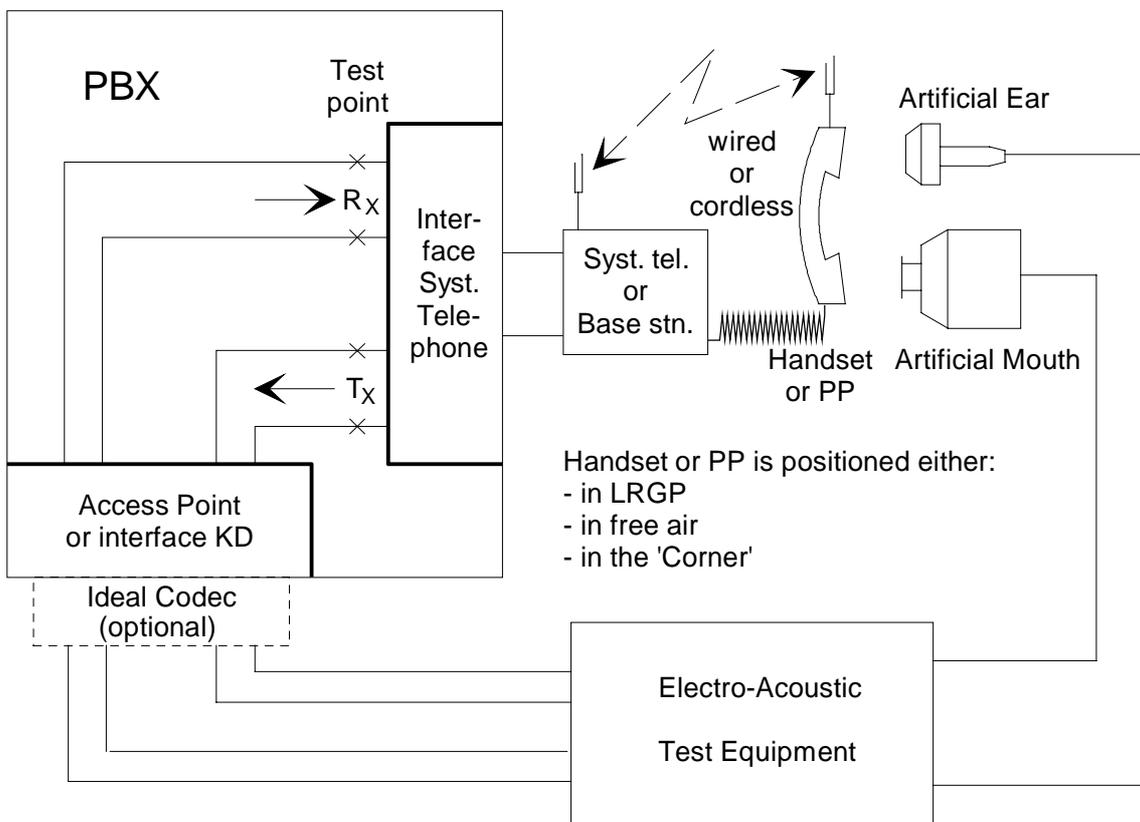


Figure A.20: Test configuration for electro-acoustic measurements

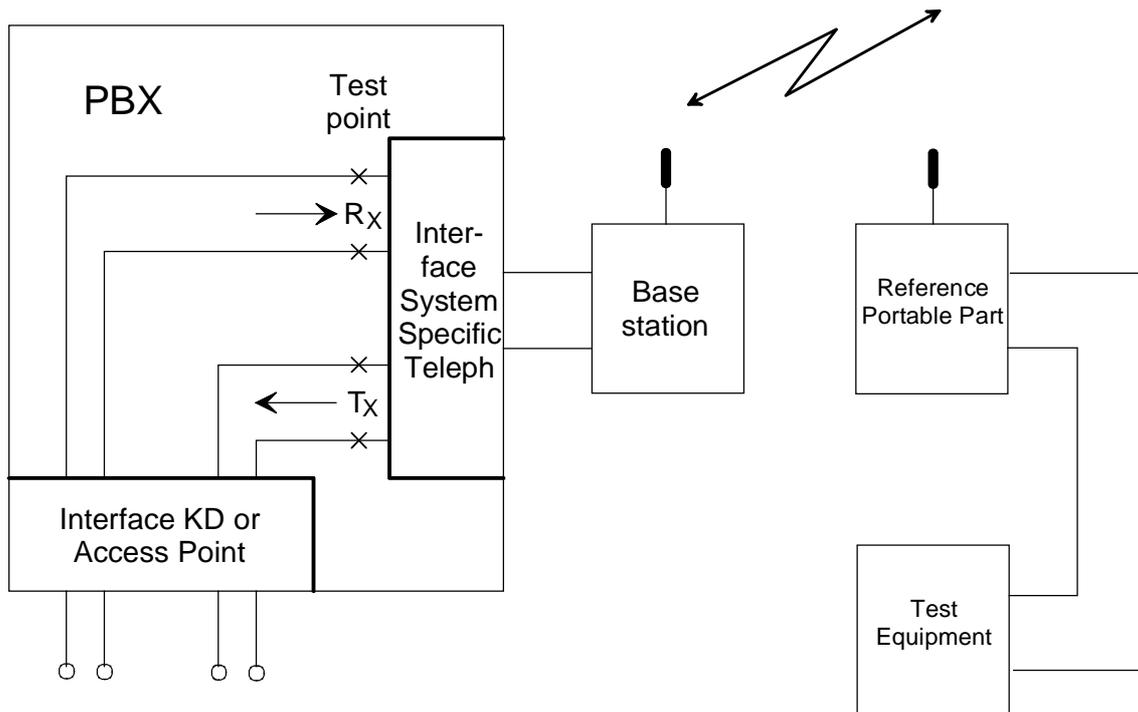


Figure A.21: Test configuration for measurement of Talker Echo Loudness Rating (case 1)

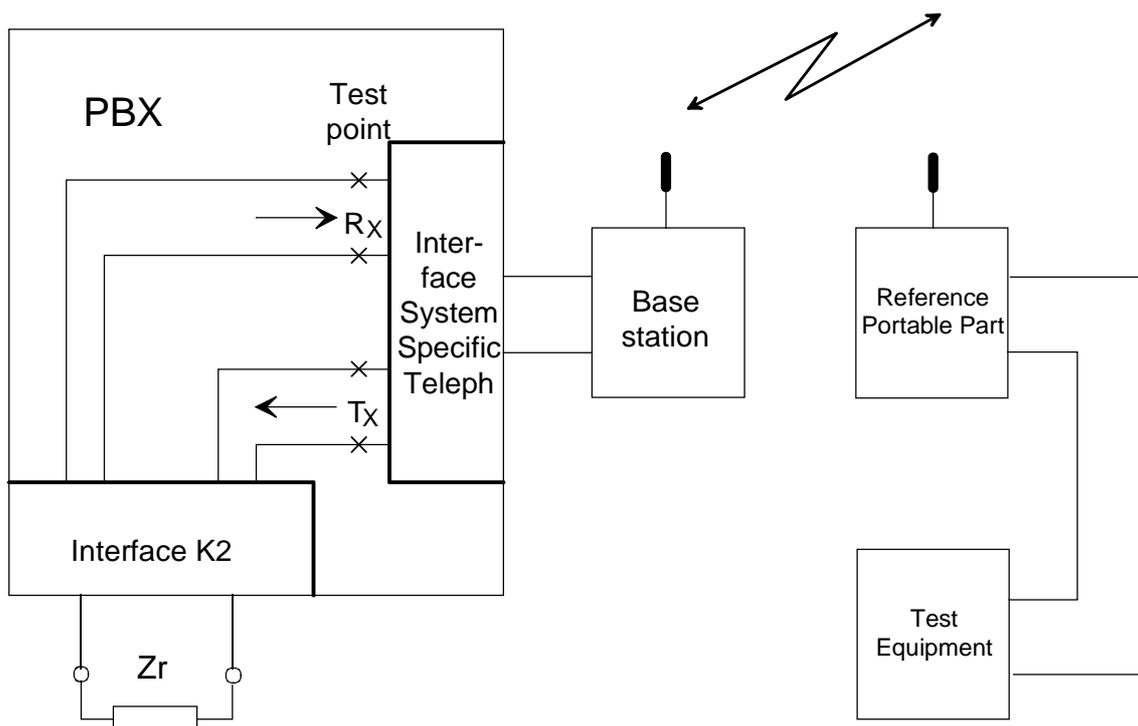


Figure A.22: Test configuration for measurement of Talker Echo Loudness Rating (case 2)

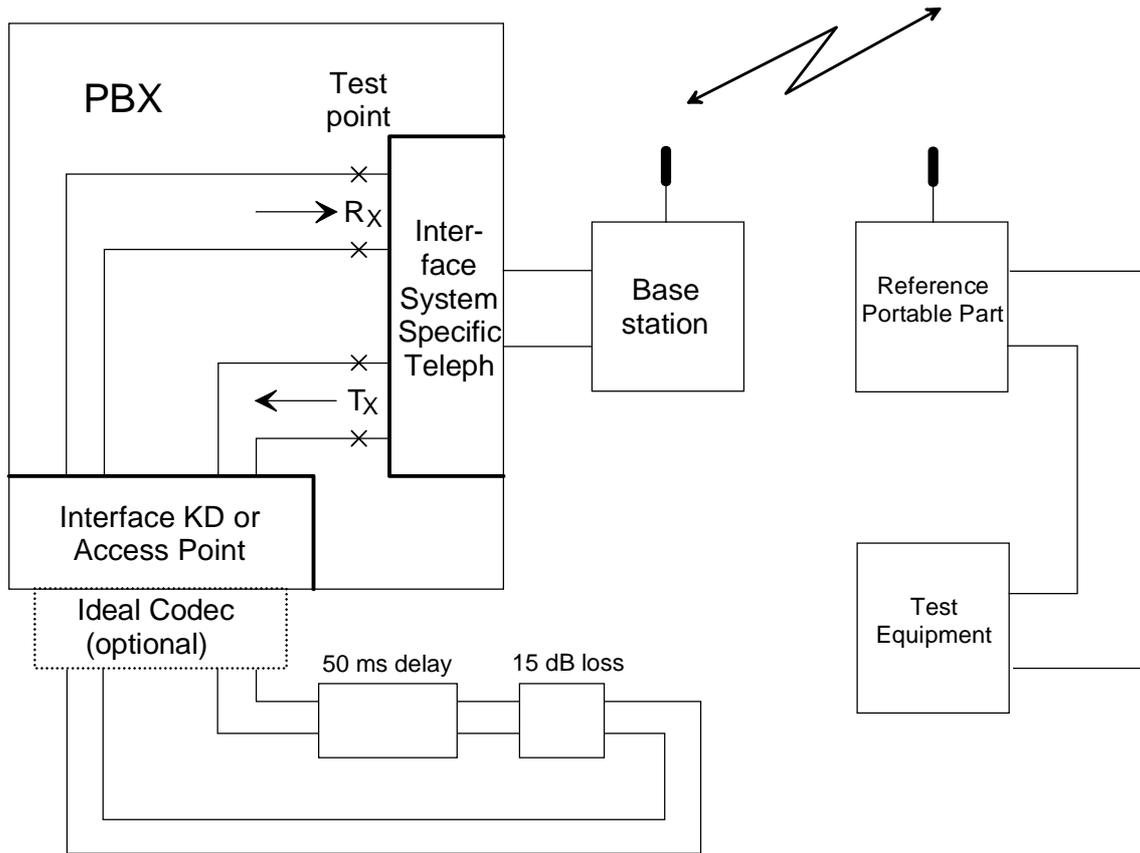


Figure A.23: Test configuration for measurement of Talker Echo Loudness Rating (case 3)

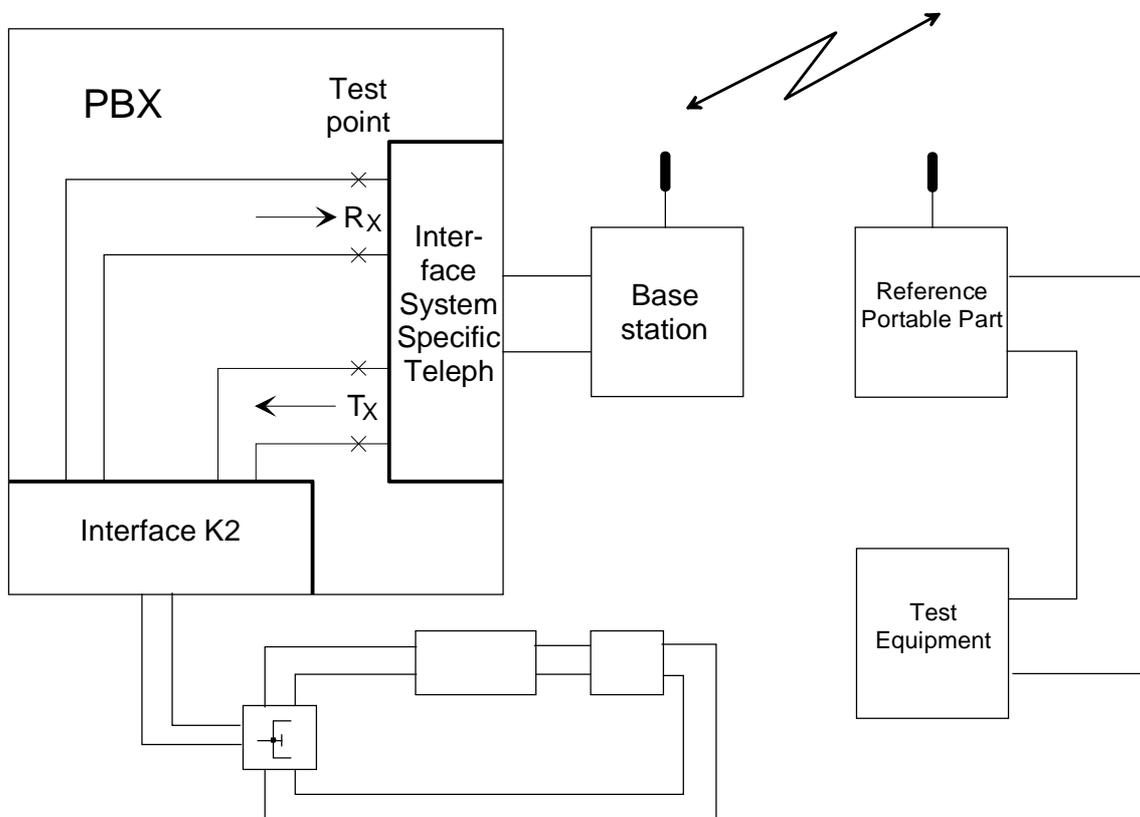


Figure A.24: Test configuration for measurement of Talker Echo Loudness Rating (case 3)

## Annex B (informative): Description of the CSS

### B.1 General

The Composite Source Signal is composed as a time multiplex of at least three signal sources with a:

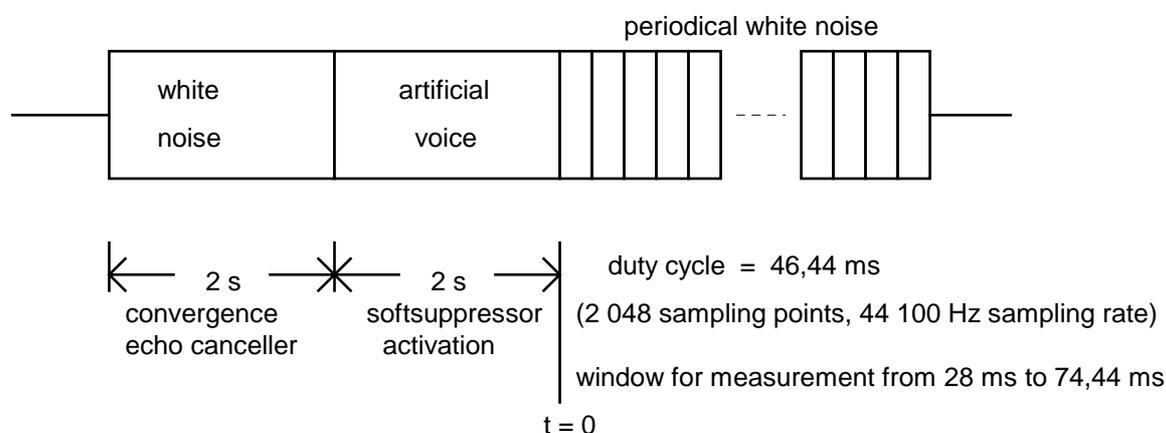
- voiced signal to simulate voice properties for a certain activation of the transfer function;
- deterministic signal for measuring the transfer function;
- pause "signal" providing amplitude modulation.

The CSS is described in detail in ITU-T Recommendation P.501 [30] and specified in annex B of I-ETS 300 245-3 [2].

For the measurement of a DECT system the PP shall be placed in the LRGP and the test signal of the CSS shall be applied at the MRP with a level of -4,7 dBPa. For the measurement of the FP the test signal of the CSS shall be applied at the TAP of the RePP or the PP with a level of -10 dBm0. Only one measurement shall be made.

### B.2 Test signal

The test signal with the characteristic as described below is applied to the input Lin at the RePP (figure 12). The measurement starts on the output Lout of the RePP (figure 12) 28 ms after the starting of the periodical white noise. The duty cycle of the measurement shall be identical with the duty cycle of the periodical white noise.



**Figure B.1**

artificial voice: according to ITU-T Recommendation P.50 [23] white noise band limited 100 Hz to 10 kHz.

**Table B.1**

Upper limit		Lower limit	
45 Hz	-36 dB	< 100 Hz	-∞ dB
90 Hz	-21 dB	100 Hz	-26,5 dB
		200 Hz	-19,5 dB
		5 000 Hz	-5,5 dB
11 200 Hz	0 dB	10 000 Hz	-6,5 dB
22 400 Hz		> 10 000 Hz	-∞ dB

## B.3 Measurement

Care should be taken for the sampling of Lin and Lout with an identical starting. The transfer function from Lin to Lout is determined by the levels Pout and Pin (at Lout and Lin respectively):

$$S_{io} = 20 \log_{10} \left( \frac{P_{out}}{P_{in}} \right) \quad (1)$$

For the determination of the transfer function an identical part of the recorded signals Lin and Lout shall be cut out (window). The time period of the window shall be identical with the time period of the white noise. For the certain receive measurement of the reflected signal the window shall start after a time period which is greater than the delay of the echo path (delay of the window).

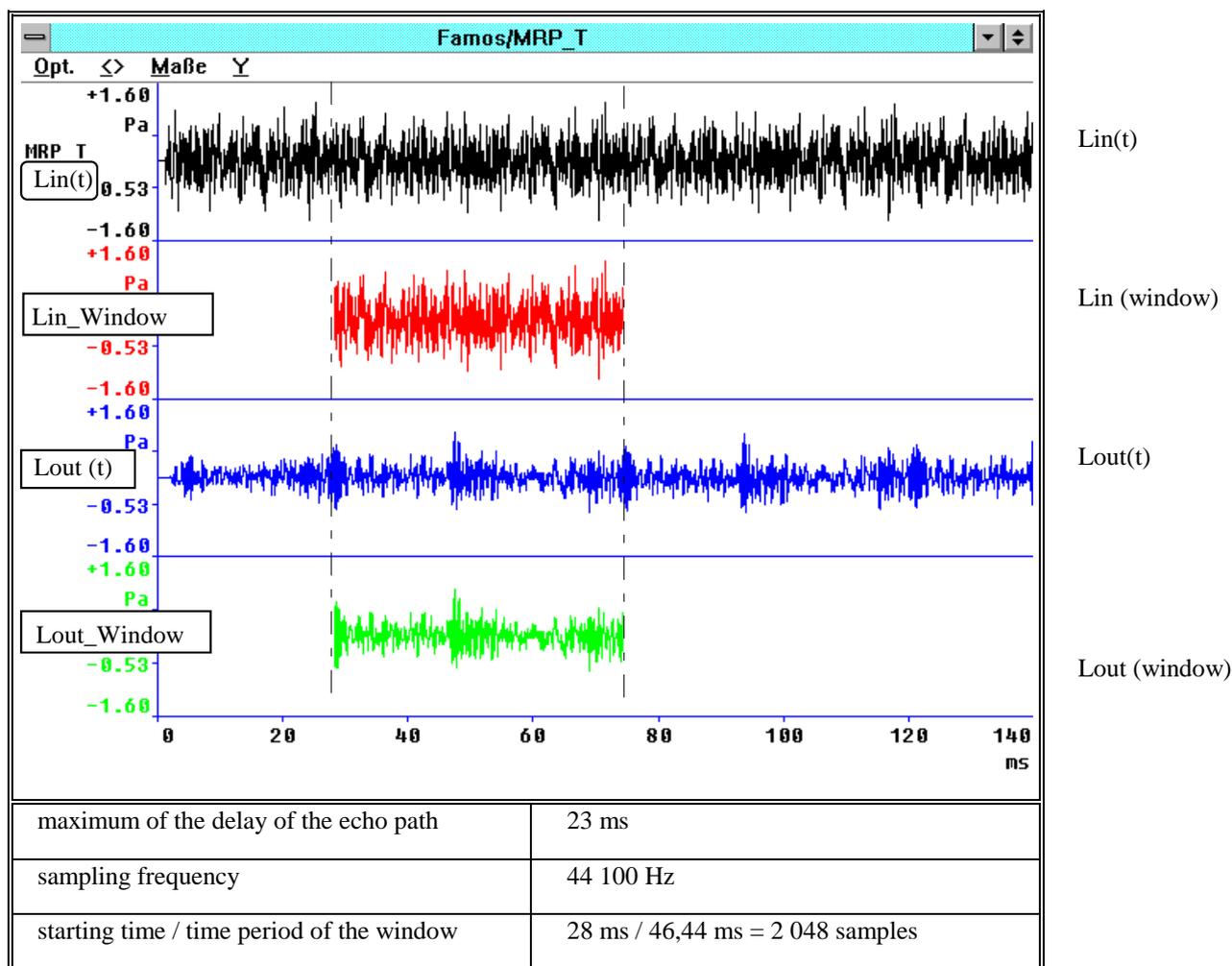


Figure B.2

## B.4 Calculation

The cut signals shall be used for the calculation of the sensitivity  $S_{io}$  by application of the Fast Fourier Transformation (FFT):

$S_{io} = \text{FFT}[\text{Loutwindow}] / \text{FFT}[\text{Linwindow}]$  for the window length of the FFT = time period of the test signal.

The time period of the window shall be applied to the FFT for the calculation to assure that all parts of the period of the test signal are used.

According to the applied bandwidth for the calculation of the Echo Loss the calculated sensitivity  $S_{io}$  shall be corrected at the upper and the lower frequency range. The values of the modulus and the phase (imaginary part) shall be reset ( $-\infty$  dB) for frequencies  $< 200$  Hz and  $> 4\,000$  Hz.

$$S_{io_{\text{corrected}}} = S_{io} \Big|_{200 \text{ Hz to } 4\,000 \text{ Hz, other values equal to } 0} \quad (2)$$

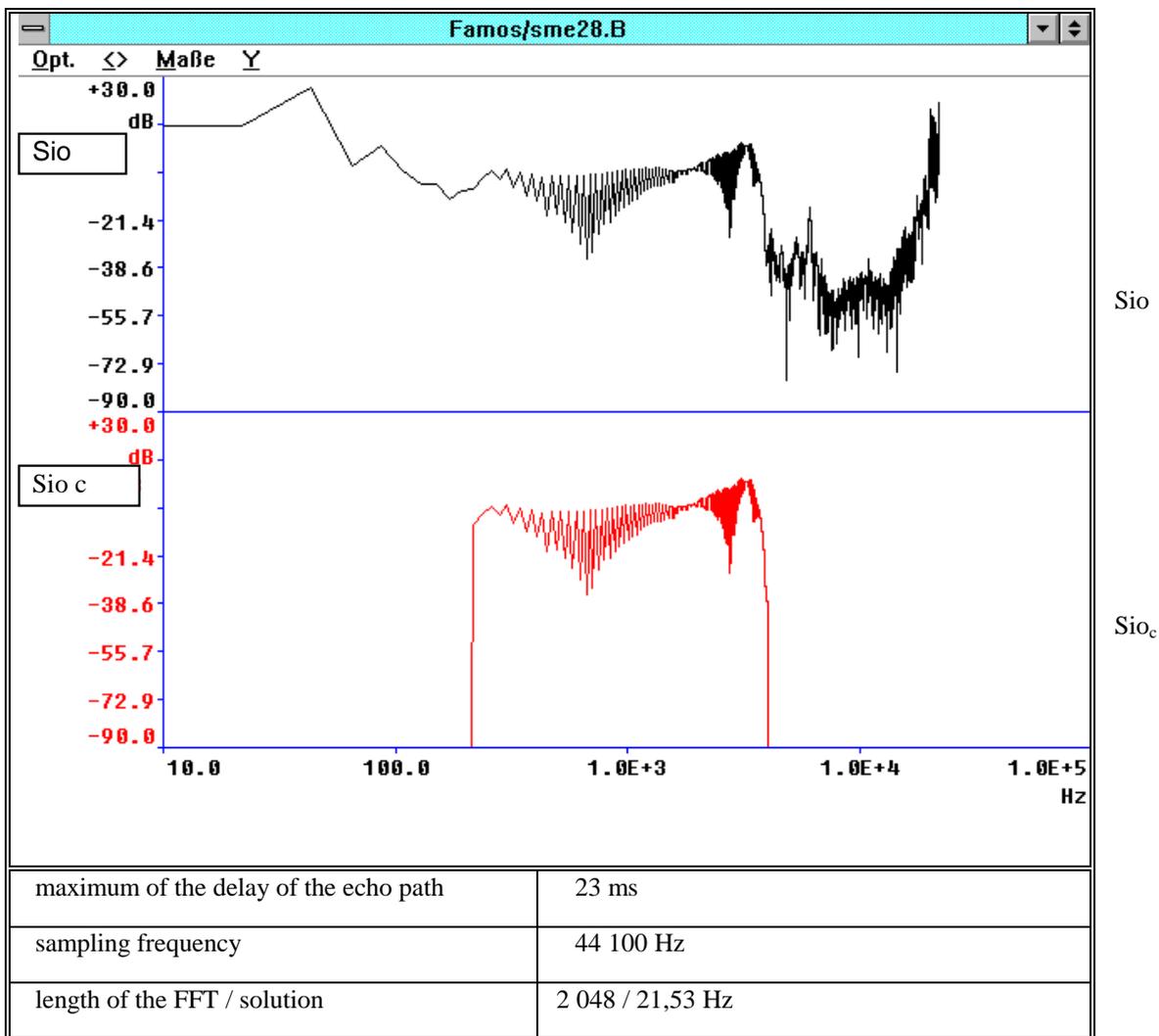
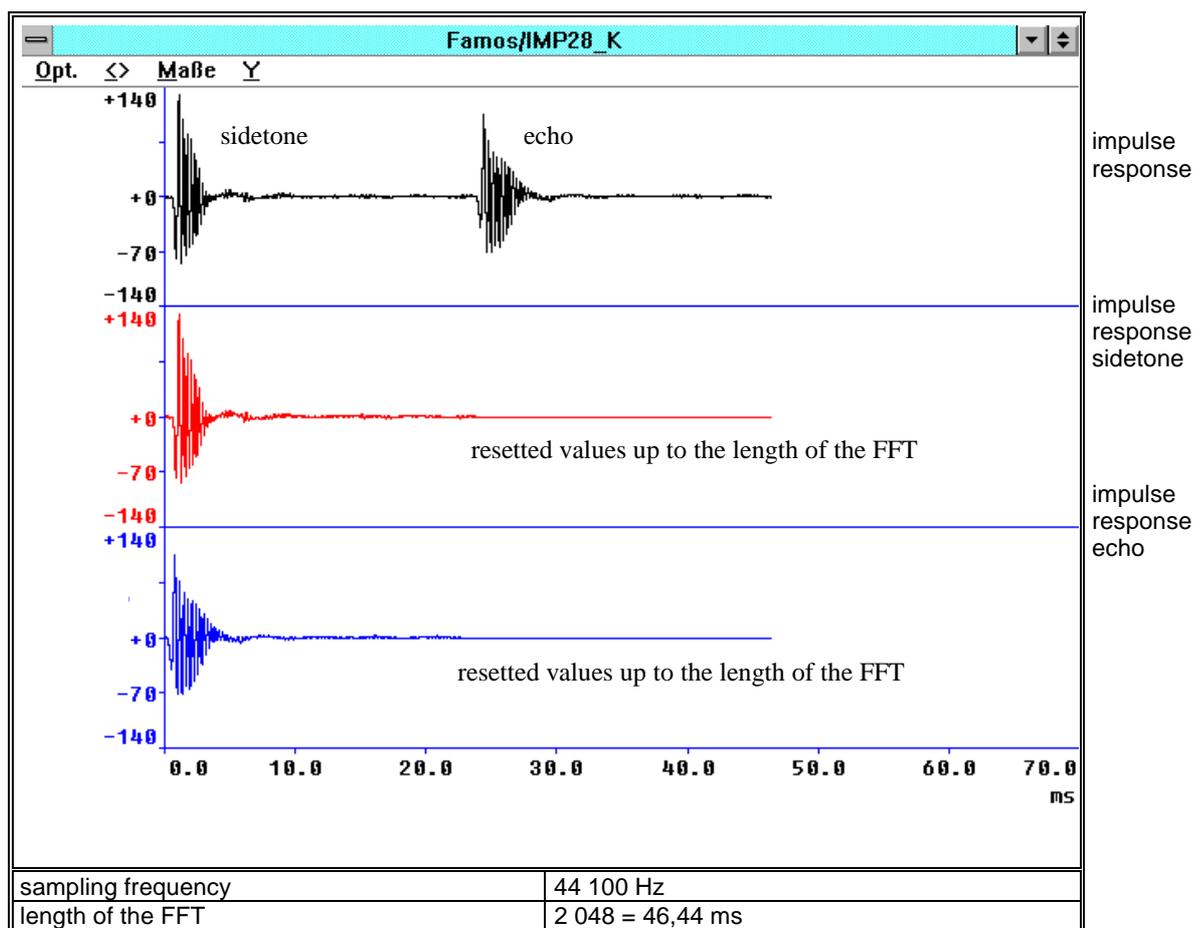


Figure B.3

The Inverse Fourier Transformation applied to the corrected transfer function  $S_{io_c}$  provides the impulse response at the time domain:

$$\text{Im}_{\text{impulse response}} = \text{iFFT}(S_{io_c}) \quad (3)$$

The impulse response demonstrates clearly the different delays for the echo and the sidetone:



**Figure B.4**

The separation at the time of the echo and the sidetone at the  $L_{out}$  is possible by use of windows at the impulse response. The windows shall overlap completely the relevant time period for the specific part of the impulse response which will be considered.

The separation of this part which corresponds to the echo by use of a special window results to a new specific echo impulse response. For the further use of this new signal the echo impulse response shall be completed by adding zeroes for this time period where the sidetone was extracted. The calculation of the echo transfer function at the frequency domain is provided by the Fourier Transformation about a rectangular window at the echo impulse response.

$$S_{io_{echo}} = \text{FFT}(I_{m_{impulse response sidetone}}) \Big|_{\text{rectangular window}} \quad (4)$$

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## Annex C (informative): Bibliography

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- ITU-T Recommendation G.121 (03/93): Loudness ratings (LRs) of national systems.
- ITU-T Recommendation G.175 (09/99): Transmission planning for private/public network interconnection of voice traffic
- ITU-T Recommendation Q.45 bis (11/88): Transmission characteristics of an analogue international exchange.
- ITU-T Recommendation Q.554 (11/96): Transmission characteristics at digital interfaces of digital exchanges

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## History

<b>Document history</b>		
V1.1.1	May 1998	Publication by EP CN
V1.2.1	July 2000	Membership Approval Procedure    MV 20000908: 2000-07-11 to 2000-09-08